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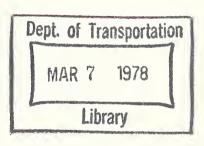
DEVELOPMENT OF ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

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PREFACE

A study of the cost of construction of underground, rapid transit tunnels in soft ground was instituted under U.S. Department of Transportation contract DOT-TSC-1104. The scope of construction work to be considered was that:

- Between existing shafts or stations and
- Completion up to and including the pouring of all finished concrete

The study was completed through an estimation of tunneling hours and downtime hours to give an expected value, and distribution about that value, of the total shift hours involved from start to breakthrough of the tunnel. Additionally, some subjective factors influencing contingency and profit are presented.

The study was sponsored by the Office of Rail Technology of the Urban Mass Transportation Administration, the Transportation Systems Center under the direction of Mr. Andrew Sluz, the Technical Monitor.

Mr. Joseph Keating, of Keating Associates, was the outside consultant and provided data for the effect of institutional factors.

Data from the Chicago tunnels were provided with the assistance of Messrs. R.I. Leland and S.J. Sulinski of the Metropolitan Sanitary District of Greater Chicago. Ing. Manuel Salvocho, of Ingenieros Civiles Asociados, S.A., kindly provided information on Mexico City tunnels. Other data were gathered and analyzed by Bechtel personnel; P.L. Shank (WMATA), N.N. Munnerlyn and F.E. Velez (BART) inspected hundreds of log sheets. Analysis of the data was performed principally by L.R. Damskey with the able assistance of V.J. Miller.

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SUMMARY

Twenty-two tunnels from the San Francisco Bay Area Rapid Transit District (BART), the Chicago Metropolitan Sanitary District, and the Washington DC, Metropolitan Area Transit Authority (WMATA) have been analyzed to determine what factors influence the Rate of Advance (RoA) through the ground. The major effect is the increase in productivity achieved through the effect of the Learning Curve. Other effects, due to soil and equipment types, are multipliers to the basic equation.

Downtime for the various pieces of tunneling and muck-removal equipment are random events that are difficult to forecast, although trends were found and estimates determined.

An important aspect of the study was to quantify the variability of the rate of advance and down time calculations. The estimator does the same in a more subjective manner - each referring to his personal source of information to decide the effects of expected soils and equipment on the rate of progress through the ground. The results of our study in quantification of these variables are a step in the direction of understanding some of the tunneling cause and effect relations and giving the causes a numerical value. Quantification of these variables should reduce the size of the contingency applied by the bidding contractors to more meaningful terms of risk.

Data on the mining progress through the ground were of a poor quality. In order to provide better data for analysis from future tunnels, recommendations have been suggested for the tunnel (Ring & Face) log. At best, the recommended data acquisition will quantify the future tunneling rates. At worst, the analyst will be given a better subjective view of what occurred during tunneling.



2. SELECTION OF COST ESTIMATING TECHNIQUES

2.1 REVIEW OF SYSTEMS ANALYSIS METHODS BASED ON COST ESTIMATES

Rapid transit tunneling is not an often repeated construction effort in which costs can be scaled to the next tunnel. Nor can a few inflation indexes be used to go from one time frame to a future period. And lastly, no two tunnels will have the same ground conditions and equipment uses. No two tunnels are the same!

Because of these differences, it seemed appropriate for the analysis to examine the tunneling systems and not their costs. Barring new technologies, some combination of personnel, equipment, and soils, taken from many experiences of the past, will be brought together for tunnels to be built in the future. Our effort, therefore, was to determine the individual contributions of each of the components. And with that knowledge, we can estimate the resources to be used for a specific future tunnel and price out the resources at their going market price at the time the tunnel is to be built. Escalation factors can be more accurately estimated on a component by component basis at that time.

2.2 SELECTION OF OPTIMUM COST ESTIMATING AND ANALYZING TECHNIQUES

The main components of a tunnel's construction are manhours, equipment depreciation and maintenance, and bulk materials.

 Bulk materials — concrete, rebar, grout materials are largely a linear function of the tunnel's length.

- Equipment depreciation and maintenance should be available from historical records as well as from published data.
- Manhours represents the crew size multiplied by the shift hours from beginning to end. (The question is how many hours will be involved? Shift hours are composed of tunneling hours plus equipment shutdown hours.)

Estimates of tunneling hours based on linear feet per hour have not resulted in an adequate estimate. The main effort should be a systems analysis of the rate of advance (RoA) through the ground.

2.2.1 The Soils Estimate

A probability analysis relating core analyses to what was found during the tunneling should be conducted. Conditional probabilities, P (Soil B | Soil A), are based on the presence of one type to predict another. And Baysian probabilities can be used to increase the likelihood of predicting probable soil characteristics with the inclusion of additional data (new core samples).

All this can be displayed by a probability tree (1,2) to determine the soils most likely to be encountered at various distances through the ground.

2.2.2 Tunneling Equipment

Several different methods of face excavation are available: the one-direction rotating cutting wheel, the cutting wheel capable of reversal, the oscillating wheel (reputed to be no longer available), the digger arm (similar to a backhoe), and manual digging. Depending on how many types of excavating processes were to be found, Discriminate Analysis could be used to find which excavation process was likely to be used with which types of soil, tunnel length, and other tunnel parameters.

2.2.3 Mucking Equipment

Discriminate analysis could also be used to determine which muck transport system fits the other tunnel characteristics best.

2.2.4 Crew Size

Crew size and the various categories of skilled and unskilled crafts are expected to be a function of the equipment used. This can be found with a simple matrix having rows and columns of excavation and types of mucking equipment.

2.2.5 Rate of Advance (RoA)

Using the weekly advance rates as the dependent variable, regression analysis can be used to relate it with the many soil characteristics, equipment used, and primary liner types.

2.2.6 Downtime

Reliability theory, together with regression analysis, can be used to estimate the amount of time the equipment would be down and unavailable for tunneling operations. Maintenance costs are, of course, related to down time.



3. QUANTIFICATION OF FACTORS WHICH INFLUENCE CONSTRUCTION COSTS

3.1 PHYSICAL CHARACTERISTICS

The set of physical variables decided on, after reviewing several sets of tunneling data, were:

Water Running in Tunne1 - $1 \rightarrow 2$ Tunnel Rate - ft/wk Cumulative Feet of Tunnel to Date Hp to Cutter/Digger Tunneling Hours in Week Total Jacking Potential of Shield - tons Shield Down Time - hr/wk OD of Shield - ft Excav Equip Down Time - hr/wk Shield + Rotating Wheel - 1/2Conveyor Down Time - hr/wk Muck Transport Down Time - hr/wk Shield + Oscillating Arms - 1/2 Shield + Digger Arm - 1/2 Misc Down Time - hr/wk Shield + Manual Digging 1/2Admin Down Time - hr/wk Mucking Equip: Conv Belt + Train - 1/2 Total Shift Time - hr/wk Mucking Equip: Conv Belt + Truck - 1/2 Silt & Clay - $1 \rightarrow 2$ Mucking Equip: Rubber Tired Truck 1/2 Clay & Sand - $1 \rightarrow 2$ Sand & Gravel $-1 \rightarrow 2$ Grnd: Non-Cohesive $-1 \rightarrow 2$ Cobbles & Boulders - $1 \rightarrow 2$ Grnd: Running - $1 \rightarrow 2$ Cemented - $1 \rightarrow 2$ Lining: Ribs & Lagging - 1/2 Peat & Trash - $1 \rightarrow 2$ Lining: Conc Pipe Jacked into Cohesive $-1 \rightarrow 2$ Place - 1/2 Last Week of Tunneling = 1/2Tunnel Pressure - psig

 $1 \rightarrow 2$: Varies between values of 1 and 2 1/2: A no/yes variable with a value of 1 or 2, usually

Based on the tunnels investigated, we believe these data items are adequate to describe the tunneling system and its RoA.

During the last six tunnels investigated, the soil was predominately sand with clay and with poor standup time. Some breasting was required, and consideration was given to adding this as another parameter. It was dropped because breasting was not the major cause of slowdown (even though

breasting did slow the RoA). The major cause was adequately described by the basic soil variables of Sand and Clay and Running Ground.

The quantification of the physical factors is discussed in Section 5 and 6, Analysis of Data and Predicting Equations.

3.2 INSTITUTIONAL EFFECTS

Institutional effects are generally subjective variables that enter into the contingency. To a large degree they are subjective because they are not directly measureable. The factors decided upon for this study are:

(1) Schedule/Time

Traditionally, bar charts have been used for scheduling; but these charts only show the time for beginning and end of activities. A network (CPM/PERT) chart shows the interrelation of activities which must be completed before another activity can start. Without this type of analysis, proper planning cannot occur; time overruns on subsequent activities are not likely to be understood.

(2) Direct Costs - Owner Acquisition

- <u>Land and Rights-of-Way</u>. Generally the owner can more expeditiously accomplish these activities (including the right of eminent domain). Entry to buildings and their preexcavation underpinning are also included.
- Materials. For items of equipment that will span more than one subcontract, procurement costs may be reduced, including the cost of financing monies.
- <u>Insurance</u>. The same rules would pertain to each subcontractor. The consistency of the policy and its jobwide scope should reduce the premium costs.
- <u>Building Permits</u>. This would not seem to be as cost sensitive to owner participation. Although

the reduction of personnel involved (owner and city agents) might expedite permit acquisitions, each must be processed individually. Negligible effect.

(3) Labor Productivity

Total job agreements are preferential so that each craft is responsible and is treated the same on each subcontract. It would appear to be more expeditious if the Owner negotiated the agreement and had it in hand by the time the bids were awarded.

It is expected that there are differences in productivity.

Factors were investigated. Our findings indicate a wide range of subjectivity with little or no quantification of the indices.

The demand on a given labor market is believed to have an effect: e.g., if the building economy is booming in a specific area, additional demands on the local labor market are likely to be met with personnel of marginal productivity.

Compressed air work is subject to local labor negotiations. During the BART construction contracts 1M0031/1S0022, the generalized maximum hours of work were restricted by the air pressure to:

Max hr =
$$8.0-0.134(psig)$$
 (3.1)

Labor negotiations resulted in an annual pay rate increase. For the three-year period, 1968 to 1971, and including the annual inflation index, the hourly wage rate is described by:

\$/Hr =
$$\left[1.1036 \text{ (Max psig)}^{-0.0133}\right]^n \star \left[\frac{1}{0.1715-0.0032 \text{ (Max psig)}}\right]$$
.

where: n = years since contract
 was first in effect

The above applied to all union rates while under pressure. Foremen received \$4/shift in addition.



4. DATA DESCRIPTION

- 4.1 SOURCES. The data were found in the following forms:
 - 1. BART: 1M0031-MR, ML; 1R0053-RR, RL.

The excavation and downtime data had been summarized into weekly increments. Soil characteristics were taken from a soil profile and written verbal descriptions. Other data were in the tunnel report summaries.

2. BART: 1S0011-TR,TL,SR,SL; 1S0051A-SR,SL.

All data were obtained from rough logs: the ring erection log with two rings/page, the foreman's log, and a weekly advance summary.

3. Chicago Metropolitan Sanitary District: Upper Salt Creek tunnels 1, 2, and 3.

All data were taken from weekly data summaries, soil profiles, and written records of equipment used. In one case, it was necessary to contact the shield fabricator for data.

4. WMATA: 1F0012-FIB North Outbound, North Inbound, South Outbound, South Inbound; 1F0021-F2A Outbound, Inbound Branch Route Outbound, Branch Route Inbound; 1D0091-D9.

All data were taken from the ring report logs (one page/ring), soil profiles, written rough logs, and oral communication with personnel involved in the tunnel excavations.

5. Mexico City Deep Sewer.

The data were received too late for study and analysis. The text is in Spanish and is appended (Appendix B) as a potential source of information. The tunnel characteristics were different enough to have been useful in the analysis.

Copies of the original data are found in Appendix A-1,2.

4.2 SOILS

Soils engineering suggested classifications other than those ultimately used. The difference lay in that the descriptions used by the face crew foreman were not those of a soils engineer, and the face crew foreman, for all his lack of exact scientific expertise, was in the hole and making a continuous log of the face conditions as he saw them. The categories finally used were:

- Silt and Clay
- Clay and Sand
- Sand and Gravel
- Cobbles and Boulders
- Peat and Trash
- Cemented
- Cohesive
- Running.

For each soil category, a value between 1 and 2 (0 to 100%) was to be assigned so as to describe the average face composition. The logged data did not permit the inclusive description, and in many cases the composition does not add to 100 percent. Fortunately, the transitory changes did not appear to have major effects on the RoA.

Running water affected the RoA whether the water was perched or from an unlowered water table. The quantity of flowing water was not metered. Our quantification became:

- 1.0 Dry
- 1.25 Moist
- 1.50 Wet
- 1.75 Running and impeding operations
- 2.0 Flooding and stopping operations.

4.3 PRIMARY LINING

All but one tunnel used either steel segmented rings or ribs and lagging. The one exception was in Chicago's Upper Salt Creek No. 2 sewer intercept, where a 9.28-foot-diameter shield was used. The concrete lining, being both primary and finished, was lowered in segments through the nearest following shaft and jacked into place over a slip bed of wet bentonite. Later the bentonite was replaced with a cement grout.

4.4 MINING OPERATIONS

For each tunnel analyzed from the basic logged data, the time for the shove, the ring erection, and what is here called "dead time," was obtained. From these data, a pseudo RoA equation was developed for each tunnel involving the intercept and learning-curve exponent in the form of equation (5-1). Time and resources did not allow further analysis. It is suggested that further study of the data may disclose information that would permit the tunneling contractor to increase his efficiency for these operations.

4.5 DATA PROCESSING

In both the RoA and downtime estimating equations, the logic suggested that cumulative feet would be the dominant independent variable (in the latter equation, Σ ft represents time, most frequently found in reliability analyses), and all other independents would act as multipliers representing the perturbations around the relation between the dependent and independent variables. To accomplish this, the multiplier must have a value of 1 when the parameter in question has no effect; a "1" or a "2" was used in no/yes statements and a range of 1 to 2 was used to denote a characteristic that varied fractionally between 0 and 1.

4.6 GROUT

Only the BART 180011 TL/SL tunnel's grouting data were analyzed. Both pea gravel and cement grouts were used in the ratio of 1.54:1. The total grout consumption was 4.1 percent greater than the theoretical void left by the shield.

Although of minor cost, it may be possible to relate the consumption of grout to the soil types.

5. ANALYSIS OF DATA

5.1 BACKGROUND

Tunneling, taken in its entirety, comprises so many diverse activities that it soon became obvious that it would be necessary to divide it into subtasks that were basically homogeneous in order to model each as a unit operation. The resulting concept is shown in Figure 5-1.

The activities within the dotted line framework are concerned only with nonmonetary resources.

- The tunnel length defines the quantities of bulk materials to be used. It also influences the choice of tunneling equipment and influences the RoA.
- Soil characteristics and primary liner types both influence the tunnel equipment choice and affect the rate of advance.
- Tunnel equipment sets the crew size, influences the contractor's capital costs, and affects the RoA.
- The above then set the RoA and have a large effect on equipment reliability.
- From the RoA, the tunneling hours are estimated.
- Equipment reliability estimates the downtime hours.
- The combination of crew size, tunneling, and down hours provides the estimate of nonexempt crew manhours.
- Current costs are then applied to estimate the tunneling cost without contingencies and profit.
- Institutional factors (identified contingencies), unidentified contingencies, and profit are applied to reach a total cost.

• Throughout the calculations, an error of estimate is carried. The various costs (the result of the average values for all the above) and their variations are combined in a risk model (Monte Carlo) simulation to obtain a range of total costs and the probability of the occurrence of each.

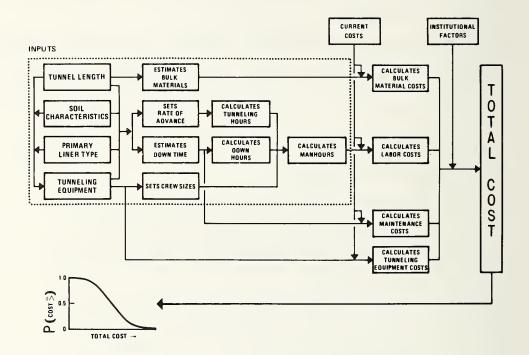


Figure 5-1. Economic Factors in Tunnel Construction

5.2 LEARNING CURVE

Literature research on Rate of Advance analysis yielded little in the way of mathematical analysis. Several authors mentioned that the RoA increased as the crews learned to work together and equipment deficiencies were eliminated. (3) One author (4) used the term "Learning Curve." An analytical approach is given by Pietrzak and McJunkin (5) based on hard-rock tunneling. Although these authors do not provide details of their model's logic, it does appear that there may be similarities between their model and the work being reported on here.

The concept of a learning curve where subsequent repetitive work is achieved at a higher rate of productivity is certainly not new. (6)

The airplane frame industry found that with their mixture of manual and machine work, an 80-percent curve, on the average, defined their increase in productivity. That is, each time the number of airframes produced was doubled, the last unit required only 80 percent as much time as the reference unit. In the case of tunneling, using the average learning curve exponent found for all the tunnels studied, 82.3 percent, and an initial rate of 4.0 hours/foot, the following rates might be expected.

Cumulative Feet of Tunnel	Hours/foot	Feet/hour(RoA)
1	4	0.25
2	3.29(4x0.823)	0.30
4	$2.71(3.29 \times 0.823)$	0.37
•	•	•
•	•	•
128	1.02(1.243x0.823)	0.98
•	•	•
•	•	•
1024	0.57(0.693x0.823)	1.75
2048	$0.47(0.57 \times 0.823)$	2.13
4096	$0.39(0.47 \times 0.823)$	2.59

In general, industry has found that the degree of learning depends on the mixture of men and machines used. Figure 5-2 describes the change in learning curve, as reported by Hirschmann, (7) with the percentage of manual effort used in the specific task.

It seemed obvious that the learning curve should apply to the repetitive tasks of the shove and primary ring erection. Theoretically, the learning curve should be a continuous negative-sloping curve. In actual practice, interruptions to the work (equipment failures, planned shutdowns, etc) as well as modifications to the tasks (different soils, substitution of new equipment) occur to change the position of the curve.

A new soil might displace the curve. New equipment might merely involve an upward perturbation and then a rapid increase in productivity to again reach the former curve position.

In general, what might have been expected from a theoretical "learning curve" approach to the analysis is what was found for the RoA in soft-ground tunneling.

An example of the persistence of the Learning Curve was found in the BART RR/RL tunnels. Upon completion of the RR tunnel, the shield was immediately moved to the RL tunnel and tunneling continued. Except for an initial perturbation to the RoA, the advance rate quickly fell into line with the rate being achieved at the completion of the RR tunnel.

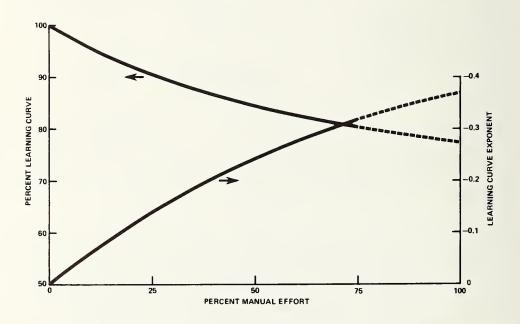


Figure 5-2. Relation Between the Percentage Mix of Manual and Machine Effort, Percent Learning Curve, and Learning Curve Exponent

5.3 PRELIMINARY ANALYSIS

In order to explore the learning-curve concept, raw data for several tunnels were plotted; Log (hr/ft) vs Log (cumulative ft), Figure 5-3. The learning-curve function is of the form

where:
$$\Sigma$$
 ft = cumulative feet
$$I = hr/ft \text{ for the first foot of excavation}$$

$$E = \text{ the learning-curve exponent}$$

$$Hr/ft \equiv (RoA)^{-1}$$
and: Percent learning curve = 100 exp (E * Ln 2) (5.2)

Data sets for the first three tunnels had been summarized into weekly units of data; therefore, all subsequent data accumulations were kept in a weekly format. The dependent variable (hr/ft) is the weekly tunneling hours, exclusive of any down time, divided by the feet of advance accomplished during the week.

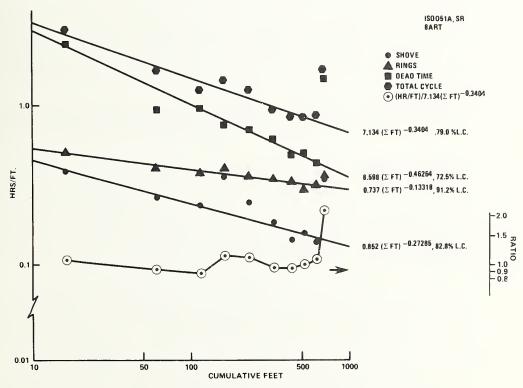


Figure 5-3. Tunneling Rate of Advance vs Cumulative Tunnel Length

The independent variable (Σ ft), in order to be compatible with the weekly average characteristics of the dependent variable, is calculated as the cumulative sum through the previous week's excavations plus half of the current week's distance.

The data can then be regressed to determine the values of I and E. The resultant equation can then be considered to be a rate equation

$$\frac{d(hr)}{d(ft)} = I(\Sigma ft)^{E}$$
 (5.3)

and can be integrated between distances n and n + m.

$$d(hr) = \iint_{n}^{n+m} (\Sigma ft)^{E} d(ft)$$
 (5.4)

For reasons that will be discussed later, valid results will not be obtained by integration between zero and the total number of feet in the tunnel; integration should be in parts to conform to the types of soils and other perturbations expected to be encountered during the excavation.

By calculating the number of hours required to excavate the tunnel and given the crew size, the number of tunneling manhours is estimated.

However, equipment does fail. And when the equipment is down for repair (or, for that matter, whenever there is a shutdown), the crew is usually on standby and must be paid. Therefore, it is necessary to estimate the downtime that may be encountered. Reliability theory has found that equipment generally responds as shown in Figure 5-4.

In developing a failure-rate function, the dependent variable was defined as hrs down/ft and the major independent variable as cumulative feet; both specified in weekly terms as before. A predicting equation to develop the number of downtime hours during the tunnel excavation will permit the estimation of crew manhours idled. The sum of the tunneling and downtime hours is an estimate of the non-exempt payroll and the time duration of the tunneling.

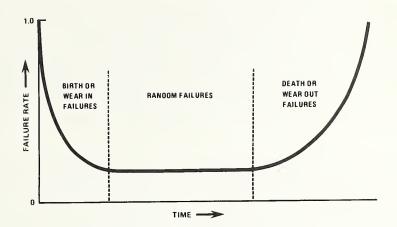


Figure 5-4. Typical Equipment Failure Rate Curve with Time

It is of primary importance to note that the Rate of Advance is not assumed (as is normally done). It is calculated, based on the conditions expected to be encountered. Among those conditions are the soil characteristics (either from a decision-tree estimate or a coreboring profile) and the equipment to be utilized.

Figure 5-1 shows the cost calculation logic. It is expected that, once the soils and tunnel length are specified, the tunneling and mucking machinery ranges are considerably reduced. And when the machinery is decided upon, barring labor union restraints, the crew size is determined. On the basis of the foregoing evolved concepts, some details of the analytical work will now be discussed.

5.4 METHOD OF ANALYSIS

Regression analysis was used to determine the effects of the so-called "independent" variables on the dependent variable, hr/ft. Independent variables should be independent from each other but, in commercial practice, a high degree of interdependence is usually found among these factors; i.e., a high degree of statistical randomness among the variables might well indicate a poorly managed project.

In fact, the lack of independence, when analyzing the individual tunnel data, resulted in the derivation of some learning-curve exponents that were considered to be impossible. The method of getting around this problem was to plot each tunnel's hr/ft vs Σ ft on log-log paper. The obvious outliers could then be eliminated. Outliers, in this sense, means those data points which are displaced from the negatively sloping line due to some other variable effects, such as a change in soils, a series of mechanical breakdowns, etc. The remaining data sets were then related, using only a desk calculator, to solve for the I and E of each tunnel.

The next step in the analysis was to find the effects of the remaining variables. The logic suggested that the effects of the other variables would be as multipliers; therefore, the regression used the logarithms of the variables.

$$\operatorname{Ln}\left(\frac{\left(\operatorname{hr/ft}\right)}{\operatorname{I}\left(\Sigma \operatorname{ft}\right)^{E}}\right) = \operatorname{f}\left(\operatorname{Ln}X_{1}, \operatorname{Ln}X_{2}, --, \operatorname{Ln}X_{n}\right) \tag{5.5}$$

The above reasoning was tried on several tunnels. The following set of figures demonstrates an example from one of the WMATA tunnels. Figure 5-5 is the plot of hr/ft vs Σ ft. Figure 5-6 is a logarithmic

plot of the same data with the assumed outliers circled. Figure 5-7 is a transformation of the dependent variable to the form used in equation (5.5) vs Σ ft; the learning-curve effect on productivity has been removed. The data have now been normalized and all data sets are scattered about a horizontal axis having a value of 1.0. Figure 5-8 is a plot of the unexplained residual (reported-predicted)* vs Σ ft after regressing in the form of equation (5.5).

The scale of the ordinate is the same as that of Figure 5-7. It can be seen, in comparing Figures 5-7 and 5-8, that the variance from the horizontal line is greatly reduced in the latter. It appears that regression analysis can develop a mathematical model that will satisfactorily estimate a tunneling Rate of Advance.

To determine how closely the tunneling hours can be duplicated, a different set of tunnel data were regressed to estimate the weekly Rate of Advance. The corrections due to soils, equipment failures, etc., are fractional multipliers whose effects are different depending upon the numerical value of hr/ft.

Two methods were used in the calculation. One was to integrate the derived equation between the weekly stations. The other was to multiply hr/ft by the weekly advance. The results are shown in Figure 5-9.

^{*}Note that the word "reported" is used rather than the usual word "actual" in calculating the unexplained residual. In general, the reported data were extremely doubtful in character. In one case, the soil changed from sand and clay to sandy clay and back again as the shifts changed. And sometimes, damp, wet, or moist sand was used interchangeably. Throughout our investigation into the raw logged data, it was obvious that little or no attention had been given to consistent observation and logging of data. And certainly no thought had ever been given to the possible future use of the data in a quantified analysis.

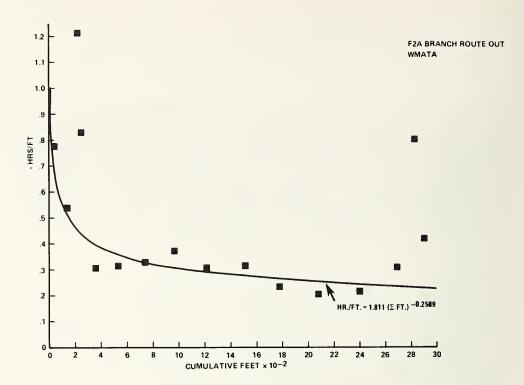


Figure 5-5. Rate of Advance vs Cumulative Tunnel Length

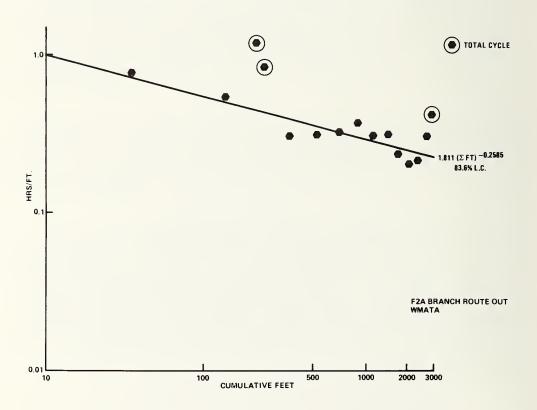


Figure 5-6. Tunneling Rate of Advance 5-10

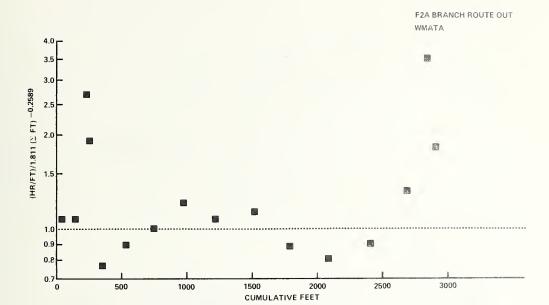


Figure 5-7. Tunnel Length; Unexplained Variations in Rate of Advance

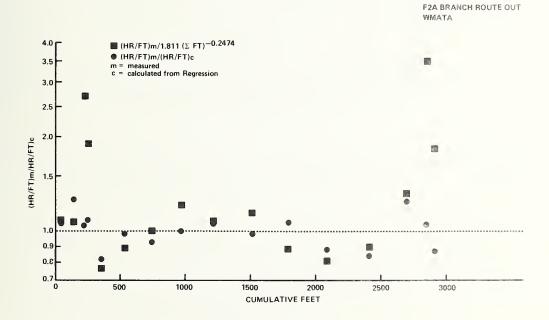


Figure 5-8. Reduction in Variance due to Equipment, Soil, and Length of Work-week Variables

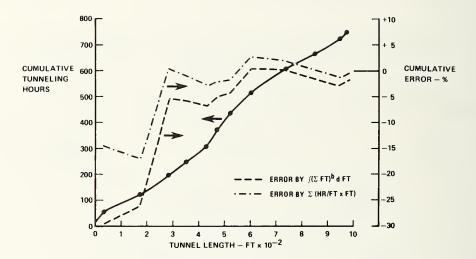


Figure 5-9. Comparison of Calculated and Reported Cumulative Tunneling Hours vs Tunnel Length

In the integration case, the error was 2.2 percent - 749.4 hours reported vs 766.0 hours calculated. In the summation case, the error was 0.7 percent - 749.4 hours reported vs 754.6 hours calculated. Again, the logic of the model development appeared to satisfactorily duplicate the reported tunneling hours.

5.4.1 Cross Tunnel Derivations

RoA equations were derived for several individual tunnels in order to investigate potential problems which might occur when all the data were combined. For instance, there were statistical outlier data points in the individual tunnel data for which there were no explanatory variables.

- An error could have occurred in the dependent variable, hr/ft. The lineal tunneling distance was probably correct, because both the starting and finishing stations were always compared with the number of rings erected. The error was most likely in the tunneling hours; i.e., shutdowns had occurred and were not reported or were incorrectly reported. This would result in too great a value for hr/ft in this data set.
- Errors in the independent variable could (and did) occur because of incomplete tunneling data logs; e.g., the soil characteristics changed and were not reported.

These outlier data were generally removed from the regression data before combining all data sets.

The combination of all the tunnel excavation data, with all the soil and equipment variations, permitted the derivation of an RoA equation that could not be derived with the limited variations in soil characteristics and single equipment sets found in individual tunnels. Additionally, the RoA equation used the intercepts and learning-curve exponents derived from the individual tunnel data.

Both the intercepts and learning-curve exponents appeared to be functions of soils, equipment, and the managerial expertise of the contractors.

No data to classify the expertise existed; therefore calculations were restricted to soils and equipment. Both derived equations gave statistically satisfactory results.

Substitution of I and E into the RoA equation permits the hr/ft to be calculated. Two methods were used to calculate the tunneling (operating) hours: integration and summing of finite units of tunneling feet.

The RoA equation (6.3) is derived in Section 6.3. For the purpose of this discussion, consider the equation to be of the form

$$hr/ft = I(\Sigma ft)^{E}(F)$$
 (5.6)

where:

hr/ft = Average time to excavate during a specific distance of the tunnel's length.

I & E = Intercept and learning curve exponent

F = A consolidation of all correction factors.

Calculation of the tunneling hours requires that the tunnel be broken into sectors of roughly equivalent soil expectations. Correction factors are then calculated for each sector. The weekly averages were used here.

5.4.2 Integration Method

Equation (5.6) is integrated between stations d and d+i along the tunnel. Each sector is considered. The tunneling hours are calculated by

$$hrs_{ii} = I F_i \int_{d}^{d+i} (\Sigma ft)^{-\bar{c}} d (ft)$$
 (5.7)

to obtain

$$hrs_{ii} = \frac{|F_i|}{E+1} (\Sigma ft)^{E+1} d^{d+i}$$
(5.8)

Total tunneling hours are the sum of the sector hours

Total Hours =
$$\sum_{i=1}^{j} (hr)_{i}$$
 (5.9)

5.4.3 Summation Method

The only difference in summation is the calculation of the sector hours; they are now estimated by using equation (5.6) directly and multiplying by the number of feet, m, in the sector, i.

hrs
$$_{is} = ft_i \mid F_i \left(\sum ft_d + 0.5 ft_i \right) \mid E$$
 (5.10)

The modification to the variable Σ ft is due to the RoA derivation useing the average rate during a sector having average correction characteristics. To conform to this logic, the cumulative feet of progress were taken to be half the distance m in sector i plus the total distance excavated up to the beginning of sector i. Total tunneling hours are as in equation (5.9).

The two methods of estimating the total tunneling hours are shown, for each tunnel analyzed, in Appendix A-3.

5.4.4 Total Down Time

To estimate the total hours required to excavate the entire length of the tunnel, the amount of non-tunneling hours due to equipment failures and administrative shutdowns must be added to the tunneling hours.

Total down time was fitted to an equation of the form shown in Figure 5-4. Because of the random nature of the failures, the equation fit

is less satisfactory, statistically, than other derived equations. The results, on a tunnel-by-tunnel basis, are shown in Appendix A-4.

It was intended to derive equations to describe the failure rates of the various excavation systems; i.e., the shield, the rotating wheel/digger arm, the mucking system, etc. Although the information is available in the data bank, insufficient time and resources precluded their derivations. Certain of these downtimes are needed in the RoA equation; e.g., shield, excavating equipment, misc. and administrative down hours/ft of advance. In addition, they are also needed to estimate maintenance costs. The latter could not be found as a separate category. Until the equations become available, the program user will continue to rely on his own data and that published by the AGC in their Contractors' Equipment Manual (7th Ed. 1974).

5.4.5 Total Hours

Total hours is the sum of tunneling and downtime hours. On a tunnel-by-tunnel basis, Appendix A-5 shows total hours, by both the integration and summing methods compared with actual hours.

5.4.6 Variability of Predictions

The only certainty about estimating is that a single monetary projection is bound to be too high or too low when compared to the final actual costs. A more useful estimate will cover the range into which the final results will probably fall. The range may be estimated subjectively by the estimator using the knowledge and background of those familiar with the task to be performed. Or, as will be discussed here, it may be quantitatively estimated from the errors of estimate produced from the statistical procedures used in deriving the equations.

A method of imputing the range is known as Monte Carlo simulation. (8) In this procedure, an equation is solved many times, and each time the equation is solved, each independent variable's coefficient is randomly

changed within the confines of each coefficient's statistical variation. In this manner, the equation, or process series, is solved enough times to permit the estimation of the distribution of the answers. The curve in the lower left corner of Figure 5-1 illustrates the result of such a simulation.

The weekly progress rate, in hr/ft., is an example of tunneling variability. The median progress value is that rate most likely to occur. However, there is approximately a 50-percent chance that this value will be exceeded. Note that Figure 5-10 is not a normal distribution; it is approximately log normal. The cumulative distribution of these data is shown in Figure 5-11 where the median RoA was 0.60 hr/ft (1.67 ft/hr). At the 80-percent probability level, the RoA was 1.125 hr/ft (0.89 ft/hr) or less. And at the 20-percent probability level, the RoA was 0.325 hr/ft (3.08 ft/hr) or less.

The variability of the tunneling hours, using equation (5.8), would now be estimated, for the integration method, by

$$hrs_{ii} = \frac{(\text{I} \pm r_{i} \sigma_{i}) e^{(\text{Ln} F_{i} \pm r_{2} \sigma_{F})}}{(\text{E} \pm r_{3} \sigma_{E}) + 1} (\Sigma \text{ ft}) e^{(\text{E} \pm r_{3} \sigma_{E}) + 1} d^{d+i}$$
(5.11)

and for the summation method, by

$$hrs_{is} = ft_{i} (\mathbf{I} \pm \mathbf{r}_{1} \sigma_{I}) e^{-(LnF_{i} \pm \mathbf{r}_{2} \sigma_{F})} (\Sigma ft_{d} + 0.5 ft_{i})^{-(E \pm r_{3} \sigma_{E})}$$

$$(5.12)$$

where:

r = random normal deviate

 σ = standard error of estimate of the individual predicting equations

Total downtime hours are calculated by

D hrs_i = ft_i e
$$^{\text{(Ln DH}_1 \pm r \sigma_{DH})}$$
 (5.13)

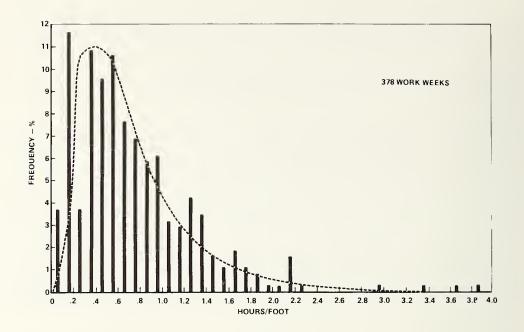


Figure 5-10. Distribution of Weekly Average Rates of Advance

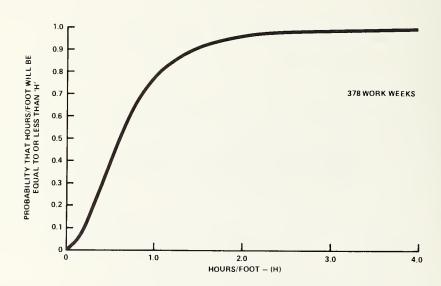


Figure 5-11. Cumulative Distribution of Weekly Average Rates of Advance

Equations (5.11) through (5.13) calculate the distribution of hours for sector i. To obtain the total hours over the tunnel's length, equation (5.9) is increased to include the individual sectors' variability. To do this it will be necessary to calculate the variance of the estimate for each sector, i, sum the variances over the sectors, and then take the square root of the sum. This is the standard error of estimate of the total hours.

$$\sigma_{i}^{2} = \frac{\sum (hr_{i}^{2}) - (\sum hr_{i})^{2}/N}{N \cdot 1}$$
 (5.14)

where;

hr,= Hours calculated for sector i

N = Number of iterations used to calculate the distribution of hours

The total hours variation, or standard error, is

$$\sigma_{\sum hr} = \begin{bmatrix} j \\ \sum (\sigma^2)_i \\ i = 1 \end{bmatrix} \quad 0.5 \tag{5.15}$$

Equation (5.9) is now modified by adding the results of equation (5.15) to obtain

Total hours
$$= \sum_{i=1}^{j} (hr)_{i} \pm \left[\sum_{i=1}^{j} (\sigma^{2})_{i} \right]^{0.5}$$
 (5.16)

The distribution of total in-the-hole hours is calculated from equation (5.16).

The above means of estimating the tunneling and downhours are based on random occurrences during normal operations; extraordinary events were excluded from the analysis. For instance, on one pair of parallel tunnels, the shield passed through shafts at 12.5 and 44.5 percent of the total tunnel distance. The contractor opted to spend about two weeks at each shaft on each tunnel for shield and excavator wheel maintenance and modifications. In addition, when the shields were within 200 feet of the tunnels' ends, forward progress was halted as the station was not ready for the breakthrough.

5.4.7 Other Costs

After the total shift hours are estimated, crew staffing and current labor costs are combined to estimate the labor cost distribution. Data on staffing were obtained for most of the tunnels. Properly, the possible variance in both the staffing and labor costs are estimated and combined with total hours variance, using the technique of the propagation of error (variance), to calculate the labor cost distribution.

The parameters of tunnel length, anticipated soil characteristics, and primary liner types are expected to influence the selection of equipment for excavation and mucking.

In the time available, maintenance costs, either total or on individual items of equipment, could not be found. It is not known whether these costs are individually itemized or are buried in other operating costs.

The effect of not quantifying crew, equipment, and maintenance costs, either because all or part of the data were not available or could not be found, results in a void in the calculation procedure. These data are normally available to contractor's estimators from the contractor's properietary information data bank. The disadvantage to the proposed calculation procedure is that the information can not be weighed to benefit from the experience of many tunneling operations. We believe that future studies should find and analyze these histories.

6. PREDICTING EQUATIONS

Derivation of the predicting equations was accomplished by stepwise multiple regression. The first equation computer run, after eliminating variables that logic suggested should not be included, was to determine the correlation coefficients between the individual remaining independent variables and those data sets that appeared to be outliers (due to a lack of explanatory variables or just poor data). Outlier data were eliminated on the preliminary tunnel-by-tunnel runs.

A technique used to reduce intercorrelation between variables is to create new variables by adding and subtracting; e.g., if \mathbf{X}_1 and \mathbf{X}_2 are highly correlated, it may be possible to find coefficients for each that are less correlated or completely independent by adding the new variables \mathbf{X}_3 and \mathbf{X}_4 to the regression matrix, where

$$x_3 = x_1 + x_2$$

 $x_4 = x_1 - x_2$

If the regression results included all four variables, such that

$$Y = a + b X_1 + cX_2 + d X_3 + e X_4,$$

the resulting coefficients for X_1 and X_2 would be for

$$X_1$$
: b + d + e

and for

$$X_2$$
: c + d

The above technique was used for all correlation coefficients $> \pm 0.3$. Unfortunately, this procedure does not directly give coefficient standard errors of estimate. In the example above, an error of estimate is calculated for all four variables.

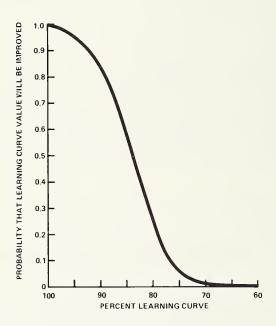


Figure 6-1. Distribution of Learning Curve Values

6.1 THE RATE OF ADVANCE EQUATION LEARNING CURVE EXPONENT

The Learning Curve Exponent varied from tunnel to tunnel; the average for the 21 tunnels was -0.281 (an 82.3 percent curve) with a standard deviation of 0.071. The cumulative distribution of the exponents found is shown in Figure 6-1. Because of the large variation in the exponent, a means of predicting is required. Managerial control undoubtedly has a large influence on the exponent (a measure of productivity) but was unknown for analytical purposes. We were quite aware of the potential value of such a subjective measure of supervisory control; however, in past attempts to quantify this variable after-the-fact, it was found that the inclusion was usually statistically nonsignificant. Nor did personnel want their gradings recorded. The subject is noted here to signify that the variable was recognized as meaningful.

In section 3.1 it was stated that the symbols $1 \rightarrow 2$ and 1/2 mean that a parameter either has an assigned value which varies between 1 and 2 or has a yes/no value of 1 or 2. The 1,2 variation was chosen for computational reasons rather than a 0,1 range, and is used in this and subsequent derived equations.

Equation (6.1) gives some quantitative insight into the effects of the independent variables on the rate of productivity increase. For instance,

- Increasing the work week from 40 to 80 hours is about a 19% increase in the exponent. A further increase to a 120-hour work week has a marginal increase of only about 9 percent. The rationale might be that the discontinuance of starting and stopping daily operations is reflected in the tunneling productivity exponent.
- Tunneling in running water (a value of 1.75 assigned) vs tunneling in moist ground (1.25) reduces the productivity rate exponent by approximately 250 percent.
- The productivity exponent is bettered by increasing the jacking potential, and it is reduced with the cross section area of the shield.

• Except for the coefficients for soil cobbles and boulders, and for peat and trash (for which there were insufficient data), the effects of soils on the productivity rate can be estimated.

Table 6-1 shows the exponent observed for the individual tunnels, the predicted value, and their differences.

LEARNING CURVE EXPONENT = -0.5538 - 0.00938 *

Ln (Total Shift Hr/Wk) + 0.03025 * Ln (Silt and Clay: $1 \rightarrow 2$) -0.03271 *

Ln (Cobbles and Boulders: $1 \rightarrow 2$) + 0.06094 * Ln (Cemented Ground: $1 \rightarrow 2$) - 0.23648 *

Ln (Peat and Trash: $1 \rightarrow 2$) + 0.03254 * Ln (Cohesive Ground: $1 \rightarrow 2$) - 0.03254 *

Ln (Running Ground: $1 \rightarrow 2$) + (i,02192 * Ln (Water Running at Face: $1 \rightarrow 2$) - 0.05555 *

Ln (Tunnel Working Pressure — Psia) — 0.03964 * Ln (Jacking Potential — Tons/ft²)

+ 0.17693 * Ln (OD of Shield - ft) + 0.04705 *

Ln (Shield and Wheel: 1/2) + 0.05597 * Ln (Shield and Digger Arm: 1/2) - 0.04746 *

Ln (Conveyor Belt and Tru-k: 1/2) + 0.04705 * Ln (Rubber Tired Muck Vehicle: 1/2);

$$S_v = 0.051 \qquad R^2 = 0.9699$$
 (6.1)

Table 6-1

COMPARISON OF ESTIMATED AND PREDICTED LEARNING CURVE EXPONENT

System	Contract	Tunnel	Observed Value	Predicted Value	Difference
BART BART BART BART BART BART BART BART	1M0031 1M0031 1R0053 1S0011 1S0011 1S0011 1S0051A 1S0051A	MR ML RR/RL TR TL SR SL SR SL SR SL	-0.2920 -0.2501 -0.2343 -0.2706 -0.3977 -0.2363 -0.3621 -0.3404 -0.3940 -0.4016	-0.2875 -0.2741 -0.2461 -0.3215 -0.2904 -0.2805 -0.3295 -0.3472 -0.3317	-0.0045 0.0240 0.0018 0.0509 -0.1073 0.0442 -0.0326 0.0068 -0.0623
Chicago Chicago	68-405-2S 68-406-2S	USC #2 USC #3	-0.3385 -0.2415	-0.3391 -0.3215	0.0006 0.0800
WMATA	1F0021 1F0021 1F0021 1F0021 1F0012 1F0012 1F0012 1F0012 1D0091	F2A Out F2A In F2ABR Out F2ABR In F1B No. Out F1 No. In F1 So. Out F1B So. In D9 So. In	-0.2764 -0.2192 -0.2589 -0.3158 -0.2229 -0.2673 -0.1287 -0.2055 -0.2476	-0.2578 -0.2607 -0.2811 -0.2777 -0.1914 -0.2324 -0.1825 -0.1839 -0.2268	-0.0186 0.0415 0.0222 -0.0381 -0.0315 -0.0349 0.0538 -0.0216 -0.0208

Based on Individual Tunnels, the:

Standard Error of Prediction: 0.0462

Amount of variability Removed by Predicting Equation: 55.4%

6.2 THE RATE OF ADVANCE EQUATION INTERCEPT

Each tunnel not only had a different learning curve exponent, but also had a different intercept value (the theoretical time to mine the first foot). The mean value of all the data was 3.815 with a standard deviation of 2.557 hr/ft. The cross tunnel computer run was made prior to the inclusion of all the data (322 data sets vs 388 finally available). Time and resources prevented a final run.

The derived equation (6.2) is given below. Table 6-2 shows the individual tunnel's observed intercept as well as that predicted.

Intercept =
$$0.4121*$$
 $\begin{pmatrix} \text{Silt} \text{ and Clay} \\ 1 \rightarrow 2 \end{pmatrix}^{0.2215} * \begin{pmatrix} \text{Clay and Sand} \\ 1 \rightarrow 2 \end{pmatrix}^{0.1216} *$

$$\begin{pmatrix} \text{Sand and Gravel} \\ 1 \rightarrow 2 \end{pmatrix}^{0.1928} * \begin{pmatrix} \text{Peat and Trash} \\ 1 \rightarrow 2 \end{pmatrix}^{-1.2698} * \begin{pmatrix} \text{Cemented Ground} \\ 1 \rightarrow 2 \end{pmatrix}^{0.146} *$$

$$\begin{pmatrix} \text{Cohesive Ground} \\ 1 \rightarrow 2 \end{pmatrix}^{0.208} * \begin{pmatrix} \text{H}_2\text{O at Face} \\ 1 \rightarrow 2 \end{pmatrix}^{0.2069} * \begin{pmatrix} \text{Tunnel Pressure} \\ 1 \rightarrow 2 \end{pmatrix}^{-0.1276} *$$

$$\begin{pmatrix} \text{Running Ground} \\ 1 \rightarrow 2 \end{pmatrix}^{0.3538} * \begin{pmatrix} \text{Shield and Wheel} \\ 1 \rightarrow 2 \end{pmatrix}^{0.0716} * \begin{pmatrix} \text{Shield and Digger arm} \\ 1 \rightarrow 2 \end{pmatrix}^{0.2068} *$$

$$\begin{pmatrix} \text{Shield and Manual Digging} \\ 1 \rightarrow 2 \end{pmatrix}^{0.5694} * \begin{pmatrix} \text{Conveyor Belt and Train} \\ 1/2 \end{pmatrix}^{-0.2784} *$$

$$\begin{pmatrix} \text{Conveyor Belt and Truck} \\ 1/2 \end{pmatrix}^{-0.4136} * \begin{pmatrix} \text{Rubber Tired Vehicle} \\ 1/2 \end{pmatrix}^{1.5395} *$$

$$\begin{pmatrix} \text{Ribs and Lagging} \\ 1/2 \end{pmatrix}^{-1.1369} * \begin{pmatrix} \text{Concrete Pipe Jacked In} \\ 1/2 \end{pmatrix}^{-2.6217} * e^{-7.3957} * E$$

$$\begin{pmatrix} \text{Ribs and Lagging} \\ 1/2 \end{pmatrix}^{-1.1369} * \begin{pmatrix} \text{Concrete Pipe Jacked In} \\ 1/2 \end{pmatrix}^{-2.6217} * e^{-7.3957} * E$$

$$\begin{pmatrix} \text{Ribs and Lagging} \\ 1/2 \end{pmatrix}^{-1.1369} * \begin{pmatrix} \text{Concrete Pipe Jacked In} \\ 1/2 \end{pmatrix}^{-2.6217} * e^{-7.3957} * E$$

Table 6-2

COMPARISON OF ESTIMATED AND PREDICTED RATE OF ADVANCE INTERCEPT

System	Contract	Tunnel	Observed Value	Predicted Value	Difference
BART BART BART BART BART BART	1M0031 1M0031 1R0053 1S0011 1S0011 1S0011	MR ML RR/RL TR TL SR SL	2.497 2.391 9.314 3.035 6.754 2.811 7.856	2.692 2.689 10.661 5.045 5.368 3.823 5.136	-0.195 -0.298 -1.347 -2.010 1.386 -1.012 2.720
BART BART Chicago Chicago Chicago	150011 150051 150051 68-404-2S 68-405-2S 68-406-2S	SE SR SL USC #1 USC #2 USC #3	7.134 8.553 3.476 0.722 0.783	1.961 0.716 1.675	2.720 0.796 -2.086 1.515 0.006 -0.892
WMATA	1F0021 1F0021 1F0021 1F0021 1F0012 1F0012 1F0012 1F0012	F2A Out F2A In F2ABR Out F2ABR In F1B No. Out F1B No. In F1B So. Out F1B So. In D9 So. In	2.390 2.353 1.811 2.928 3.083 3.456 1.776 2.108 4.879	3.194 3.624 2.488 3.007 2.431 2.872 2.398 2.453 4.217	-0.804 -1.271 -0.677 -0.074 0.652 0.584 -0.622 -0.345 0.662

Based on Individual Tunnels, the:

Standard Error or Prediction: 1.201

Amount of Variability Removed by Predicting Equation: 76.8%

Some conclusions that can be inferred about the initial Rate of Advance from the equation are:

- Relative to the clay and sand category,
 - silt and clay is about 7 percent slower,
 - sand and gravel is about 5 percent slower,
 - cemented ground is about 2 percent slower,
 - cohesive ground is about 6 percent slower,
 - running ground is about 17 percent slower.
- Compared with the rotating cutting wheel, and where soil conditions will permit alternate excavation methods,
 - the digger arm is about 10 percent slower,
 - manual digging is about 41 percent slower
- Compared with a conveyor belt and tram for muck removal,
 - a conveyor belt and truck are about 9 percent faster,
 - a rubber-tired vehicle is about 35 percent slower.
- The initial rate is inversely proportional to the learning curve exponent (E).

6.3 RATE OF ADVANCE EQUATION

The large matrix size, 115 real and created variables, required the location of a computer program with larger capacity. The time delay reduced the time available for analysis. Although equation (6.3) predicts with a high degree of accuracy, improvements can be made by manipulation of data and the inclusion of new types of soils (no glacial till soils were included).

The predicting equation (6.3) is given below. Table 6-3 shows the standard error of estimate, based on equation (6.3), for each tunnel.

 $Ln S_{E} = 0.4094$ (the variables between the square brackets)

Table 6-3

RATE OF ADVANCE PREDICTION ERROR OF ESTIMATE

Tunnel System	Contract	Tunnel Number	Standard Error Relative to Equation 6.3
BART	1M0031 1M0031 1R0053 1S0011 1S0011 1S0011 1S0011 1S051A 1S051A	MR ML RR/RL TR TL SR SL SR SL	.277 .204 .358 .429 .587 .279 .493 .305
Chicago	68-404-2S 68-405-2S 68-406-2S	USC #1 USC #2 USC #3	.218 .159 .041
WMATA	1F0012 1F0012 1F0012 1F0012 1F0021 1F0021 1F0021 1F0021 1D0091	F1B No. Out F1B No. In F1B So. Out F1B So. In F2A Out F2A In F2A B.R. Out F2A B.R. In D9 So. In	.242 .452 .232 .177 .279 .293 .253 .257

Average 0.270

Amount of variability removed by predicting equation

71.8%

The errors are logarithmically distributed. USC #3 is not in the log normal distribution; without USC #3, the Mean = 0.297.

Some interesting observations may be made relative to the effect of certain correction factors.

Equation (6.3) suggests that soils effects on the RoA, from greatest impediment to greatest ease of progress, would be: cemented ground, sand and gravel, running ground, cobbles and boulders, silt, clay and sand mixes, cohesive ground. Logic doesn't support the above order. The cobbles and boulders should be a higher order and probably resulted in its position (and exponent) due to interactions with more favorable conditions in the few data sets in which they appeared. Statistically, considering the numerical values of the derived exponents and their individual errors of estimate, the first three soils are different from the last three, but in the two groups of three there is not much difference.

The RoA is increased with increasing jacking potential and decreased with increasing diameter of the shield.

The last week of tunneling is inefficient relative to the RoA.

There are correlation interactions between the various down times as well as the equipment in use. Table 6-3 shows the standard error of estimate by individual tunnels.

6.4 TOTAL DOWNTIME EQUATION

Total downtime per foot of mining was not a good prediction — the event appears to be too random. Reliability theory suggests that a U-shaped curve, Figure 5-4, should describe the events with time, and the regression, equation (6.4), was done in that form. However, because of the poor fit of the equation, it is suggested that the average downtimes, hr/ft, may be used. For all equipment failures, the averages are shown in Table 6-4.

(TOTAL DOWN HOURS + 0.001)/Ft = 4.5054 x 10^{-3} Exp[-5.0536 x 10^{-5} * (Σ Ft) - 1.3573 x 10^{-7} *

 $(\Sigma Ft)^2 + 2.1773 \times 10^{-11} * (\Sigma Ft)^3 + 0.85647 * (Silt and Clay: 1 \rightarrow 2) + 0.67523 *$

(Clay and Sand: $1 \rightarrow 2$) + 0.82934 * (Sand and Gravel: $1 \rightarrow 2$) + 0.30376 *

(Cobbles and Boulders: $1 \rightarrow 2$) - 1.27427 * (Cohesive Ground: $1 \rightarrow 2$) + 1.28616 x 10^{-3} *

(Total Jacking Potential of Shield - Tons) - 0.18252 * (OD Shield - Ft) + 2.66974 *

(Shield and Cutting Wheel: ½) + 0.80838 * (Shield and Digger Arm: ½) - 1.46578 *

(Conveyor Belt and Train: ½) - 0.39557 * (Rubber Tired Truck: ½)];

$$R^2 = 0.174$$
, $Ln S_v = 1.9563$ (6.4)

Table 6-4

AVERAGE DOWNTIME - HR/FT

Category	Average Hr/Ft Down	Standard Deviation	σ/μ *
Total Hours	0.1720	0.3718	2.16
Shield	0.0249	0.0878	3.53
Excavating Equipment	0.0440	0.2410	5.48
Conveyor	0.0113	0.0404	3.04
Muck and Other Transportation	0.0166	0.0789	4.75
Miscellaneous	0.0697	0.1459	3.53
Administrative	0.0089	0.0400	4.49

^{*}The coefficient is a relative measure of the variability of the data about the mean. A satisfactory value, for nominal use, would be less than 0.5.

A further investigation into the total down hours is shown in Figure 6-2. The plot between cumulative total down hours and cumulative feet of tunnel suggests a relationship that could be developed and would involve the cumulative history of soils penetrated, and the equipment types in use, as well as the shield diameter and jacking potential in $tons/ft^2$.

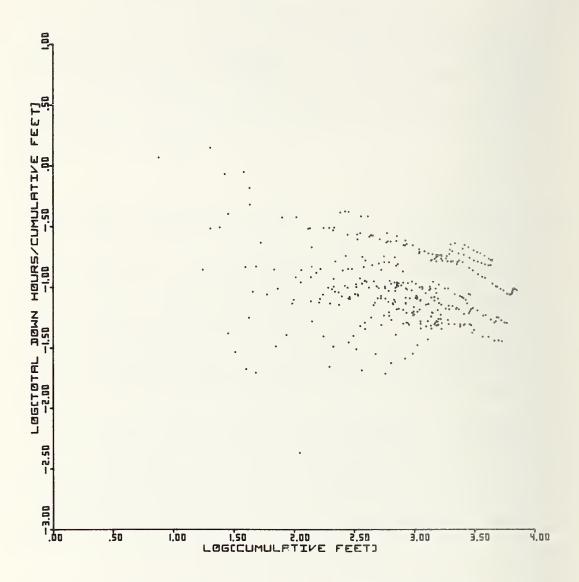


Figure 6-2. Total Downtime as Related to Cumulative Feet of Tunneling

6.5 OTHER DOWN HOURS

The "other equipment down hours" were investigated plotwise and are shown merely to display their potential as a means for prediction.

Figure 6-3 shows the downtime for the excavating cutting wheel used on the Chicago USC No. 1 tunnel.

Figures 6-4, 5(a), 5(b), 6 and 7 indicate the cumulative downtime hours vs cumulative tunneling feet for the shield, excavating equipment, miscellaneous, and administrative down hours.

Statistical analysis of these data would likely develop usable predicting equations except for predicting the shield and administrative down hours. These events appear to be completely random.

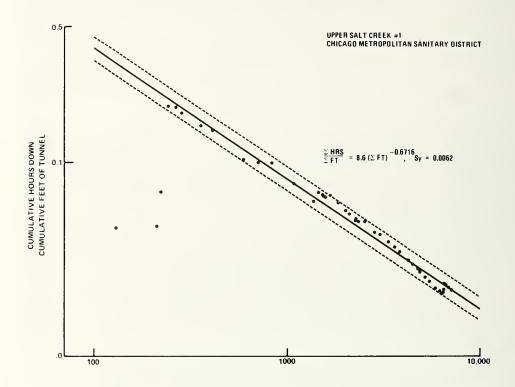
The conclusion that may be drawn from Figures 6-2 to 6-7 is that

- There appears to be a linear relation between down hours and cumulative distance of tunneling (time) for total down hours, excavating equipment, and miscellaneous hours. Statistical analysis of the data would be expected to result in a useful predicting equation,
- The shield and administrative down hours appear to be random events not correlated with tunneling distance (time). Under these circumstances, the mean and standard deviation of downtime (Table 6-4) is a satisfactory means of estimation.

The disadvantage of using a mean downtime for equipment that shows wearout characteristics is that:

- Short tunnels will be overstated for downtime
- Long tunnels will show too much downtime at the beginning and insufficient downtime at the end.

The argument for further analysis is pervasive.



Cumulative Feet of Tunnel

Figure 6-3. Excavating Cutting Wheel Downtime for USC No. 1

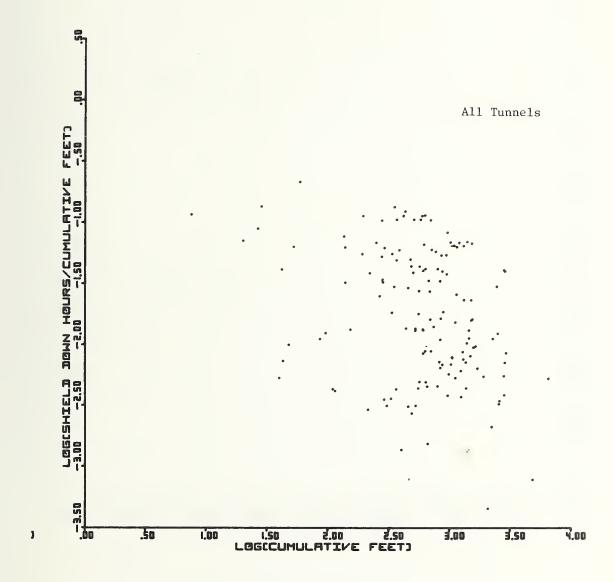


Figure 6-4. Shield Downtime

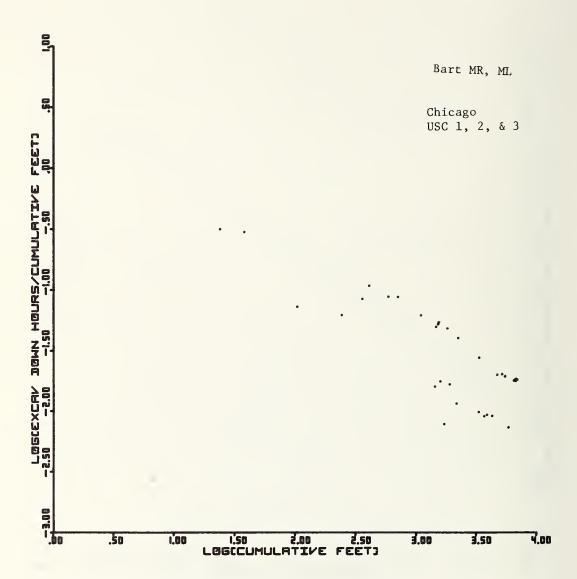


Figure 6-5A. Rotating Cutting Wheel Downtime

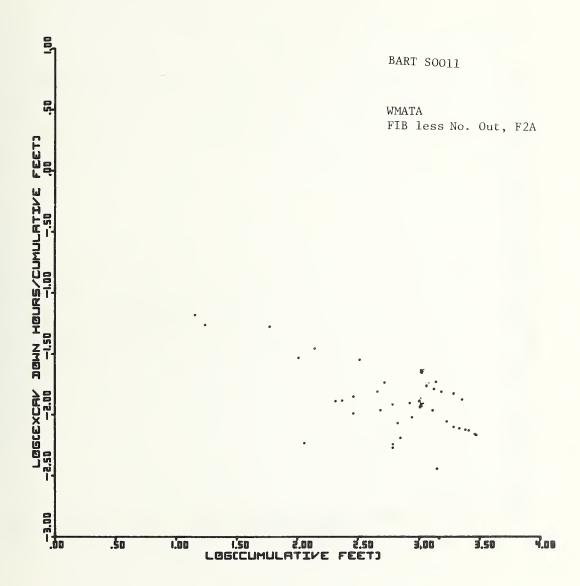


Figure 6-5B. Digger Arm Downtime

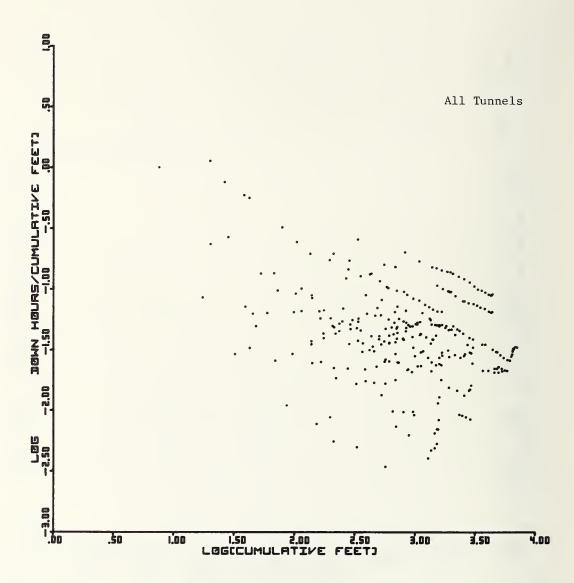


Figure 6-6. Miscellaneous Downtime

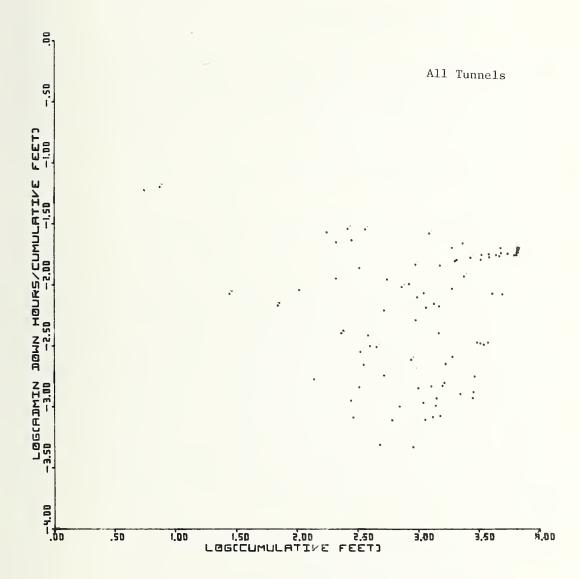


Figure 6-7. Administrative Downtime



7. INSTITUTIONAL EFFECTS

Institutional effects are those factors, usually subjective, that are applied as multipliers to the direct labor costs to allow for identified parameters with unknown or partially known ranges of variability. In the categories of

- Risk an action with a known set of outcomes and each outcome occurring with a known probability distribution; and
- Uncertainty an action with a known set of outcomes, but each outcome occurs without a known probability distribution

institutional effects fall into the classification of uncertainty. In order to reduce some of the uncertainty, a number of questions were asked of tunneling contractors relative to the effects of various institutional factors. The results of the analysis of the questionnaire answers have been incorporated into a guideline for planners' use for determining the factors' impact on costs. The factors examined were those deemed most significant in their effect on project costs. Discussions with transit system owners and tunneling contractors by Bechtel's consultant, J.M. Keating, as well as Bechtel's own estimating staff, led to the following selection of eleven major institutional factors.

 Availability and Analysis of Subsurface Geological Conditions

This factor covers the extent to which the Owner-engineer has collected, evaluated, and disseminated subsurface information to the contractor prior to the contractor's bid preparation. Included in this information would be any geological interpretations obtained by the Owner-engineer.

2. The Extent of Owner Disclaimers with Regard to Subsurface Information Provided to the Contractors

3. Flexibility of Engineering Specifications

Flexibility refers to the degree to which the engineering specifications allow for design changes suggested by the contractors to accommodate the selected construction method.

4. Quality of Engineering Specifications

Quality refers to the accuracy of the Owner-engineer design including assumptions on which the design and specifications are based.

5.A Owner-obtained Rights-of-way

Rights-of-way include arrangements with all Owners of property, including utilities that must be relocated. Rights-of-way are also construed to include areas needed by the contractor as work and storage areas, including any rights-of-way needed for muck disposal.

5.B Owner-obtained Construction and Entry Permits

These include permanent and temporary construction permits and entry permits where required.

6. Potential Contractor Liability

Liability here is used to include only the contractor liability related to changed conditions.

7. Labor Agreements

The existence of systemwide labor agreements.

8. Labor Union History in the Area

Included in the history are work practices, craft availability, work stoppages, jurisdictional disputes, and union management relations.

9. Owner Payment and Retention Periods

10. Owner History of Claims Settlements on Past Projects

7.1 DATA COLLECTION AND ANALYSIS

The impact of institutional factors on tunneling costs, for the most part, has a twofold effect. First, there are what we have chosen to call the <u>identifiable costs</u>. These represent, for example, estimated expenditures incurred by the contractor to:

- Collect and evaluate subsurface data where none is provided by the Owner,
- Obtain rights-of-way and construction permits not obtained by the Owner, and
- Cover added financing costs where owner payment periods are excessive or retention amounts excessive.

The second effect of the institutional factors is on contingency costs included by the contractor at the time of bid to cover expenditures that are "likely" to occur during the tunnel drive, but which cannot be quantified at the time of the estimate. Contingency costs are directly related to the risks incurred by the contractor. The greater the risk burden, the greater the contingency costs. This second impact, the impact on contingency costs, is by far the greater of the two and also less visible to the owner.

7.2 DATA

Since current industry practices do not require sufficient detailing of contractor bids to identify contingency costs, an alternate approach was taken to obtain data from which to evaluate institutional cost factors. The questionnaire discussed in paragraph 7.7 was sent to 25 softground tunneling contractors through Bechtel's consultant, to determine the impact of each of the institutional factors on contingency. Since contingency costs are a measure of the contractor's risk and risk is theoretically related to profit, the questionnaire also included several questions relating to profit. Profit, in this case, can be

construed to mean gross margin. Of the 25 questionnaires sent out, 12 were returned; 2 of the responses were rejected because of incompleteness. The questionnaire established a base project; twin 3,000-lineal-feet tunnels from a common work shaft through standing soil, primary liners of segmented steel, and the drive assumed through free air with wrap-up insurance provided by the Owner. The contractor's labor costs were assumed to be 50 percent of his total costs before contingency and profit.

7.3 ANALYSIS AND FINDINGS

The questionnaire asked each contractor to evaluate the relative contribution of each of the eleven factors to the contingency he would apply to his estimate under the best and worst circumstances associated with each factor. He was also asked to express, as a percentage of his base labor package, the total contingency and total profit that would be included in his bid price under the best and worst circumstances. It should be noted that the best and worst cases are unlikely to occur but were included here as upper and lower boundaries.

Each respondent was asked to add to the list of factors if he chose to do so; two did.

As expected, the responses showed a wide range of variation. Part of the variation is obviously attributable to differing interpretations of the questions.

Table 7-1 illustrates the spread in responses to the questions regarding contingency and profit amounts. The median value is that for which half the responses are lower or higher. From the contractor's point of view, in the worst case, where the majority of risks must be shouldered, contingency could be an amount equal to his total labor bill.

As classically interpreted, potential profits should increase as the contractor's risk increases. This is illustrated in Figure 7-1 where contingency is plotted on the horizontal scale and contingency and profit on the vertical. The contingency figures from the questionnaires represent the contractor's evaluation of relative uncertainty.

The "best" and "worst" case responses were analyzed by arranging them into frequency distributions. For the best case, the 10% to 90% frequency spread covered the range of 0% to 24% contingency; for the worst case, the 10% to 90% spread covered 19% to 96% contingency. As shown in Figure 7-1, there is a small overlap in what is considered best and worst. In fact, the graph could be interpreted as a continuum of responses representing profit and contingency as a function of the contractor's uncertainty (contingency).

The center curve (in the two fan-shaped projections) is bounded by an upper and lower limit, and this range of uncertainty contains the area into which approximately 70 percent of responses would be expected to fall.

When the contingency is removed from the Profit and Contingency, it can be seen that, in both the expected values of the best and worst cases, profit reaches a maximum and then decreases; in the best case, it is at approximately 10 percent contingency, and, in the worst case, it is at approximately 70 percent contingency. It could be surmised that the profit percentage represents the contractor's minimum expected profits and the contingency plus profit percentages his maximum expected profit.

No inferences should be drawn concerning the justification of these maximum profit levels. It only indicates that owners can significantly reduce tunneling costs by minimizing the monetary risks to be assumed by the contractor and thereby reducing the applied contingencies.

Table 7-1

HIGH-LOW RANGE OF RESPONSES

CONTINGENCY AND PROFIT ASSIGNED AS A PERCENT OF LABOR

	Best Case			Worst Case		
	Lowest Median Highest			Lowest	Median	Highest
Contingency Profit Profit + Contingency	$\begin{array}{c} 0\\ \frac{10}{10} \end{array}$	6 29 35	25 40 65	15 20 35	40 51 91	100 100 200

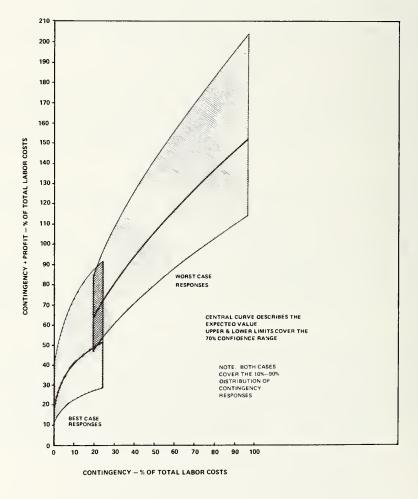


Figure 7-1. The Change in Profit Plus Contingency With Changes in Contingency

7.4 INSTITUTIONAL FACTORS IMPACT ON CONTINGENCY

The impact of the various institutional factors on contingency varied significantly among contractors; the ranges and averages are shown in Figure 7-2. Table 7-2 lists the factors by <u>best</u> and <u>worst</u>, and the median response of all contractors sampled. Availability of subsurface information in both cases is the highest contingency factor. The Owner's history of claims settlement and the labor union history account for the next largest amounts.

Figure 7-3 is a plot of the average contractor responses to the best and worst cases for each factor, in descending order, and indicates the cost differentials between the best and worst conditions.

Under usual contracting conditions, institutional factors do not generally fall completely into "best" and "worst" classes; statistically, this is a highly unlikely condition. There will more likely be a mixture of the two. In order to examine this aspect, the data for the two cases were combined and analyzed. Table 7-3 shows the result of the combination. The mean is the arithmetic average and the median divides the data into halves. The 10 percent and 90 percent points cover the statistical range into which 80 percent of the data are most likely to fall.

The spread between the mean and the median is a rough measure of the degree to which the distribution is skewed. The sign of the difference between the (Median-Mean) indicates the direction of the skewness; a negative sign means the distribution is skewed to the higher side. For instance, it is believed that it is more likely to require a greater contingency for subsurface geology information than less (Question No. 1).

Table 7-1 can now be added to recognize the variability of the data and to consider the responses as a total distribution.

Note that only the median values are added arithmetically. The 10 percent and 90 percent points are by the root-mean-square $-(\sqrt{10\%^2+90\%^2})$.

Table 7-2

AVERAGE UNCERTAINTY EFFECTS ON CONTINGENCY

Unce	rtainty Items	Percent	Contribution Best Case	ns to Contingency Worst Case
1.	The availability and analysis on subsurface geological conditions		2.5	15.7
2.	Extent of Owner disclaimer with r to subsurface conditions	egard	0.7	5.4
3.	Flexibility of engineering specif	ications	0.6	3.1
4.	Quality of engineering specificat	ions	0.6	3.3
5.	Owner obtained rights-of-way		0.2	2.0
6.	Owner obtained permits for constrand entry	uction	0.1	1.5
7.	Liability		0.6	3.8
8.	Labor agreements		0.7	2.8
9.	Labor union history in area		1.1	4.9
10.	Owner retention period		0.3	0.4
11.	Owner history of claims settlemen	.t	0.6	4.0
12.	Mobilization payments			
13.	Scheduling problems		0.4	1.7
14.	Weather			
15.	Proximity to water			
	Average Total Contingency as a Percentage of Total Labor Costs		8.4	48.6
	Median Total Contingency as a Percentage of Total Labor Costs		6.0	40.0

INSTITUTIONAL FACTOR		PERCENT OF DIRECT LABOR COSTS 5 10 15 20 25 30
1. AVAILABILITY AND ANALYSIS OF SUBSURFACE CONDITIONING	BEST WORST	
2. OWNER HISTORY OF CLAIMS SETTLEMENT	BEST WORST	111111111111
3. LABOR UNION HISTORY IN THE AREA	BEST WORST	01111111 9 11111111
4. EXTENT OF OWNER DISCLAIMERS WITH REGARD TO SUBSURFACE CONDITIONS AND ANALYSIS	BEST WORST	
5. LABOR AGREEMENTS	BEST WORST	**************************************
6. LIABILITY	BEST WORST	Mar. 11101111 ♥ 11111111111
7. QUALITY OF ENGR. SPECS.	BEST WORST	da 111111
8. FLEXIBILITY OF ENGR. SPECS.	BEST WORST	A
9. OWNER OBTAINEO RIGHTS-OF-WAY	BEST WORST	•
10.0WNER OBTAINEO PERMITS FOR CONSTRUCTION AND ENTRY	BEST WORST	inding:
11.0WNER RETENTION Perioos	BEST WORST	10111111
12.OTHER FACTORS	BEST WORST	11.01.11.11.11

AVERAGE OF RESPONSES

Figure 7-2. Impact on Contingency Measured as a Percentage of Direct Labor Cost

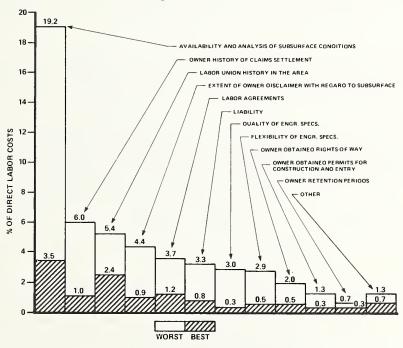


Figure 7-3. Risk Components of Contingency Under Best and Worst Cases

This again indicates to the user that extreme values are not very likely to occur.

In use, Table 7-2 would be modified by using the data from Table 7-3 (or a modification to suit the user) and Table 7-4. Medians of Table 7-3 and the contingency of Table 7-4 would be multiplied and the 10-percent and 90-percent points combined, by propagation of error, to obtain the individual contingencies as a percentage of total labor costs.

7.5 CONTINGENCY SIMULATION

To integrate the contingency information collected by the sample, three stochastic simulations were carried out, using a Monte Carlo technique; one for the average case and another for both the best and worst cases. Figure 7-4 depicts the results of this simulation. The curves representing the best and worst cases are highly unlikely and are included here for reference.

The interpretation of the lines is as follows: under the best conditions, 50 percent of the contractors will include contingency values greater than 35 percent of direct labor. Similarly, under best conditions:

- 85% will have contingency values greater than 11% of direct labor
- 70% will have contingency values greater than 18% of direct labor
- 50% will have contingency values greater than 33% of direct labor
- 30% will have contingency values greater than 51% of direct labor
- 15% will have contingency values greater than 68% of direct labor.

Similar figures can be extracted for the average and worse cases from Figure 7-4.

As a starting point, planners may find the following work sheet, Figure 7-5, useful in evaluating the impact order-of-magnitude of these institutional factors on contingency. Numerical values are based on the average values calculated from the questionnaire sample.

Table 7-3

DISTRIBUTION OF CONTINGENCY RESPONSES-BEST AND WORST CASES COMBINED

Question Number		10%	Mean	Median (50%)	90%
1. Soils	_	8.5	30.9	29.0	56
2. Soils	Disclaimer	- 6	8.4	7.0	27.5
3. Engine	ering Specs.	0	6.6	5.5	15
4. Spec. (Quality	0.5	7.0	4.0	20
5. Right-	of-Way	0	3.1	3.0	8
6. Permit	5	0	2.3	1.5	6
7. Liabil:	ity	0	7.8	8.0	16
8. Labor	Agreements	0.5	7.2	7.5	14
9. Labor 1	History	1	11.4	9.5	23
10. Retent:	ion	0	2.1	1.0	7
ll. Claim	Settlement	1	7.6	7.5	15
Mobilizatio	on	0	1.6	0	7.5

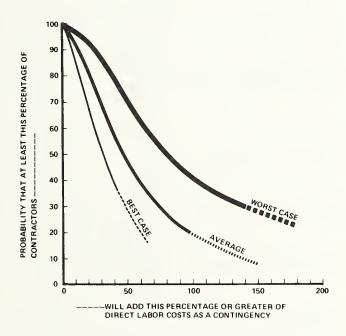


Figure 7-4. Contingency Level Probabilities

Table 7-4

CONTINGENCY AND PROFIT ASSIGNED AS A PERCENTAGE OF DIRECT LABOR-BEST AND WORST CASES COMBINED

	10%	Mean	Median (50%)	90%
Contingency Profit	1 17.5	28.5 40.5	21 37.5	61 71
TOTAL	17.5		58.5	93.6

Soft Ground Tunneling

IMPACT OF INSTITUTIONAL FACTORS ON COST CONTINGENCY

V CHECK LIST

	FACTORS	IF	ADD	CONTINGENCY— PERCENT (%) OF DIRECT LABOR	
1.	AVAILABILITY AND ANALYSIS OF SUBSURFACE GEOLOGICAL CONDITIONS	NONE MARGINAL ADEQUATE GOOD		31.0 16.5 8.5 5.0	
		EXCELLENT		1.0 _	
2.	EXTENT OF OWNER DISCLAIMERS WITH REGARD	EXTENSIVE	-	8.0	
	TD SUBSURFACE CONDITIONS	NOMINAL		2.5	
		FEW			
3.	FLEXIBILITY OF ENGINEERING SPECIFICATIONS	RIGID		3.0	
		ADEQUATE		1.5	
		FLEXIBLE		0.5 _	
4.	QUALITY OF ENGINEERING SPECIFICATIONS	MARGINAL		3.0	
		SATISFACTORY EXCELLENT		1.5 0 _	
_			-		
5.	DWNER OSTAINEO RIGHTS-DF-WAY, ENTRY PERMITS AND CONSTRUCTION PERMITS			5.5	
	AND CONSTRUCTION PERMITS	MAJOR ONES ALL		1.5 0 _	
6	LIABILITY	EXTENSIVE		5.5	
٥.	LINGILITI	NOMINAL		2.5	
		MINIMAL		0 _	
7.	SYSTEM WIDE LABOR AGREEMENTS	NO		7.0	
		YES		, 0.5	
8.	LABOR UNION HISTORY IN THE AREA	POOR		7.0	
		MARGINAL		5.5	
		AVERAGE		4.5	
		G000		1.5	
		EXCELLENT		1.0	
9.	DWNER RETENTION PERIOD	LONGER THAN AVERAGE		2.5	
		AVERAGE		0.5	
		SHORTER THAN AVERAGE		Ö	
10.	DWNER HISTORY OF CLAIMS SETTLEMENT	POOR		12.0	
		MARGINAL		5.5	
		AVERAGE		1.5	
		G000		1.0	
		EXCELLENT		0.5	

Figure 7-5. Impact of Institutional Factors on Cost Contingency

7.6 AREA PRODUCTIVITY

The concept that productivity of skilled and unskilled craft workers varies in different geographical areas of the U.S. is generally accepted as a subjective variable. The quantification of this subjectivity is another matter and, at the present stage of knowledge, is not well established.

From proprietary sources, it is estimated, based on a value of 1.0 for the West Coast, that manhour requirements for other areas of the U.S. would have multipliers of

- 1.1 for the Midwest
- 1.15 for the East Coast (excluding New York City) and Southeast $\,$
- 1.2 for the Gulf Coast

based on 1972 data.

In general, the multiplier is skewed to the high side (less productive) rather than the low side. When a range of values is to be considered, the expected value +0.5, -0.3 can be considered a range into which, by chance, 20 percent of the productivity values will fall; e.g.

For the East Coast:
$$1.15 + 0.5 = 1.65$$

 $1.15 - 0.3 = 0.85$

7.7 TUNNELING QUESTIONNAIRE

As explained earlier in this section, data had to be gathered by direct contact with major contractors, since usual breakdowns of bid figures did not provide adequate insight into the built-up estimates for our purposes. The following letter was dispatched to some 25 tunneling specialists late in December 1976.

"We are working on a D.O.T. study evaluating the cost of soft ground tunneling.

"This report is being prepared by Bechtel Corporation and basically has involved gathering statistical data from job reports in North America. The information gathered to date shows a good correlation at the direct cost level when adjusted for regional variations.

"In the areas of contingency and profit, we would like your assistance and have included a questionnaire that we hope you will take the time to fill out.

"The questionnaire is being sent to twenty-five men in the tunneling business and your response will be anonymous and tabulated to develop ranges for contingency and profit.

"The format is laid out in such a way as to reflect the extra cost of construction if the contractor is saddled with the unknown and owner-engineer has put the burden of solving problems on the contractor.

"Please respond to both cases "best" and "worst." The "best" condition would be ideal from the contractor's standpoint; for example, no disclaimer by owner-engineer regarding data and evaluation of subsurface conditions, job labor agreement, etc. The "worst" case would be your opinion of the opposite of "ideal."

"In your evaluation you will have to make assumptions based on your experience with soft ground tunneling projects but consider the basic project as:

- A. 2 3000 LF tunnel from a common work shaft. Ground tends to stand up as steel liners are extruded from the tail of the shield.
- B. Compressed air is not required and the contractor is covered by owners wrap-up insurance.
- C. The contractor's labor package is equal to 50% of the total cost without contingency and profit.

"Thank you for your time on this questionnaire and we will send you a summary of the results."

Contingency Areas

Contribution of Risk Items

to Contingency

Working with the job conditions described, how would the "Risk Components" tabulated below change when considering the "best" and "worst" cases.

% Contribution % Contribution

"Worst"

____''Best''

. The availability and analysis on subsurface geological conditions		
. Extent of owner disclaimer with regard to subsurface conditions.		
. Flexibility of engineering specification	ıs	
. Quality of engineering specifications		
. Owner obtained right-of-way		
. Owner obtained permits for construction and entry		
. Liability		
. Labor agreements		
. Labor union history in area		
. Owner retention period		
. Owner history of claim settlement		
. Etc.		
. Etc.		
. Etc.		
Total Contingency	100%	100%
Contingency Values	_	
Working under the above two case condition contingency vary.	s how would the	percent of
As % of total labor	"Best"	''Worst''
As % of total cost		
7–15		

Profit

Α.	Working under the above two case conditi dence in estimate cost and contingency v of profit vary.		
		"Best"	"Worst"
	As % of total labor		
	As % of total cost		
В.	Same as A. with additional conditions no	ted.	
		"Best"	"Worst"
	5 or more bidders As % of total labor		
	As % of total cost		
	3 bidders As % of total labor		
	As % of total cost		
С.	Modify contracting method to target esti 25% sharing in profit or losses based on		_
		"Best"	"Worst"
	As % of total labor		
	As % of total cost		

7.8 CONCLUSION

The above data processing has been discussed with a degree of precision probably not supported by the accuracy of the data. The purpose was to indicate the statistical procedures involved. It is a first step in the reduction of uncertainty concerning institutional factors and can be used as a reflection of the concern of ten tunneling contractors.

More contractors should be concerned and contribute to reducing such uncertainty to the level of risk by contributing their subjective (and quantitative, if available) values to increase the discipline's total knowledge. It does seem unfortunate that a much higher degree of accuracy can be achieved in estimating tunneling labor and total costs, only to have this accuracy destroyed by the present high degree of uncertainty of institutional effects.



8. RECOMMENDATIONS

8.1 FUTURE DATA COLLECTION

Rapid Transit tunneling data generally have not been summarized into formats whereby the data could be used for future estimating. Reports, as such, have been in terms of funds expended. Because of the rapid rates of inflation during the last ten years, between and during tunnel construction, the extrapolation of past to future costs is deemed infeasible; there is no one inflation index that can be applied to all the resources used during construction.

In order to use past data, the actual resources consumed — manhours, equipment, and bulk materials — must be known so that current costs and expected escalation factors can be applied at the time new construction is contemplated to estimate the total cost of a finished tunnel.

Based on the above concept and in conformation with the study contract, the following are recommended as minimum information requirements to be reported on completion of future tunneling contracts subsidized by U.S. Department of Transportation funds.

8.1.1 Economic Factors in Tunnel Construction/Case History Data

The format is shown (filled out) in Appendix A-1. Sheets 1 through 5 summarize all but the weekly progress. The unnumbered pages are for weekly progress summaries and average soil characteristics.

The latter breakdown is not displayed. The characteristics used in this study resulted from the descriptions found in the tunneling logs. Better

descriptions can and should be developed by soils engineers — but must be compatible with the capability of the face crew foreman to quickly recognize and log. It must not be time-consuming, as his primary responsibility is the safe advancement of the tunnel face.

8.1.2 Ring and Face Log (Figure 8-1)

The weekly summary of tunnel progress is composed of Ring and Face Log data. The latter should contain sufficient information so that only clerical assistance is needed for compilation.

A suggested set of face description criteria are included that are mutually exclusive and in combination will give an adequate picture of the advancing face. The BART log sheet contained data for two rings per sheet, and the WMATA log had one ring per sheet.

8.2 ADDITIONAL STUDIES

The results reported upon here are based on tunnels whose data appeared to be quickly available. There may be data errors because there was not sufficient time to verify certain reported information that, upon study, raised questions of correctness. These data should be verified or corrected.

Not enough different soil types were included. Glacial till soils, to evaluate the effect of cobbles and boulders, need inclusion. The Toronto subway and Edmonton sewer systems have those soil characteristics and one or more tunnels should be added to the data deck.

All the collected data were not studied and should be analyzed to determine:

 Equipment types most applicable to expected tunneling conditions and lengths.

RING & FACE LOG

Tunnel # (OB/IB), Contract #, (Contractor, Walker:, Shifter:
Date:/	innel Pressure: psig, Weather:
Ring #, Station @ Start of Shove:	++. Time @ Start of Shove:(24 hr clock) Time @ End of Shove:
No. Muck Vehicles Filled:	Minutes:
	n:, Time @ Start of Ring Erection: psig, Time @ End of Ring Erection:
	Minutes:
ESTIMATED SOIL FACE COMPOSITION	FACE PROFILE BEFORE SHOVE
Silt:%, Clay:%, Sand:%, Gravel:%, Rocks & Boulders:%, Peat & Trash:%.	(Sketch Soil Characteristics & Location)
ESTIMATED FACE CONDITION (SCALE 0-1.0) Running:, Moderately Stable:, Stable:, Hard:, Breasting:Yes, No	
ESTIMATED WATER CONDITIONS Dry:(0), Damp:(.2), Slight Flow:(.5) Operating w/Pumps:(.75), Flooded Out:(1.)	
Shove Jacks, Show jacking pressures on profile. TARGET POSITIONS AFTER SHOVE:	
Left Right Hi Lo Front	(Note: Outside circle = 100 units. Each square = 1% of total area) Roll of Shield:
SHUTDOWNS	
Time @ Beginning:, Continuing (ck) Time @ Beginning:, Continuing (ck) Time @ Beginning:, Continuing (ck) Slowdowns, Reasons For:	
Other Comments:	
(Note crew size on first ring log of shift)	

Figure 8-1. Ring and Face Log

 Crew staffing as a function of equipment to be used and expected tunneling conditions.

Bulk material requirements must be added to the system.

Although a beginning was made in estimating the effects of institutional factors, it was only a beginning. Mailed-out questionnaires are notorious for their poor responses. Because of the gross effects these factors have on costs — which far overshadow the quantitized tunneling effort — a more detailed study needs to be made. Contractors should be interviewed because the response percentage will be increased. And more factors will be included.

Our questionnaire only went to transit tunneling contractors. All tunneling contractors, including those for large-diameter sewers, for both soft ground and hard rock should be included. The questionnaire should be expanded.

Equipment maintenance and depreciation were not readily found, but need to be included.

The derived predicting equations should be analyzed for stability of the derived coefficients. Ridge analysis (9) is one method of modifying the coefficients to achieved satisfactory stability. It was precluded in this study by the restraints of time and resources.

8.3 RISK MODEL

All the above data, including the results of the study to date together with their variances, will be useless unless they are combined in a simulation model. Not only useless, but incomprehensible.

A risk analysis model must be written to facilitate the complete use of the data $^{(10)}$ and allow the decision maker to make a rational judgment about the economics of the project.



9. GUIDELINES

Two forms are suggested for future data acquisition. Section 3.1.1 lists the data used in this study. The data are keypunched in a 7F10.5 format on the card deck forwarded separately as part of this report.

The key document on the advance rate is the Ring and Face Log. Daily perusal of the shift's logs should be made by supervisory personnel to ensure accuracy and completion. Weekly averaging of the data is highly recommended so that questions on omissions and errors can be corrected before memories of events are forgotten. To save time, the weekly averages should be posted directly to keypunch sheets. The forms used are shown in Appendix A-6.

In the following, consider each variable on the keypunch form of Appendix A-6 as XI, X2, ----, X42.

The intercept and learning curve exponents are estimated first:

- Plot X4/X2 (hr/ft) vs $X3-0.5*X2(\Sigma ft)$ on log-log paper.
- Remove obvious outliers from the immediate analysis (they will be used later).
- Regress $Ln(hr/ft) = f[Ln(\Sigma ft)]$

The estimated values are punched into the data cards as X38 and X42.

Analysis of the tunnel RoA or a larger matrix composed of many tunnels is made by -

- Obtaining correlation coefficients between all input variables,
- Eliminating variables that have no logical (engineering) basis for being included in the analysis,
- Eliminating variables having correlation coefficients greater than ± 0.9 (the analyst may have his own level for elimination). In such cases, one variable is probably adequately explaining the variation in the other,
- Eliminating variables that appear only a few times. These variables may induce an exaggerated effect. If the variable is considered to be logically important, it may be useful to examine its effect in a smaller matrix of data with other variable characteristics of a similar nature.

Based on the inter-correlation coefficients of independent variables left for consideration, new dummy variables may be constructed (see section 6.0) that will increase the explanatory value of the predicting equation.

The effect of the learning curve and intercept have been previously determined. Only the multiplier effects of soils, equipment types, and their breakdowns are to be found. The dependent variable (see Figure 5-7) is calculated by

$$Y = \frac{.X4/X2}{X38* (X3-0.5*X2)**X42} = \frac{hr/ft}{I* (\Sigma ft)^E}$$

The Ln Y is regressed against the logs of the independent variables and their dummys.

A best equation can now be selected.

The same basic procedure is followed for estimating the other prediction equations.

The best form for the downtime predictions is not yet finalized. Figure 6-2 may provide a satisfactory basis for analysis.

Figure 5-1 shows the system calculations for estimating the tunnel construction cost. As a final step, the equations are combined, together with costs and derived (as well as subjective) variabilities into a Monte Carlo simulation to estimate the expected cost and its distribution. This is known as risk analysis (10). The contractor can then bid, based on his "feel" for the degree of confidence he believes is justified. The advantage of risk analysis is that it quantifies a large portion of the unknown.



Appendix A

PHYSICAL DATA

Data included in this appendix are:

A-1	Characteristics of tunnels and equipment
A-2	Average weekly progress
A-3	Rate of advance calculations
A-4	Calculation of downtime hours
A-5	Total estimated shift hours and percentage of error
A-6	Keypunch forms



Appendix A-1

A partial record of the physical characteristics of the individual tunnel and equipment used in several tunnels.

Although it is expected that the complete history is available in the historical record files, complete information could not be located in the time available for the searches.

It is recommended that this or a similar form be used to record the pertinent history of future tunneling operations.



CASE HISTORY DATA

DESCRIPTION		B. OESIGN INFORMATION	SHEET1 OF
1. PROJECT NAME 24th to Randall St.	NUMBER /MOO3/	1. PLAN AND PROFILE ATTACHED	YES NO
1. LOCATION San Francisco, Calife	erois	2. TYPICAL SECTION DRAWING ATTACHED	YES NO
3 OWNER Bay Area Rapid Transit District	ENGINEER PIST B	3. TEMPORARY LININGS OFFAILS ATTACHED	YES NO
4 CONTRACTOR Morrison-Knudsen Coloc		4 PERMANENT LININGS DETAILS ATTACHED	YES NO
5. DATES: START May 27, 1967	COMPLETE November 17, 1969	5. GEOLOGICAL PROFILE ATTACHEO:	YES NO
6 PROJECT SCOPE (INCLUDE ANY APPURTENANT STRUCTUR	ES)	6. VERBAL DESCRIPTION OF SOIL CONDITIONS	
locludes construction tunnels of approximately the state of the line, placing wolkway concrete; constitution and switching station and mechanical and electrical was of segmented steel tuniforms.	Sas if of MR line and tunnel invert and uction of a vent shaft d a pumping station; rk, and installation	Sail consists of sandy clay to very dense; gray clay with so and gray clay, all with densit dense, plus two areas that of fractured rock. The contractured churt	ome sand; red, brown by of medium to very had a large amount
7. OWNER FURNISHED MATERIAL AND EQUIPMENT LIST	-	7. DEWATERING PLAN ATTACHED	YES ND
Scomented steel cious	numning station	8. GROUNO WATER CONDITIONS DESCRIPTION	
Segmented steel rings, equipment and ventilation D. OTHER OWNER SUPPLIED COST ITEMS (e.g. INSURANCE) Right of ways	n'equipment,	Underground water table : throughout the right-of-way so C entire tunnel length making it pos or tunnel length in compress 9 SITE PREPARATION & RESTORATION DESCRIPTION	contractor dewatered the sible to drive only 1/3

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

. OESIGN INFORMATION (CONTINUEO)	C. CONSTRUCTION METHODS	SHEET OF
	1. FREE AIR 2/3 of tunnel	LENGTH (FT) 60/8
	2 COMPRESSED AIR 1/3 of tunos	LENGTH (FT) 3007
	PSIG MIN O PSIG MAX 14	PSIG WTO AVG. 3.233
	3. DESCRIPTIONS	
10. UNDERPINNING DESCRIPTION	TUNNEL EXCAVATION	
Underpinning of the Sears store at Mission and	Excavation was with a	17.92' shield with
Army streets use accomplished by drilling	2 Full Breasting Wheel-Type 1	lining machines
caisson holes to extend about 10 ft. below the	and a conveyor system	consisting of
invert of the future tunnel. Bentonite slurry was used	and a conveyor system skiphoist and conveyor extend	ing 165 IF
to keep the holes open. Then reinforcing was lowered into the caisson holes and tremie concrete	<u> </u>	J
lowered into the eaisson holes and tremie concrete		
was placed in the slurry-filled holes. New concrete		
pile caps were constructed to support the		
existing pile caps and the building.		
11. UTILITIES. OESCRIPTION	PRIMARY LINING	
Relocation is minimal. Electric, gas and water	Composed of 30-inch wie	le 17.3-ft. outside
lines on the east side of Mission St. were	diameter circular welded steel	rings, each consisting
relocated around the end of the access shaff.	diameter circular welded steel of 6 larger segments and c	one small key
All other utilities supported in place.	segment	J
	J	
	FINAL LINING.	

CASE HISTORY DATA

D. MAJOR EQUIPMENT UTILIZ	ZED			
1. CUTTING AND EXCAVATING				
MAKE MINING &	Equipment	Yanufaci	turing (orp.
TYPE	ROTATING WHEEL	OSCILLAT	ING ARMS	DIGGING ARM
	OTHER (SPECIFY)			
CONNECTEO HORSE PO	NER 225			
NO. USEO 2				
2. SHIELO				
OUTSIDE DIA.	17.921	- -	ENGTH	12 ft. 5 in.
NO. OF JACKS 3 hour	19 THRUST	FORCE (TONS)	115 NO. OF	JACKING MOTORS 4
HORSE POWER EA. JACI	CING MOTOR 50			
NO. SHIELOS USEO	1			
3. MUCKING EQUIPMENT (UNDER	RGROUNO)			
TYPE Convey	or and 3	ki phois	st	
CONVEYOR LENGTH	165 (FT.)			1 5,400,000 lbs
RAIL CARS NO.	_ 5		CAPACIT	ry 7 cy m
RUBBER TIRE VEHICLE NO)		CAPACIT	(T)
COMBINATION (SPECIFY)				
4. MUCKING EQUIPMENT UNDER	GROUND TO SURFACE	(OESCRIBE)		
A skip hoist	extending for	om a sc	imp 15A	below the
base slab to an el				
surface was cree	ted An cle	ctric m	otor-pou	scred winch
at the top of the	. structure	605 US	ed to h	noist a ten-
cubic yard ski,	o from th	sump	to a	conveyor
attached to the	e hoist s	tructúr	c 25-f	7. chave
the street su	rface. The s	kipuxs	lifted up	the hoist and
tipped and emptica				

LINERS (PRE CAST)		
DESCRIPTION	CAPACITY	NO.
GROUTING		
DESCRIPTION	CAPACITY	NO.
Mayno Grout Rump - Rotor - Stator pump Kwik-Mix Cyclo Grout Mixer	ping type	_a_
Kwik-Mix Cyclo Grout Mixer	1/2 yd.	
Grout cars	1/a cyd.	
CONCRETE INVERT (AND WALKWAYS)		-
OESCRIPTION	CAPACITY	NO.
P8a Whiteman Concrete pump - 90 hp	14-1/2 cuft	_2_
5. VENTING, PUMPING, COMPRESSION, EQUIPMENT		
OESCRIPTION	CAPACITY	MO
LOW Air Compressors - 300 Hp ca.	(F3 @ 50 Psi	5

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

1 TUNNEL (II	MULTIPLE, SH	OW FOR EACH)		
LENGTH	Both tu	nnels - 9	000 L	F
INSIDE DI	a. 16'-	6"	00 /	7 '- 6"
CONFIGURA	ATION C	ircular		
NO. CROSS	OVERS, IF MULT	TIPLE		EA
TOTAL EXC	AVATION	80,8	00	CY
TUNNEL PE	ESSURE RANGE	12	PSI _ /	4 PS
2 GROUTING	(CY)			
		EST	ACT	UAL
BE HINO TE	MP. LINING		40	500
CONSOLIO	ATION (FACE)			
PREGROUT	TING			
3 PR	IMARY LIN	ING		
	OESCRIPTIO	N	OUAF	ITITY
Liner	Segmen	nts, steel	36	12
4. SE	CONDARY	LINING		
TYPE T	upc II c	ement		
NO LINERS	IF PREFABOR	PRECAST		E
OUANTITIE	S IF CAST IN PL	ACE		
	OESC RIPTIO	N	OUAF	ITITY
				(C
CONCRETE				
CONCRETE REINFORCIA	ıG			(TON

	ALKWAYS), ARCH	0114	NTITY
CONCRETE -	Invert, Type	T 653	9 (64
REBAR			(TONS
FORMS - 81	+ long Steel		IS F
STRUC STEEL	9		(TOMS
concrete	: - Walkways	_ 7	a cy
7. MAJOR UNDER	INNINGS		
	DESCRIPTION	ARE	A (S.F.)
TOTAL			
B. AIRLOCK SYST	M (IF USEO)		
MAN LOCKS			
	NUMBER	2	(EA
	LENGTH	40	(FT
	DIAMETER	6	(FT
MUO LOCK			
	NUMBER	2	(EA
	LENGTH	140	(FT
	DIAMETER	9	(FT
BULK HEAD OF	EICH	50	PSIC

	SHE	ET OF
9 APPURTENANT STR	UCTURES	
VENT AND FAN SHA	FTS	
CONSTRUCTION METH	oo Soldier I	Beam and
Laggir		
WIOTH 94 (FT	BREAUTH 27 FT	DEPTH JO FT
WALL THICKNESS	3 yt	
EXCAVATION QUANTI	TES 4900	(CY)
CONCRETE OUANTITIE	s 2200	(CY)
PUMPING STATIONS		
CONSTRUCTION METH	oo Shect Pil	es and
Internal	Support	
CONFIGURATION C	reulor Manho	le Type Struct
		8-16 (FT)
EXCAVATION QUANTI		· (CY)
CONCRETE QUANTITIE	s 130	
OTHER APPURTENA	NCES (SPECIFY)	
O E SC RIPTION	EXCAV (CY)	CONCRETE (CY)
22/th street Construction	11,706	
10. SITE PREPARATION	& RESTORATION	
OESCRIPTION	TYPE	AREA (S.F.)
CLEAR & GRUB		
REMOVAL		
RESTORATION		

Appendix A.1. (Continued)

CASE HISTORY OATA

F TYPICAL CREW SIZE	AND UT	ILIZATI	ON (1)
1. CREW - Heading	- Fro	c Ai	r
SHIFTS / DAY 3	HDURS /		,
WORKING DESIGNATION	1ST SHIFT	⊋nd SHIFT	3rd SHIFT
Shifter	1_	1	
Heading Engr	1	1	
Mole Operator	1	1	
Mole Mechanic	2	a	a
Iron Movers	2	2	a
Iron Workers	4	4	4
Hog Rod and	a	a	2
Grout Rump Oper.	1	L	1
Grout Hen	2	a	a
Locomotive Oper.	1	1	
Brakeman		1	1
Electrician	1/2	1/2	1/2
	(one	man	ding.
			3
TOTAL	18.1/2	181/2	181/2

2 CREW - Heading - C	ompra	sord	Air		3 CREW - Top Sic	ناد		
SHIFTS / DAY	HDURS /		6		SHIFTS / DAY 3	HDURS /	SHIFT	8
WORK DESIGNATION	1ST SHIFT	2 ND SHIFT	3RD SHIFT	THIET	WDRK DESIGNATION	1\$T SHIFT	2ND SHIFT	3RD SHIF
Heading Engr.	1	1_		1	General Supt	-1	-	-
Shifter	L	_1_	1_		Walker	1	1	
Yole Lead Mechanic			1	1	Surveyor	3		_
Mechanic	1			L	Mechanic Foreman	1	i	1
Mole Operator	1			1	Mechanic	4	1	1
Iron Worker	4	4	4	4	Electrical Fareman	1		-
Iran Mayer Hog Rod and Bracket Man	2	2	2	2	Electrician	3	- 1	1
Bracket Man	_ಎ_	_ಎ_	2	2	Top Laborer	2	a	a
amut Rump Operator			1	1	Bridge Crane	_ 1	- 1	1
Grout Man	2	2	2	2	Lube Engineer	_1_		-
Locomotive Oper	L_		1	1	Gen'l Operator	i	t	1
Brakeman	1	. 1.	1	1	Compressor Ope.	1	- 1	1_
Electrician	1/2	1/2	1/2	1/2	Compressor Opr. Change House Attendant	1	-1	1
balack Operator	1		1		Warehouseman	2	~	-
outside Muck-		1	1	1				
nside Muck- lock Operator	1	1_		1				
						-		
TOTAL	21-110	21-1/2	21.1/2	21- 1/2	TOTAL	23	10	10

	EE1	_ 05	
4_CREW - Invert	Con	crete	
SHIFTS / DAY	HOURS /	SHIFT	8
WDRK DESIGNATION	1ST SHIFT	2ND SHIFT	3RD Shift
Foreman	1		
Winch Operator			
Vibrator Men	a		
Cement Finishers	3		
Rebar Man			
Laborers	2		
Final Clean-up -	4		
Aumo-Laborer			
Operator at Plump			
,			
TOTAL	16		
5. Crew-Prep. and	For	n Sc	Hing
SHIFTS DAY !	HR3 =	н≀€Т	8
Foreman	1		
Laborers	18		
repairis for	9		
7			
TOTAL	28		

SHEET __5__ OF ___

11) NOTE CATEGORY OF CREWS HEADING, SUPPORT SURFACE SHAFT ETC.) REPORT AS LOGGEO

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

A DESCRIPTION	
1 PROJECT NAME Berkeley- Morth	NUMBER 1R0053
2 LOCATION Berkeley, California	
3 OWNERBay Area Rapid Transit District	ENGINEER PBTB
4 CONTRACTOR Shea-Macco	
5 DATES START // 27/66	CDMPLETE 3/5/68
6 PROJECT SCOPE (INCLUDE ANY APPURTENANT STRUCTUR	ES)
Approximately 1,475 feet of	curved twin subway
line tunnels, Approximately 27	100 feet of cut-and-cover
twin box subway structure, i	including installation of
mechanical and electrical equ	vipment and the
relocation and construct	ion of utilities.
and the second s	
7 DWNER FURNISHER MAREGIAL AND EDUIPMENT LIST	
Swier turnsned tunnel lining outside diameter circular weld	of 30 inches wide, 18-ft
foutside diameter circular weld	ed steel rings, pumping
8 OTHER DWNER SUPPLIED COST ITEMS (P. g. INSURANCE)	
	1

B DESIGN INFORMATION	SHEET_	1	OF	
1 PLAN AND PROFILE ATTACHED		YES	NO	
2 TYPICAL SECTION DRAWING ATTACHED.		YES	NO	
3 TEMPORARY LININGS DETAILS ATTACHED		YES	NO	
4 PERMANENT LININGS DETAILS ATTACHED		YES	NO	
5 GEOLDGICAL PROFILE ATTACHED		YES	NO	
6 VERBAL DESCRIPTION OF SOIL CONDITIONS Interfingering Lea	13e5 al	: de	iue c	
gravel, sandy and silty clays, and clay	su ac	si.If	7 201	ods
Layers are of irregular thickness and g	rade i	a ta	eac	h
other within short distances, both hori	zonta	114	and	
vertically olive gray sandstane was	cncor	wite	red	'
in the invert of the tunnel, weathered	1 +0 0	Lic	ht	
brown at the upper soil contact and	unc	leci	ain	
by a dark olive green shale.				
J				
7 DEWATERING PLAN ATTACHED		YES	NO	
B GROUND WATER CONDITIONS DESCRIPTION				
Before dewatering, the water level was 10 ft	. about	the	e top	of
the future structure. No denotering systemi execuation. Submersible Sweck pump was	placed	in	tunn	re4
invert at heading and was in all cases	SUP	احزحا	nt	
9 SITE PREPARATION & RESTORATION DESCRIPTION				

Approximately 150-ft wide area above future cut-and cover area was available as a work area. Owner provided a lot about 55 ft wide and 280ft long to

Contractor for use during construction. Temporary

CASE HISTORY DATA

B DESIGN INFORMATION (CONTINUED)	C. CONSTRUCTION METHODS	SHEET 2 OF
work area on the adjacent contract (ROOST) was used	1. FREE AIR:	LENGTH (FT) 4, 1
c a saw yard until contract 10057 was bid, mid-1968	2. COMPRESSED AIR. not used	LENGTH (FT)
J	PSIG MIN PSIG MAX	PSIG WTD AVG
	3. DESCRIPTIONS	
10. UNDERPINNING DESCRIPTION	TUNNEL EXCAVATION	
	Exequation was with an	18 ft 8/2 in shield
	A rubber-tired truck transp	
	from the heading to the Te	monrary Access St
	After the last mucking run	the mucker brow
	in a set of ring segmen	to for the next
	ring. The tunnel was	
	J	
11. UTILITIES. DESCRIPTION	PRIMARY LINING	
	30" wide, 18.0 ft outside dia	
	steel rings each consisting	a of 6 larger
	segments and one small	key scament
		3 0
	FINAL LINING	
	Invert was especiate with a	
	aggregate size Walking con	recte used a l-in
	maximum aggregate size.	

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

MAKE			
MOOEL			
TYPE.	ROTATING WHEEL	OSCILLATING ARMS	DIGGING ARM
	OTHER (SPECIFY)	loguel Diggia	
CONNECTEO H	DRSE POWER	lanual Diggine	j
NO USED			
SHIELO			
OUTSIDE DIA.	18ft 81/2 in	LENGTH	13'6" - 11'6
NO. OF JACKS		ORCE (TONS) 100/ NO O	F JACKING MOTORS 4
HORSE POWER	EA. JACKING MOTOR 20		1.1
NO. SHIELOS L		, , , , , , , , , , , , , , , , , , ,	
MUCKING EQUIPMENT	(UNOERGROUNO)		
TYPE: Dies	el Powered Mu	cker	
CONVEYOR LE		CAPACI	TY (1
RAIL CARS	NO.	CAPACI	TY (
AUGUER TIRE VE	HICLENO. LEL 714 M	odel CAPACI	TY 22,000 Lbs (
COMBINATION (S	PECIFY)		
MUCKING EDUIPMENT	UNDERGROUND TO SURFACE (DESCRIBE)	
-			
			

	SHEET	3 OF
5. OTHER MATERIAL HANDLING EQUIPMENT (SPECIFY) SURFACE TO HEA	OING	
LINERS (PRE CAST)		
OESCRIPTION	CAPACITY	NO.
Gardner Denver Air Hoist - Model 86-24	201	
Impact Wrenches		
GROUTING	-	
DESCRIPTION	CAPACITY	NO.
Moyno grout pumps	22 Hp	2
Grout Plant for Cement	,	
Grout Mixer (First tunk only) 1000 Wes plaster mortar mixer with air motor	f	
plaster morfar mixer with vair motor		
CONCRETE INVERT (AND WALKWAYS)		
DESCRIPTION	CAPACITY	NO.
Belterete Swinger conveyor system		
VENTING, PUMPING, COMPRESSION, EQUIPMENT		
DESCRIPTION	CAPACITY	NO.
Jou Air Fan for Ventilation	50 Hp	
Joy Air Fan for Ventilation Gardner Denver compressor	185 Hp 1/ 500 Cfm	2

CASE HISTORY DATA

1. TUNNEL (IF MULTIPLE, SH	ACCESS SHAFT)		_
LENGTH	2,903		F T
			_
	reular	- 0	-
NO. CROSS OVERS, IF MUL			A
TOTAL EXCAVATION			CY
TUNNEL PRESSURE RANG			PS
	· 0	PSI O	Ρ\$
2. GROUTING (CY)		r	_
	EST	ACTUAL	_
BEHINO TEMP. LINING			
CONSOLIOATION (FACE)			_
PREGROUTING			
3. PRIMARY LININ	G		
OESCRIPTIO	ON	OUANTITY	
Lielded Steel Ric	ngs-Circular	580	
4. FINAL LINING			_
TYPE Concrete			
NO. LINERS IF PREFABOR	PRECAST		EΑ
OUANTITIES IF CAST-IN-PL	ACE		
DESCRIPTIO	QUANTITY		
CONCRETE			ÇY
CONCRETE			
REINFORCING		110	N:
			NS F
REINFORCING			

DESCRIPTION	QUANTITY
CONCRETE - Invert	ICT: 1080
REBAR	(TON:
FORMS	IS.F
STRUC. STEEL,	(TON:
Walkways RR: 299 Cy	RL: 285 C4
Cross-Possoge	74 64
7. MAJOR UNDERPINNINGS	J
OESCRIPTION	AREA (S.F.)
TOTAL	l
8. AIRLOCK SYSTEM (IF USEO)	
MAN LOCKS	
NUMBER	(EA
LENGTH	(FT
DIAMETER	(FT
MUO LOCK	
NUMBER	(E.A
LENGTH	(FT
DIAMETER	IF1
BULK HEAO OESIGN	PSIG

		SHI	EET 4	OF
9 APPURTENANT STRU	CTURES			
T EMPORARY	ACCESS	SHAFT		
CONSTRUCTION METHO	0. 5010	dier pi	le and	1
Lagging wi	th tic	bars	for las	eral
support for	pile:	٥.		
WIOTH 45 (FT)	8REAOTH	150 F	ОЕРТН	FT
WALL THICKNESS				
EXCAVATION DUANTIT	ES			(C Y)
CONCRETE QUANTITIES				(CY)
PUMPING STATIONS				
CONSTRUCTION METHO	0			
CONFIGURATION				
DEPTH	(FT)	DIAMETER		(FT)
EXCAVATION QUANTIT	IES			(CY)
CONCRETE QUANTITIES				
OTHER APPURTENAN	ICES (SPECII	Y)		
DESCRIPTION	EXCA	V (CY)	CONC	RETE (CY)
10. SITE PREPARATION	& RESTORA	TION		
DESCRIPTION	T	rPE	ARI	EA (S.F.)
CLEAR & GRUB				
REMOVAL			1	
RESTORATION				

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

TIME	-1		7
luck Operator	4	4	4
hield Operator	1	1	1
Surveyor	1	1)
Shift Boss	1	1	1
WORKING DESIGNATION	1ST SHIFT	2ND SHIFT	3RD SHIFT
HIFTS/DAY 3	HOURS /	SHIFT =	8

2. CREW - Grout C	rew		
SHIFTS / DAY	HOURS /	SHIFT 8	\$
WORK DESIGNATION	1ST SHIFT	ZNO SHIFT	3RO SHIFT
Grout Foreman	1		
Grout Man	3_		
TOTAL	4		
Coulking Crew	Gray	tyard hr 3	nist
Laborer			a
TOTAL			a

3. CREW - Top and 3	haft	Crcu	ر
SHIFTS / DAY	HOURS /		
WORK DESIGNATION	1\$T SHIFT	2NO SHIFT	3RO SHIFT
Compressor Operate Forklift Operator		1	1_
Laborer	1		
TOTAL	3	1	,
Carpenter Crew	1-8	hrs	1111
Corpenter Supt.			
Carpenter Foreman	11		
Carpenter	4		
,			
,			
TOTAL	6		

SH	EET	OF	
4 CREW - Cleanup	Crei	٥	
SHIFTS / DAY	HOURS /		8
WORK DESIGNATION	1ST SHIFT	2NO SHIFT	3RO SHIFT
Shifter			
Laborer		6	
Laborer Compressor Operator Forklist			
Sperator Operator			
`			
TOTAL		9	
Concrete Crew	1-8	hr 51	1410
Shifter			
Belt Operator	1		
Swing Operator	_1_		
Swing Operator Vibrator Man	3		
Laborer	3		
Finisher	a		
TOTAL	11		

Appendix A-1.(Continued)

CASE HISTORY DATA

A. DESCRIPT	ION		B. DESIGN INFORMATION.	SHEET1_ OF
PROJECT N	AMENEW CARROLLTON ROUTE-D	.9 NUMBER 100091	1. PLAN AND PROFILE ATTACHED	YES NO
LDCATION	WASHINGTON, D.		2. TYPICAL SECTION DRAWING ATTACHED:	YES NO
3. OWNER	WHATA	ENGINEER JOSEPH K. KNOERLE	3. TEMPORARY LININGS DETAILS ATTACHED:	YES NO
4. CONTRACT	OR FRUIN- COLNON		4. PERMANENT LININGS DETAILS ATTACHED:	YES NO
5. OATES:	START /-30-75	COMPLETE 5-4-15	5. GEOLOGICAL PROFILE ATTACHEO:	YES NO
6. PROJECT SI	COPE (INCLUDE ANY APPURTENANT STRUCT	URES)	6. VERBAL DESCRIPTION OF SOIL CONDITIONS:	
DESM AFTA		CHANGED TO TOWNEC	MO STLY CLAY WITH SOM	NE CEMENTED
7. OWNER FUF	RNISHED MATERIAL AND EQUIPMENT LIST	NONE	7. OEWATERING PLAN ATTACHED	YES NO
			8. GROUND WATER CONDITIONS DESCRIPTION	
8. OTHER OWN	IER SUPPLIED COST ITEMS (e.g. INSURANCE)		9. SITE PREPARATION & RESTORATION DESCRIPTION	
-			L	

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

. DESIGN INFORMATION (CONTINUED)	C. CONSTRUCTION ME	THODS	SHEET_	2 OF
	1. FREE AIR.	YES	LENGTH (FT)	735-755
	2. COMPRESSEO AIR:		LENGTH (FT)	7
	PSIG MIN	PSIG MAX	PSIG WTO AVG.	
	3. DESCRIPTIONS	·		
10. UNDERPINNING DESCRIPTION	TUNNEL EXC	AVATION	·····	
UNDERPORT 22' x 23'-6" SEWER STENCEPHOR SEWER				
11. UTILITIES DESCRIPTION	TEMPORARY	LINING		
STANDARD WOERSTREET UTNITIES				
SUPPORTED ANDION RELOCATED - A LANGE	K/E	s & LAGGING +	GROUT	
UTICITY SAVINGS IN CONTRACT PRICE RESULTED IN CHANGING FROM DEN CUT TO TUNNES				
IN CHANGING FROM- OPEN CUT TO TUNNER				
	FINAL LINING	· · · · · · · · · · · · · · · · · · ·		
		154 CONCRETE		

CASE HISTORY DATA

5. OTHER MATERIAL HANDLING EDUIPMENT (SPECIFY) SURFACE TO HEADING

SHEET 3 OF

D. MAJOR EQUIPMENT UTILIZED

HAND EXCAVATION

1. CUTTING AND EXCAVATING

							LINERS (PR						_			
MOOEL								OE:	CRIPTION	1			CAPACI	TY	ND	
TYPE:	ROTATING	WHEEL	OSCILLATING ARMS	DIGGING	ARM											
	OTHER (SE							·					1			
													+			
CONNECTEO HORSE	POWER					_							+			
NO. USEO																
. SHIELD	<u> LG000</u>	MAYO					GROUTING									
OUTSIDE DIA.	18	1	LENGTH -	16:6	•			OE:	CRIPTION	ı			CAPAC	ITY	ND	١.
NO. OF JACKS	24	TIARUST FORC	E (TONS) 75 NO. OF JA	CKING MO	TORS	4							1			
HORSE POWER EA. J		20				-										
NO, SHIELOS USEO		, 20					*****						1	-		
	000000000000000000000000000000000000000												+			
MUCKING EQUIPMENT (UNI						-										
	CONT E		LOADER				CONCRETE	INVERT (AND WA					Т.			
CONVEYOR LENGTH	1	FT.)	CAPACITY			(11)		DE	CRIPTION				CAPAC	ITY	NO).
RAIL CARS: NO			CAPACITY			m										
AUBBER TIRE VEHICLE	NO. EIMO	2 9150	- LHO CAPACITY	50	CY	m							1			
COMBINATION (SPECIF													Î			
MUCKING EDUIPMENT UND		SURFACE IDE	SCR(RF)													
	LIGHOUND TO						6 VENTING O	UMPING COMPRES	SIDN ED	LIPMENT			1			
			0				v. venting, Pl						T			
LOADER	10 10	NNEL	YOUTAL					DE	CRIPTION				CAPAC	1114	NO	,
RELOADED	007	6 TRU	PORTAL CR FOR DISPO	SAL									-			
						\neg	7. DTHER (Spe	ecity)								
										-						
: TYPICAL CREWSIZE A	NO LITILIZAT	ION (1)	EC	CONOMI			TUNNEL CONST	RUCTION					e.	ICET I	5 05	
F. TYPICAL CREW SIZE A	NO UTILIZAT	ION (1)	2. CREW –	CONOMI				RUCTION			4,1	CREW –	SH	IEET	5 OF	
1. CREW-		ION (1)	2. CREW –		-		3. CREW -		SHIET		-	CREW -	SF			
1. CREW-	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS/DAY	HOURS 15T	2110	3RD	-	IFTS / DAY		HOURS	/ SHIFT	
1. CREW -	HOURS / SHIFT	ON (1)	2. CREW –	HOURS /	SHIFT	CASE HIS	3. CREW -	HOURS	2110	3RD SHIFT	-				/ SHIFT	3RD SHIFT
1. CREW -	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS/DAY	HOURS 15T	2110	3R0 SHIFT	-	IFTS / DAY		HOURS	/ SHIFT	
1. CREW -	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS/DAY	HOURS 15T	2110	3RD SHIFT	-	IFTS / DAY		HOURS	/ SHIFT	
1. CREW -	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS/DAY	HOURS 15T	2110	3RO SHIFT	-	IFTS / DAY		HOURS	/ SHIFT	
1. CREW -	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS/DAY	HOURS 15T	2110	3RD SHIFT	-	IFTS / DAY		HOURS	/ SHIFT	
1. CREW -	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS/DAY	HOURS 15T	2110	3RD SHIFT	-	IFTS / DAY		HOURS	/ SHIFT	
1. CREW -	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS/DAY	HOURS 15T	2110	3RD SHIFT	-	IFTS / DAY		HOURS	/ SHIFT	
1. CREW -	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS/DAY	HOURS 15T	2110	3RD SHIFT	-	IFTS / DAY		HOURS	/ SHIFT	
1. CREW – SHIFTS / DAY WORKING DESIGNATION	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS/DAY	HOURS 15T	2110	3RD SHIFT	-	IFTS / DAY		HOURS	/ SHIFT	
1. CREW -	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS/DAY	HOURS 15T	2110	3RD SHIFT	-	IFTS / DAY		HOURS	/ SHIFT	
1. CREW – SHIFTS / DAY WORKING DESIGNATION	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS/DAY	HOURS 15T	2110	3RD SHIFT	-	IFTS / DAY		HOURS	/ SHIFT	
1. CREW – SHIFTS / DAY WORKING DESIGNATION	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS / DAY	HOURS 15T	2110	3RO SHIFT	-	IFTS / DAY		HOURS	/ SHIFT	
1. CREW – SHIFTS / DAY WORKING DESIGNATION	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS / DAY	HOURS 15T	2110	3RD SHIFT	-	IFTS / DAY		HOURS	/ SHIFT	
1. CREW – SHIFTS / DAY WORKING DESIGNATION	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS / DAY	HOURS 15T	2110	3RO SHIFT	-	IFTS / DAY		HOURS	/ SHIFT	
1. CREW – SHIFTS / DAY WORKING DESIGNATION	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS / DAY	HOURS 15T	2110	3RO SHIFT	-	IFTS / DAY		HOURS	/ SHIFT	
1. CREW – SHIFTS / DAY WORKING DESIGNATION	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS / DAY	HOURS 15T	2110	3RO SHIFT	-	IFTS / DAY		HOURS	/ SHIFT	
1. CREW – SHIFTS / DAY WORKING DESIGNATION	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS / DAY	HOURS 15T	2110	3RD SHIFT	-	IFTS / DAY		HOURS	/ SHIFT	
1. CREW – SHIFTS / DAY WORKING DESIGNATION	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS / DAY	HOURS 15T	2110	JRD SHIFT	-	IFTS / DAY		HOURS	/ SHIFT	
1. CREW – SHIFTS / DAY WORKING DESIGNATION	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS / DAY	HOURS 15T	2110	3RO SMFT	-	IFTS / DAY		HOURS	/ SHIFT	
1. CREW – SHIFTS / DAY WORKING DESIGNATION	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS / DAY	HOURS 15T	2110	3RO SHIFT	-	IFTS / DAY		HOURS	/ SHIFT	
1. CREW – SHIFTS / DAY WORKING DESIGNATION	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS / DAY	HOURS 15T	2110	3RO SHIFT	-	IFTS / DAY		HOURS	/ SHIFT	
1. CREW – SHIFTS / DAY WORKING DESIGNATION	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS / DAY	HOURS 15T	2110	3RD SHIFY	-	IFTS / DAY		HOURS	/ SHIFT	
1. CREW – SHIFTS / DAY WORKING DESIGNATION	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS/DAY	HOURS 15T	2110	JRD SWIFT	-	IFTS / DAY		HOURS	/ SHIFT	
1. CREW – SHIFTS / DAY WORKING DESIGNATION	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS/DAY	HOURS 15T	2110	JRD SMIFT	-	IFTS / DAY		HOURS	/ SHIFT	
1. CREW – SHIFTS / DAY WORKING DESIGNATION	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS/DAY	HOURS 15T	2110	3RO SMIFT	-	IFTS / DAY		HOURS	/ SHIFT	
1. CREW – SHIFTS / DAY WORKING DESIGNATION	HOURS / SHIFT		2. CREW – SHIFTS / DAY	HOURS /	SHIFT	CASE HIS	3. CREW - SHIFTS/DAY	HOURS 15T	2110	3RO SHIFT	-	IFTS / DAY		HOURS	/ SHIFT	

CASE HISTORY DATA

DESCRIPTION		B. DESIGN INFORMATION
PROJECT NAMES ECTION FZA - BRANCE ROUTE	NUMBER [FOOZ]	1. PLAN AND PROFILE ATTA
LOCATION WASHINGTON D.C.		2. TYPICAL SECTION DRAW
3. OWNER WATA	ENGINEER PBQD	3. TEMPORARY LININGS DE
4. CONTRACTOR TRAYLOR BODS. &		4. PERMANENT LININGS DE
5. DATES: START	COMPLETE	5. GEOLOGICAL PADFILE A
6 PROJECT SCOPE (INCLUDE ANY APPURTENANT STRUCT	URES)	6. VERBAL DESCRIPTION OF
	BORES- INBOUND - OUTBOUND)	SAND WIT
PLUS: VENTILATION S	TRUCTUESS,	SAUD & G
UNDERGROUN FLEETING	AL SUBSTATION.	
DRAINAGE PUMPING	STATIOUS ELEGALE STRUCTURES	
UNDERPLUMING OF	ELECARE STRUCTURES	
7. OWNER FURNISHED MATERIAL AND EQUIPMENT LIST		7. DEWATERING PLAN ATTA
NONE		8. GROUND WATER CONDIT
8. OTHER OWNER SUPPLIED COST ITEMS (e.g. INSURANCE)		9. SITE PREPARATION & RE
		REPLACE 48
1.10		1075 LF -

B. DESIGN INFORMATION	SHEET 1	_ OF		
1. PLAN AND PROFILE ATTACHED	YE	s	NB	_
2. TYPICAL SECTION DRAWING ATTACHED.	YE	s	NO	٢
3. TEMPORARY LININGS DETAILS ATTACHED:	YE	s	NO	_
4. PERMANENT LININGS DETAILS ATTACHED:	YE	s	NO	~
5. GEOLOGICAL PADFILE ATTACHEO	YE	s	NO	
6. VERBAL DESCRIPTION OF SOIL CONDITIONS				_
SAND WITH CLAY LENSON, SOME MEDIUM	STIFE	C/	47	
SAND WITH CLAY LENSES, SOME MEDIUM SAND & GRAVEL LAYERS WITH SOME	BOULDE	عرية	-,-	
7. OEWATERING PLAN ATTACHED	YE	s	NO	v
8. GROUND WATER CONDITIONS DESCRIPTION				
		_		
9. SITE PREPARATION & RESTORATION DESCRIPTION				
REPLACE 482 SY OF STREET PAVEN	15:17			
1075 LF - CURB & GUTTER & 5555	Y SING	WA	عد	
to the Li Corn order ter dossos	1146		, ~	
			-	

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

ESIGN INFOR	MATION (CONTINUED)
. UNGERPINNING	OESCRIPTION
Truma	PARY SUPPORT OF 7th STREET BRIDGE
	FROUT UNDER PINNING
PVI/H_C	TEOUT UNDERPHANING
64.	T UNDBERMING - SEFFERSON MEMORIAL
GROU	T UNUBLYINING - SETERSON MEMORIAL
JUNIO	A HIGH SCHOOL
W711 17150 050	ADDITION OF THE PROPERTY OF TH
. UTILITIES. DES	CRIPTION
S7	PANDARD UTILITY INSTALLATIONS BURIED IN
STREE	TS ABOVE - SUPPORTED AND/OR RELOCTED
As t	PEQUIRED

CONSTRUCTION ME	THODS	SHEET 2	OF
. FREE AIR.	YES	LENGTH (FT)	592
. COMPRESSED AIR		LENGTH (FT)	
PSIG MIN	PSIG MAX	PSIG WTO AVG.	
REHOVE	ED BY CONVERTED THE CONVERTED HUCK C	THRU SHIGED - MU EYOR BELT TO RA THRU STEEL LINER	10
TEMPORARY (LINING A/ONF		
	A lost c	-	
CINAL LINING	STERL LA	VER PATES	

Appendix A-1. (Continued)

CASE HISTORY DATA

	OR EQUIPMENT UTILIZE	D			
1. CUT	TING AND EXCAVATING				
	MAKE				
	MOOEL				
	TYPE	ROTATING WHEEL	OSCILLATING ARMS	DIGGING AR	м
		OTHER (SPECIFY)			
	CONNECTED HORSE POWE	R			
	NO. USEO			· ·	
2. SHII	ELO	ROBB	INS		
	OUTSIDE DIA.	18'-0"	LENGTH	162	, 2
	NO. OF JACKS		RCE (TONS) 75 N	O. OF JACKING MOTO	RS 4
	HORSE POWER EA. JACKII	1	200		
	NO. SHIELOS USEO	/			
3. MU(CKING EQUIPMENT (UNDERG	ROUNO)			
	TYPE	FRONT END	LOBOER		
	CONVEYOR LENGTH	(FT.)		APACITY	(T
	RAIL CARS NO		CA	PACITY	{ T
	RUBBER TIRE VEHICLE NO	9150	- 4DEMCS	APACITY SC	/ (T
	COMBINATION (SPECIFY)		-//-		
s. MUC	KING EQUIPMENT UNDERGR	OUNO TO SURFACE (O	ESCRIBE)		

LINERS (PRE CAST)		
DESCRIPTION	CAPACITY	NO.
·		
		-
GROUTING		
OESCRIPTION	CAPACITY	NO.
·		
CONCRETE INVERT (AND WALKWAYS)		
OESCRIPTION	CAPACITY	NO.
VENTING, PUMPING, COMPRESSION, EQUIPMENT		
OESCRIPTION	CAPACITY	NO.
OTHER (Specify)		

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

1. TUNNEL (IF MULTIPLE, SHI		
LENGTH 2942	-1B - Z980'	OB FT
INSIDE O.O.	OUTSIDE O.O	18'+
CONFIGURATION		
NO. CROSS OVERS, IF MULT	IPLE	EA
TOTAL EXCAVATION		CY
TUNNEL PRESSURE RANGE	PSI	PS
2. GROUTING (CY)		
	ESY	ACTUAL
BEHINO TEMP, LINING		
CONSOLIDATION (FACE)		
PREGROUTING		
3. TEMPORARY LINING (IF US	EO)	
OESCRIPTION		DUANTITY
I. FINAL LIMING		
	. / P.	
NO. LINERS IF PREFAB OR F	LAWER RA	
OUANTITIES IF CAST-IN-PLA		EA
OESCRIPTION		
		DUANTITY
CONCRETE		(C Y
REINFORCING		(TOWS
FORMING		tS F

OESCRIPTION	DUANTITY
CONCRETE	(CY
RESAR	(TOWS
FORMS	(S.F.
STRUC STEEL	(TONS
7. MAJOR UNDERPINNINGS	
DESCRIPTION	AREA (S.F.)
CHENICAL GROST -	
CHEMICAL GROWT - JEFFERSON JUVIAN 415, 75 STREET BRIDGE	
75 STREET BRIDGE	1
	1
	'
TOTAL	
TOTAL	
TOTAL 8. AIRLOCK SYSTEM (IF USED)	(EA)
TOTAL 8. AIRLOCK SYSTEM (IF USED) MAN LOCKS	
TOTAL 8. AIRLOCK SYSTEM (IF USED) MAN LOCKS NUMBER	(EA)
TOTAL 8. AIRLOCK SYSTEM (IF USED) MAN LOCKS NUMBER LENGTH	(EA)
TOTAL 8. AIRLOCK SYSTEM (IF USED) MAN LOCKS NUMBER LENGTH DIAMETER	(EA) (FT)
TOTAL 8. AIRLOCK SYSTEM (IF USED) MAN LOCKS NUMBER LENGTH DIAMETER MUO LOCK	(EA)
TOTAL 8. AIRLOCK SYSTEM (IF USED) MAN LOCKS NUMBER LENGTH DIAMETER MUO LOCK NUMBER	(EA)

9. APPURTENANT STR	UCTURES		
VENT AND FAN SHA	FTS		
CONSTRUCTION METH	00 SOLDIER H	Prest Las	SING
FORMEDO	00 SOLDIER H ONCRETE KI	us of S	433
WIOTH (FT	BREADTH	FT DEPTH	FT
WALL THICKNESS			
EXCAVATION QUANTIT	TES		(€∀)
CONCRETE OUANTITIE	s		(CY)
PUMPING STATIONS			
CONSTRUCTION METHO	00:		
CONFIGURATION			
DEPTH	(FT) DIAMETER		(F T)
EXCAVATION QUANTIT	TIES		(C Y)
CONCRETE QUANTITIES	S		
OTHER APPURTENAN	NCES (SPECIFY)		
DESCRIPTION	EXCAV. (CY)	CONCRET	E (CY)
10. SITE PREPARATION	& RESTORATION		
OESCRIPTION	TYPE	AREA (S	i.F.)
CLEAR & GRUB			
DEAMONAL	PAVING REPAVE		
REMOVAL	MAINIANG		

Appendix A-1. (Continued)

CASE HISTORY DATA

HOURS/SHIFT 2 3		
1ST SHIFT	.aπo SHIFT	SHIFT
		l
	- 1	
i	1	
1	1	
7	1	
	1	l
8	8	
1	1	
2	2	
	,	
23	ひ	
	1 1 1 1 7 1 8 1 2 1	15T ##05 SHIFT SHIFT 1 1 1 1 1 1 1 1 1

TOTAL

HIFTS/DAY	HOURS / SHIFT		
WORK DESIGNATION	1ST	2NO	3R0
	SHIFT	SHIFT	SHIFT
			1
			
		ļ	ļ
	1		
	+		
			-
		L	
	1		
			-
	1		i
	+		
			<u> </u>
	1		
			-
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			l —
			
			L

3. CREW ~					
SHIFTS / DAY HOURS / SHIFT					
WORK DESIGNATION	1ST SHIFT	2ND SHIFT	3RO SHIFT		
	-				
	1				
	1				
	_				
	1	_	-		
			-		
	-				
	<u> </u>		_		
	+				
		<u> </u>			
			-		
	-				
	4				
	_				

SHEET _ 5 _ OF			
4. CREW –			
SHIFTS / DAY	HDURS /		
WORK DESIGNATION	SHIFT	2NO SHIFT	3F SH
	1		1
	†		
	1		
	 		
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	4		L
			_
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			_

(1) NOTE CATEGORY OF CREWS (HEADING, SUPPORT SURFACE, SHAFT ETC.) REPORT AS LOGGED

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

1. CREW- Mining ('ceis		
SHIFTS/DAY 3	HOURS /		
WORKING DESIGNATION	IST SHIFT	SHIFT	3 P.D. SHIFT
Foreman	ı		1
Shield Operator			
Miners	7	7	7
Muck Operator	1	1	
Conveyor Operator	1	i	1
accomptive Opr.	a	a	a
· ·			
4			

2. CREW - Support Crew				
SHIFTS/DAY 3	HOURS /	SHIFT	8	
WORK DESIGNATION	1ST SHIFT	2NO SHIFT	3RO SHIFT	
Foreman	1	1	1	
Crone Operator	1	1		
Crane Oiler	_1_	1	1	
Bottom Men	a	_2_	a	
Compressor Oper	_1_	1	1	
Top Man	- 1	1	\Box	
-				
TOTAL	7	7	7	

3. CREW - Grout Crew				
SHIFTS/DAY 3	HOURS/	SHIFT	8	
WORK DESIGNATION	1ST SHIFT	2NO SHIFT	3RO SHIFT	
Foreman	- 1	1	1	
Nozzlemen	a	a	a	
Pumpman	1	. 1	1	
Pumpman Helpers	a	a	a	
•				
TOTAL	(-	(.	<u></u>	

SHI	EET	OF	
4. CREW - Bull G	4119		
SHIFTS / DAY 3	HOURS /	SHIFT 8	3
WORK DESIGNATION	1ST SHIFT	2ND SHIFT	3RD SHIFT
Foreman	_	-	1
Miners	4	4	4
		_	
TOTAL	5	5	5

(1) NOTE CATEGORY OF CREWS (HEADING, SUPPORT SURFACE, SHAFT ETC.) REPORT AS LOGGED

CASE HISTORY DATA

A. OESCRIPTION		B. DESIGN INFORMATION	SHEET1 OF
1. PROJECT NAME FOO 12	NUMBER FIB	1. PLAN AND PROFILE ATTACHED	YES NO 4
2. LOCATION WASHING TON D.	, C.	2. TYPICAL SECTION DRAWING ATTACHED	YES NO -
3. OWNER WMATA	ENGINEER	3. TEMPORARY LININGS DETAILS ATTACHED:	YES NO -
4. CONTRACTOR		4. PERMANENT LININGS DETAILS ATTACHED:	YES NO -
5. OATES: START	COMPLETE	5. GEOLOGICAL PROFILE ATTACHEO:	YES NO »
6. PROJECT SCOPE (INCLUDE ANY APPURTENANT STRUCTUR	RES)	6. VERBAL DESCRIPTION OF SOIL CONDITIONS.	
		SAND - SOME CLAY, BOUL	-DERS & GRAVEL
7. OWNER FURNISHED MATERIAL AND EQUIPMENT LIST		7. DEWATERING PLAN ATTACHED	YES NO
		8. GROUNO WATER CONDITIONS DESCRIPTION	
8. OTHER OWNER SUPPLIED COST ITEMS (e.g. INSURANCE)		9. SITE PREPARATION & RESTORATION DESCRIPTION	

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

B. DESIGN INFORMATION (CONTINUED)	C. CONSTRUCTION MET	HOOS	SHEET2	OF
	1. FREE AIR	YES	LENGTH (FT)	333K
	2. COMPRESSEO AIR	'	LENGTH (FT)	
	PSIG MIN	PSIG MAX	PSIG WTO AVG.	
	3. DESCRIPTIONS			
10. UNDERPINNING DESCRIPTION /VON C	TUNNEL EXCAV	ATION		
11. UTILITIES. DESCRIPTION	PRIMARY LIN	ING		
STANDARD UNDER STREET UTILITIES NO SIEGLA GROWTING, ETC		TECK RIBS &	(WOOD LAGGIN	9
No SIBUR GROWTING, ETC				
	FINAL LINING			
		15" CONCRETE		

CASE HISTORY DATA

. CUTTING AND EXCAVA	TING	ANA	MININ	٢		_
MAKE						
MODEL						_
TYPE:	ROT	ATING WHEEL	OSCILLA	TING ARMS	DIGGING ARM	L
	ОТ	HER ISPECIFY)				
CONNECTED HOR	SE POWER					
NO. USEO						
2. SHIELD	MILW	AUKEE	BOILE	RE MEG	F	
OUTSIDE DIA.		2017		LENGTH	21,9'	
NO. OF JACKS		THRUST	FORCE (TONS)	Z,500 NO. 0	F JACKING MOTORS	
HORSE POWER E	A. JACKING N	OTOR -				
NO. SHIELOS US	EO					_
3. MUCKING EQUIPMENT	UNDERGROL	IMO)				
TYPE:						_
CONVEYOR: LER	IETH	(FT.)		CAPAC	HTY	٢
RAIL CARE:	NO.			CAPAC	SITY	(
AUGUER TIRE VEH	IICLE NO.			CAPAC	:ITY	(
COMBINATION (SP	ECIFY)					
4. MUCKING EQUIPMENT	UMOERGROU	ND TO SURFAC	E (DESCRIBE)			

	SHEET3	OF
OTHER MATERIAL HANDLING EQUIPMENT (SPECIFY) SURFA	CE TO HEADING	
LINERS (PRE CAST)		
DESCRIPTION	CAPACITY	NO.
GROUTING		
DESCRIPTION	CAPACITY	NO.
CONCRETE: INVERT (AND WALKWAYS)		
DESCRIPTION	CAPACITY	4 0.
6. VENTING, PUMPING, COMPRESSION, EQUIPMENT		
DESCRIPTION	CAPACITY	NO.
DESCRIPTION		
		L
7. OTHER (Specify)		

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

1. CREW -				2. CREW –				3. CREW -				4. CREW -		
SHIFTS / DAY Z	HOURS	SHIFT	3.0	SHIFTS / DAY	HDURS	SHIFT		SHIFTS / DAY	HOURS /	SHIFT		SHIFTS / DAY	HOURS	
WORKING DESIGNATION	SHIFT	SriFT	1 00	WORK DESIGNATION	1ST SHIFT	2ND SHIFT	3RO SHIFT	WORK DESIGNATION	IST SHIFT	2ND SHIFT	3RO SHIFT	WORK DESIGNATION	IST	
SUPERINTENDENT	(1)													
FORFHAN		1												
OPERATORS	2	2												
(MINERS)	6	6												
FLECTRICIAN	Lı_	1	\square			L								
MECHANIC	ı	2												
LOLDERS	~	Y												
	1										\neg		1	
TOTAL (AVERAGE	1,1	14												
TO THE OTHER PROPERTY.	1		\Box						1				1	
	1												1	
-	<u> </u>		\Box		1—								1-	
						-								
									1					
													1	
		-							+				1	
			\vdash	_					+		\exists		+	
TOTAL			H						1-				+	

CASE HISTORY DATA

A. DESCRIPTION		B. DESIGN INFORMATION.	SHEET OF
1. PROJECT NAME Embarcadere to Montgomery S	NUMBER 150051-A	1. PLAN AND PROFILE ATTACHED:	YES ND
2 LOCATION San Francisco, Califo		2. TYPICAL SECTION DRAWING ATTACHED	YES ND
3. OWNER BARTD	ENGINEER PBTB	3. TEMPDRARY LININGS DETAILS ATTACHED:	YES ND
4. CONTRACTOR		4. PERMANENT LININGS DETAILS ATTACHED:	YES ND
5. OATES: START /0/8/70	COMPLETE 2/5/7/	5. GEOLDGICAL PROFILE ATTACHED:	YES ND
6. PRDJECT SCDPE (INCLUDE ANY APPURTENANT STRUCTUR	F\$/	6. VERBAL DESCRIPTION OF SOIL CONDITIONS.	
Approximately 1440 St. line tunnels	of twin subuny	Mostly clay and sand with ground encountered. Ground	
7. OWNER FURNISHED MATERIAL AND EQUIPMENT LIST		7. DEWATERING PLAN ATTACHED	YES ND
		8. GROUND WATER CONDITIONS DESCRIPTION	
		Dewatering wells were u	ised throughout.
0. DTHER OWNER SUPPLIED COST ITEMS (e.g. INSURANCE)	-	9. SITE PREPARATION & RESTORATION DESCRIPTION	

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY OATA

B. DESIGN INFORMATION (CONTINUED)	C. CONSTRUCTION METHODS	SHEET 2 OF
	1. FREE AIR: VCS	LENGTH (FT) 729, 7 F
	2. CDMPRESSED AIR: Y,C S	LENGTH (FT) 709,96
		13.82 PSIG WTD AVG.
	3. DESCRIPTIONS	1
10. UNDERPINNING DESCRIPTION	TUNNEL EXCAVATION	
	Excauation was carri	ed out by a shield
	Excavation was carri used with a muck cor A rubber-tired uchicle	was also used
11. UTILITIES. DESCRIPTION	PRIMARY LINING	
	Steel liner rings	21/2 ft wide
	CONCICTO	

CASE HISTORY DATA

	TING AND EXCAVATING				
	MAKE				
	MODEL				
	TYPE:	ROTATING WHEEL	OSCILLA	TING ARMS	DIGGING ARM
		OTHER (SPECIFY)	Manual	Diggino	
	CONNECTEO HORSE POW	ER		221	
	NO. USEO				
2. SHIE	ELO				
	OUTSIDE OIA	18.125	7.	ENGTH	
	NO. OF JACKS	THRUST EACH JA	FORCE (TONS)	5800 NO. OF	JACKING MOTORS
	HORSE POWER EA. JACKI	NG MOTOR			
	NO. SHIELDS USED				
3. MUC	KING EQUIPMENT (UNDERG	ROUNO)			
	TYPE: 248 EI	mco Air	Muckers		
	CONVEYOR: LENGTH	(FT.)		CAPACIT	Y (1
	RAIL CARS: NO.			CAPACIT	Y (1
	RUBBER TIRE VEHICLE NO			CAPACIT	γ (1
	COMBINATION (SPECIFY)				
	KING EQUIPMENT UNDERGE				
2 5	ortable generati Swheel dump ock jack, 193 lydynamic c	na I Ja	544 Bac	khoc. 10	shicky
2 10	s-wheel duma	trucks.	2 iack 1	cos a b	reakers
Lro	cle jack. 1 9-	so-loader	1 pick	Up 15	50-hopper
1 H	ludunamic c	canc. 1 8	-10 cu du	mo truci	k 1 compress
	J - J	,	J		1, . CO / W/C C

OTHER MATERIAL HANDLING EQUIPMENT (SPECIFY) SURFACE TO	TIENOING	
LINERS (PRE CAST)		
DESCRIPTION	CAPACITY	NO.
GROUTING		
DESCRIPTION	CAPACITY	NO.
Grout Agitators		a
Chemical Grout Plant		1
Grout Pump Cars		a
21 201 1 000p = 01 J		
CONCRETE. INVERT (AND WALKWAYS)		
DESCRIPTION	CAPACITY	NO.
Concrete trucks		10
Batch plant		
odici pari		
VENTING, PUMPING, COMPRESSION, EQUIPMENT		
DESCRIPTION	CAPACITY	NO.
Bottery Locomotives Trains	15 Tan	1- 2
Bottery Locomotius, Trains Cranes Muck Cars	10-50 Tans	
M. ch. Core	10-30 lans	
Mucic Cors		6
OTHER (Specify)		

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

. QUANTITIES (NOT INCL	. ACCESS SHAFT)				
1. TUNNEL (IF MULTIPLE, SH	OW FOR EACH)				
LENGTH SR - 709,9	6 5R-70	29.7 FT			
INSIDE DIA. 17					
CONFIGURATION Cir	cular				
NO. CROSS OVERS, IF MUL	TIPLE	EA			
TOTAL EXCAVATION		CV			
TUNNEL PRESSURE RANG	· 2.75	PSI - 13.82 PS			
2. GROUTING (CY)					
	EST	ACTUAL			
BEHING TEMP. LINING		1163.50			
CONSOLIDATION (FACE)	_				
PREGROUTING		1			
3. PRIMARY LINI	NG				
DESCRIPTION DUANTITY					
2.1/a ft. Steel Rings					
4. FINAL LINING					
TYPE Concrete	_				
NO. LINERS IF PREFAB OR PRECAST E					
OUANTITIES IF CAST-IN-PLACE					
DESCRIPTIO	DUANTITY				
CONCRETE		(C)			
REINFORCING	(TON:				
FORMING		(S F			

6. INVERT (AND WALKWAYS), ARCH	
DESCRIPTION	DUANTITY
CONCRETE	(CY)
REBAR	(TONS)
FDRMS	(S.F.)
STRUC. STEEL	(TONS)
7. MAJOR UNDERPINNINGS	
DESCRIPTION	AREA (\$.F.)
TOTAL	
B. AIRLOCK SYSTEM (IF USEO)	
MAN LOCKS DODG	
NUMBER	(EA)
LENGTH	(FT)
DIAMETER	(FT)
MUD LOCK DONE	
NUMBER	(EA)
LENGTH	(FT)
DIAMETER	(FT)
BULK HEAD DESIGN	PSIG

		SHE	E1 Ur	-
9. APPURTENANT STRE	JCTURES			
VENT AND FAN SHA	FTS			
CONSTRUCTION METH	00:			
WIOTH (FT	BREADTH	FT	OEPTH	FY
WALL THICKNESS				
EXCAVATION QUANTIT	ES			(CY)
CONCRETE QUANTITIE	s			(CY)
PUMPING STATIONS				
CONSTRUCTION METHO	00:			
CONFIGURATION				
DEPTH	(FT)	DIAMETER		(FT)
EXCAVATION DUANTIT	IES			(CY)
CONCRETE DUANTITIE	5			
OTHER APPURTENA	NCES (SPECIF	FY)		
DESCRIPTION	EXCA	V. (CY)	CONCRETE	(CY)
			,	
10. SITE PREPARATION	& RESTORA	TION		
DESCRIPTION	TY	YPE	AREA (S.	F.)
CLEAR & GRUB				
REMOVAL				
RESTORATION				

Appendix A-1. (Continued)

CASE HISTORY DATA

1. CREW - Heading	(rcw			2. CF	IEW - Surf	ace			3. CREW -				4. CREW -			
SHIFTS / DAY 2	HOURS / SE	HET	8		S/OAY	HOURS /	SHIFT		SHIR#S / DAY	HOURS	SHIFT	Ĩ	SHIFTS / DAY	HOURS	SHIFT	
WORKING DESIGNATION	1ST SHIFT	2 N D SHIFT	3RD SHIFT	w	ORK DESIGNATION	N 1ST SHIFT	2NO SHIFT	3RO SHIFT	WORK DESIGNATION	1\$T SHIFT	2NO SHIFT	3RO SHIFT	WORK DESIGNATION	1ST SHIFT	2NO SHIFT	3R O SHIFT
Superintendent Shift Bass Heading Engineer Miners	1										-					1
Shift Boss															ļ	
Heading Engineer	1-2							<u> </u>			-				-	-
Miners	8-13			<u> </u>							-			-	-	_
Mechanics	1-4			<u> </u>		_	<u> </u>				-				-	_
Walker	1			-							-				-	-
Brakeman	1			<u> </u>							-			-	ļ	-
Operators Materman	1-2						-			_	ļ				-	₩
Matorman	1			-			-				-			-		-
Laborers	5						-	\vdash			-					+
Iron Workers Oiler				-			-			_	-			-	-	
Oiler	1			\vdash							+			-	-	
			_	-			-				+				-	
				-			-			+	+			+		
							-	-		-	+			-		-
	-			\vdash			-	+		-	+					
				-		-	1	+-+		-	+			+		-
				-												
														-		
							<u> </u>			1 -				1		
		-														
							-									
TOTAL	28-29	21									1				1	

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

A. DESCRIPTION		B. DESIG
1. PROJECT NAME LOWER Market Street	NUMBER /500//	1. PLAN A
2. LOCATION San Francisco, Calif.		2. TYPICA
3. OWNER BARTD	ENGINEER PBTB	3. TEMPO
4. CONTRACTOR Shea-Ball-Granite-C)/sen	4. PERMA
5. DATES: START 7/7/67	COMPLETE 4/10/70	5. GEOLO
6. PROJECT SCOPE (INCLUDE ANY APPURTENANT STRUCTU		6. VERBA
Four-bore (two bores on as steel ring lined. Total drive heading approximately 1570	of 6,283 LF Each	nos
cross over passages and ?	terminating tunnel	arco
ends.	<u> </u>	wea
	· · · · · · · · · · · · · · · · · · ·	
7. OWNER FURNISHED MATERIAL AND EQUIPMENT LIST		7. DEWAT
Segmented steel liners	\$	8. GROUN
Electrical switchgear		T
Lighting fixtures		appe
	rs, controls +dampers	mos
Power distribution	panels	insta
D. OTHER OWNER SUPPLIED COST ITEMS (e.g. INSURANCE)		9. SITE PE
Right-of-ways		
	en's compensation Insur.	

B. DESIGN INFORMATION.	SHEET_	1	OF		
1. PLAN AND PROFILE ATTACHED		YES		ND.	
2. TYPICAL SECTION DRAWING ATTACHED.		YES		NO	
3. TEMPORARY LININGS OETAILS ATTACHEO.		YES		NO.	
4. PERMANENT LININGS OETAILS ATTACHEO:		YES		NO	
5. GEOLOGICAL PROFILE ATTACHEO:		YES		NO	
6. VERBAL DESCRIPTION OF SOIL CONDITIONS.					
Soil was mostly clay and so	and.	w	i Ł	h	
some solid blue day The around	(wa	-2			
mostly cohesive except for occas	sion	21			
some solid blue clay The ground mostly cohesive except for occas areas of running sand some	arca	5			
were very firm in consistency.					
7. DEWATERING PLAN ATTACHEO		YES		NO	
8. GROUNO WATER CONDITIONS DESCRIPTION					
There were a few instances where	c w	ato			
appeared at the face Wetness st					
mostly below a level of "wet" but	the	cc		اعن	ح
instances of running water					
9. SITE PREPARATION & RESTORATION DESCRIPTION					

CASE HISTORY DATA

DESIGN INFORMATION (CONTINUEO)	
. UNDERPINNING DESCRIPTION	
. UTILITIES, DESCRIPTION	
Remove relocate support or replace	
Remove relocate, support or replace existing utility lines such as storm drown tary sewers, water, gas, lighting opposer distribution, and Muni lines.	nias
a stage for sail and the sail	21113
sunitary sewers, water, gas, ngriting	yna_
power distribution, and Muni Times.	

C. CONSTRUCTION METHOOS		SHEET	2 OF
1. FREE AIR:		LENGTH (FT)	6,283
2. COMPRESSED AIR: DOT	ped	LENGTH (FT)	
PSIG MIN	PSIG MAX	PSIG WTD AVG.	
3. DESCRIPTIONS			
TUNNEL EXCAVATION			
Exequation for	r tunnel SL was	witha	17,92 }
shield with a c	ligger arm. Tuni	oc/s 5R 1	TR. and
The used on 18	. 08 ft. shield u	with ad	igaer
	nels used a co		
and train for	muck removal.	About	
	ining was don		and.
	<u>J</u>	J	
PRIMARY LINING			
Scorented &	-1/off steel line	<u></u>	
3			
FINAL LINING			
Concrete			

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

I. CUI	TTING AND EXCAVATING						
	MAKE						
	MDDEL ,						
	TYPE	ROTATING WHEEL	0	SCILLATING ARMS	Π	OIGGING ARM	X
		OTHER (SPECIFY)	lan	d Minir	20		
	CONNECTED HORSE P	OTHER (SPECIFY) L	aile	ble	J		
	ND. USED						
. SHI	IELO						
	OUTSIDE DIA.	18.08 f	<i>¥.</i> \	LENGTH			
	NO. OF JACKS	THRUST I	ORCE (TONS) SA- 5	\$00°	TR-4800 - 3600	
	HORSE POWER EA. JA	CKING MOTOR					
	ND. SHIELOS USEO	1					
. MU	CKING EQUIPMENT (UND	ERGROUND)					
	TYPE: CONUC	for Belt an	d +	mins			
	CONVEYOR: LENGTH	(FT.)			APACITY	•	(T)
	RAIL CARS. NO.			C	PACITY		(T)
	RUBBER TIRE VEHICLE	NO.		C	PACITY		(T
	COMBINATION (SPECIFY	1					
. MU	CKING EQUIPMENT UNDE	RGROUND TO SURFACE	(OESCF	RIBE)			
_							
_							

LINERS (PRE CAST)		
DESCRIPTION	CAPACITY	NO.
	·	
		
GADUTING		
OE\$CRIPTION	CAPACITY	NO.
Grout Machine		1
CONCRETE INVERT (AND WALKWAYS)	L	
DESCRIPTION	CAPACITY	NO.
Truck Mounted Thompson Concrete Pump		
mack floating mornpaon carriers with		
	-	
VENTING, PUMPING, COMPRESSION, EQUIPMENT		
OESCRIPTION	CAPACITY ·	NO.
Bottery Lac amotives		1-2
Battery Locomotives Fince Air Mucker		
	60 tons	1-2
Crones	GU TUIS	
7. OTHER (Specify)		

Appendix A-1. (Continued)

CASE HISTORY DATA

E QUANTITIES (NOT INCL	. ACCESS SHAF	T)	
1. TUNNEL (IF MULTIPLE, SH	IOW FOR EACH)		
ENGTH /	567		FT
INSIDE DIA. /6	6 " OUTSIG	DE DIA.	
	ale track b	0102 00 00	och
NO. CROSS OVERS, IF MUL		2	EA.
TOTAL EXCAVATION			CY
TUNNEL PRESSURE RANG	E O	PSI	PSI
2. GROUTING (CY)			
	EST	ACT	TUAL
BEHING TEMP_LINING			
CONSOLIDATION (FACE)			
PREGROUTING			
3. PRIMARY LINING	3		
DESCRIPTION)N	OUA	NTITY
Segmented ste	el rinos		
	J-		
4. FINAL LINING			
TYPE Concret			
NO. LINERS IF PREFAB OR	-		EA
OUANTITIES IF CAST-IN-PL	ACE		
DESCRIPTIO	N	OUA	NTITY
CONCRETE			(CY)
REINFORCING			(TONS)
FORMING			(S F)

6. INVERT (AND WALKWAYS), ARCH	
DESCRIPTION	OUANTITY
CONCRETE	(CY
REBAR	(TON:
FO RMS	(S.F
STRUC STEEL	(TON:
7. MAJOR UNDERPINNINGS	
· · · · · · · · · · · · · · · · · · ·	
DESCRIPTION	AREA (S.F.)
TOTAL	
8 AIRLOCK SYSTEM (IF USED)	
MAN LOCKS DODE	
NUMBER	(EA
LENGTH	(F1
DIAMETER	(F
MUO LOCK none	
NUMBER	(E
LENGTH	(F
DIAMETER	(F
BULK HEAO OESIGN	PSI

	SHE	ET 4	OF
9. APPURTENANT STRU	CTURES		
VENT AND FAN SHA	FTS		
CONSTRUCTION METHO	10		
WIOTH (FT)	BREADTH FT	DEPTH	FT
WALL THICKNESS			
EXCAVATION QUANTIT	ES		(CY)
CONCRETE OVANTITIE	s		(CY)
PUMPING STATIONS			
CONSTRUCTION METHO	0:		
CONFIGURATION			
DEPTH	(FT) DIAMETER		(FT)
EXCAVATION QUANTIT	IES		(CY)
CONCRETE QUANTITIES	5		
OTHER APPURTENAN	ICES (SPECIFY)		
DESCRIPTION	EXCAV (CY)	CONC	RETE (CY)
10. SITE PREPARATION	& RESTORATION	-	
DESCRIPTION	TYPE	AR	A (S.F.)
CLEAR & GRUB			
REMOVAL			
RESTORATION			

ECONOMIC FACTORS IN TUNNEL CONSTRUCTION

CASE HISTORY DATA

1. CREW -			
SHIFTS/DAY 3	HOURS /	SHIFT 9	ζ
WORKING DESIGNATION	1ST SHIFT	2 ND SHIFT	3 R D SHIFT
Compressor Huseman		1	
Laborers			
Mechanics	1-5	1.5	1-5
Operator	1-2	1-2	1-2
Motorman	L	-	١
Brokeman	L.	- 1	
Giler	1	- 1	1
Shifter		1	1
Miners	7-13	7-13	7-13
Surveyors	3-5	3-5	3-5
Iron Workers			
Grout Crew			
Superintendent		1	1
Walkers	1	1	
TOTAL			

SHIFTS/DAY 3	HOURS /		ζ	SHIFTS / DAY	HOURS/	SHIFT	
WORKING DESIGNATION	1ST SHIFT	2 ND SHIFT	3 R D SHIFT	WORK DESIGNATION	1ST SHIFT	2NO SHIFT	3A C SHIF
Compressor Huseman			1				ļ.,
Laborers							
Mechanics	1-5	1.5	1-5		1		
Operator	1-2	1-2	1-2				<u>L</u>
Motorman	L	1	1				
Brokeman	L.	- 1	L				
Giler	1	1	1		.1!		
Shifter		1	1				
Miners	7-13	7-13	7-13				
Surveyors Iron Workers Grout Crew Superintendent Wolkers	3-5	3-5	3-5				
Iron Workers							
Grout Crew							
Succintendent	1	1	1				
Walkers	1	ı	1				
TOTAL							

IIFTS / DAY	HOURS /	SHIFT	
WORK DESIGNATION	IST " SHIFT	2ND SHIFT	3RO SHIF
	+		
	1		
	+		
	+	-	
	1		
	1		
	-		
	-		
	-		

4. CREW -			
SHIFTS / OAY	HOURS /		
WORK DESIGNATION	SHIFT	2ND SHIFT	3AD Shift
	3,,,,	3.1.1.1	JAILL
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SHEET _ 5 OF ___



Appendix A-2

A record of the weekly average, for each tunnel studied, of the

- progress rate,
- down hours and
- soils encountered.

All data, including those concluded to be outliers, are listed. These data are also available on the punched-card data sets submitted.



(AY AREA RAPIO TRANSIT DISTRICT CCNTRACT NUMBER 190031 PR TUNNEL - 24TH 10 FANDALL STPLET SAN FRANCISCO, CALIFORNIA

				00%	HOURS + I		WEEK			FEL	SVITA	FFLOU	ENCY THE W		IL T	rPE C	URI40	
			12222			=====	:====:			====	=====	=====		=====	====:		====	
STATION TUNNE AT START RATE OF BEEK FIZER			1HIELO	EXCAV	CONVEYOR	HUCK		ADMIN	TOTAL EOWN HOURS	I	II	111	ΙV	٧	V 1	V11	VIII	RUNNING BATER*
		======	======	======		======				=====	=====	=====	=====	=====	====:	====	=====	
300.83 15.0	0 15.40	6.00	• 50	.00	• C U	- 60	- 00	.00	•90	.00	1.00	.00	.00	- OC	.00	1.00	.00	•20
360.68 32.5	9 47.50	32 • C G	•00	5.60	. C O	• CO	2.58	.00	7 + 5 C	.00	1.00	•00	.03	•00	.00	1.00	.00	•20
300.35 187.5	0 235.06	110.00	• 90	• O C	• 0 0	. CO	10.60	.00	10.60	.00	1.00	٠٤٥	.06	.00	.00	1.00	.00	•20
298.48 97.5	0 332.50	41.60	.00	.00	.00	• 00	78.00	1.00	79.00	0 نا ه	1.00	.00	.00	.00	.CO	1.00	• O C	•20
297.50 220.0	ე 552÷5C	111.00	•0	2.00	• 0 0	4 + 00	3.00	.30	9.00	•10	•50	.00	.00	.00	.00	1.00	•00	•20
295 • 30 127 • 5	0 680.00	56.00	.00	5.00	• 0 0	• 00	17.00	.00	22.00	.5?	.50	.00	.00	*CO	•CO	I + C O	•00	·20
294.03 145.0	0 825.00	54.00	• 30	• C C	•30	. ພ	66.50	.00	66.50	. 50	•5 C	•20	.00	.00	• C O	1.00	.00	.20
292.56 260.0	0 1685.00	94.06	0 ن ه	7.00	• 0 0	+ U O	19.00	.00	26.00	.5C	.50	.2C	.00	• UC	. CO	1.00	+00	+2 G
289.98 292.5	0 1377.50	94 - (.0	e (, 9	.00	. C O	. LC	26.50	.00	26.50	•10	1.00	• 1 C	.00	۰00	٥٦.	1.00	.00	.20
287.05 125.0	o 1502.5⊜	84 .CD	• 50	19.50	.00	- CC	17.00	.00	36.00	.10	1.00	-10	.90	٠٤٥	.00	1.00	• 00	•20
265.80 155.0	0 1657.50	77.03	00	29.00	۵0 ه	- 60	14.00	.00	43.06	.16	1.00	-10	.06	.00	.00	1.00	.00	.20
264.25 192.5	n 1650.00	90.00	.00	8.00	• O O	• CO	22.00	.00	30.00	.10	1.00	·IC	ن ٥٠	-00	• CO	1.00	+00	·20
282.33 110.0	0 146C.00	56.CO	•60	56.00	• 0 0	.00	13.50	•70	69.50	.10	1.00	.35	.00	.00	.00	1.00	.00	•20
281.23 90.0	0 2050.00	112.50	• 6 0	3.00	.00	.00	5.00	.00	00.8	.10	1.00	.35	.00	-60	.00	1.00	.00	.20
280.33 250.0	0 2300.00	8 6 .[U	. Jn	15.00	. O O	00 ء	18.50	۰00	33.50	.10	1.00	.35	•00	+60	.00	1.00	.00	•20
277 - 63 257 - 9	0 2557.50	82.00	• 70	19.50	• 0:0	.00	18.50	.00	38.00	- 10	1.00	.35	.00	.00	.00	1.00	.00	•20
275.25 300.0	0 2857.50	95.00	. JO	5.50	• C O	4.00	15.50	.00	25.00	.10	I.0C	.35	•00	.00	. CO	1.00	.00	·20
272 - 25 245 - 0	0 3102.50	100.00	.00	16.50	• 0 0	• CO	4 • 0 0	• 0 0	20.00	-15	1.00	-15	٠٥٠	.00	.00	1.00	.00	÷20
269.80 237.5	0 3344.00	88.00	• 10	22.00	.00	5 .00	4.50	.00	31.50	+15	1.00	.15	•70	+OC	.00	1.00	.00	.20
267.43 257.5	U 3597.50	94.10	• 10	7.00	• C O	• CO	19.50	.30	26.50	-10	1.00	1.00	1.00	• 8 C	.00	1.00	.00	.50
VEY FOR SOIL T				v - cs	MENTED GI	RUTIND		* 14.	E V 10 V	ALUES	FOR	RUNN	ING WA	TER				
11 - CLAY AND 111 - SAND AND IV - COBBLES	SANO GRAVEL	ERS	v	V1 - PE	AT AND TE	RASH		. 2	= 0RY 5 = MOI 0 = WET	S T		= RUN = FLO	IN I N G	WATER				

PROGRESS AND PRODUCTION

EAY AREA RAPID TRANSIT DISTFICT CONTRACT NUMBER 190331 PA TUNNEL - 2411 TO RANDALL STREET CAR FRANCISCO, CALIFORNIA

A011412	TUNNEL	CUMUL.	J0 19		=====	NHOURS - By C	A U S E	=====	=====	TOTAL	20L	ATIVE	FREO	THE W		01L T	YPE ()URIN(;
CF &ZEK	FI/wk	[ATE	HRS IN	SHICLD	E ACAV	CGNVEYOR	MUCK TPANS		AOM1N	LOWN HOURS	I	I1	111	ΙV	٧	٧1	V1 I	VIII	RUNNING #ATER*
										=======	2:::				=====	====:		=====	
264.85	257.50	3655.00	95.[U	+60	12.50	.00	.00	13.00	• 00	25.50	.15	1.00	.15	• O O	٠ ۵ ۵	• 0.0	1.00	.00	.50
262.28	247.50	4102.50	92.00	+10	20.50	• 0 0	.00	8 • 00	• 00	28.50	.15	I.NG	• 15	د نا د	.00	. i 0	1.00	.00	•50
259.80	195+60	4297.50	83.60	.00	22.00	• N C	• UO	15.00	.00	37.40	+15	1.00	-15	• 20	.00	.00	1.00	.00	
257.85	47.50	4345.00	41.00	• 10	76.00	.00	.00	3.00	.00	79.DC	. 15	1.00	• 15	.00	• CO			.00	
257.38	86.00	4425.0C	56.00	٥٥.	•00	• 0 6	.00	16.50	• 30	16.50	.15	1.00	.15	1.00	.80				

EAY AREA RAPID TRANSIT CISTFICT CONTRACT NUMBER 195031 ML TUNNEL - 24TH TO FANUALL STRUCT SAN FRANCISCO, CALIFORNIA

	DO=NHOURS - HOURS BY CAUSE		FELATIVE FREQUENCY OF SC THC NCEK	
STATION TUNNEL CUMUL. PROF	JHICLU EXCAV CONVCYOR MUCK EGUIP TRAN	HISC ACHIN LOWN S HOURS	1 11 I11 1V V	VI VII VIII RUNNING WATCR*
203-63 20-00 20-00 32-00	1.50 .00 .00 .00	5.00 .00 6.50	.00 1.00 .00 .00 .00	.CO 1.00 .OC .20
300.63 32.50 52.50 34.00	2.00 2.00 .00 .00		.00 1.00 .00 .3u .60	.00 1.00 .00 .20
700.30 122.50 175.00 76.00	0 34.50 .00 .00		.00 1.00 .00 .00 .00	.00 1.00 .00 .20
259.08 16E.00 335.GE 89.00	3.00 27.00 .CO .00		.00 1.00 .00 .00 .00	
257.26 220.00 555.00 113.00	4.00 .00 .00		.50 .50 .00 .06 .00	.00 1.00 .00 .20
295.06 237.50 792.50 102.00	00. 00. 00.	18.50 .JC 18.50	.50 .50 .20 .0C .CO	•00 1•00 •00 •26
292.70 37L.00 1162.5° 112.00	•00 1•50 •00 •00	5.00 1.50 8.00	.50 .50 .20 .00 .00	•CO 1•00 •00 •20
269.00 187.50 1350.00 60.00	•J0 2•00 •00 •C0	13.50 2.00 17.50	•10 1•30 •10 •03 •0 0	.00 1.00 .00 .20
207.13 137.5U 1487.50 63.00	.00. 00. 00.	14.50 .50 15.00	.10 1.90 .10 .00 .00	.00 1.00 .00 .20
285.75 27.50 1515.50 10.00	.00 2.00 .00 .00	108.00 .JC 110.3C	.10 1.00 .10 .0C .00	.00 1.00 .00 .20
265.48 186.00 1695.00 84.00	1.00 -00 14.00 13.00	7.50 .30 35.56	-10 1-00 -10 -00 -CO	•00 1•00 •00 •20
283.68 175.00 1870.00 93.10	.50 16.00 .00 .00	11.00 .00 27.00	.10 1.CO .1C .OC .CO	.00 1.CO .00 .20
281.93 65.00 1935.00 59.00	. JO 57.00 .00 .00	4.00 .30 61.30	-10 1-00 -35 -06 -00	.CO 1.OO .NO ' .ZO
رى 280 - 96 22 - 50 1987 - 50 28 - Cن	.30 96.00 .00 .UC	4.50 .00 92.50	.10 1.00 .35 .DU .00	.00 1.00 .00 .20
280-75 175-00 2162-55 66-00	.00 40.50 12.50 .00	1.00 .00 54.00	.10 1.00 .35 .00 .60	.00 1.00 .00 .20
279.00 332.50 2495.00 104.00	.J0 6.CO .OO .CO	10.50 .30 16.50	.10 1.00 .35 .00 .00	.00 1.00 .00 .20
275 • 67 82 • 50 2577 • 50 56 • 0	.00 58.00 .00 .00	5.50 .00 63.50	•10 1•00 •35 •00 •C0	.CO 1.OO .OO .20
274.85 210.00 2787.50 101.00		10.00 .00 19.00	.10 1.00 .35 .00 .00	.00 1.00 .00 .20
272.75 292.50 3080.00 94.00			.15 1.00 .15 .0C .00	.00 1.00 .00 .20
269.83 205.00 3285.60 95.60	.00 14.50 .00 .60	9.50 .50 24.50	.15 1.00 .15 .30 .00	.00 1.00 .00 .20
KEY FOR SOIL TYPES 1 - SILT AND CLAY 11 - CLAY AND SAND 11I - SAND AND GRAVEL 1V - COBBLES AND BOULDERS	V - CEMENTED GROUND V1 - PEAT AND TPASH V11 - COMESIVE GROUND V111 - RUNNING GROUND	0 = ORY	ST 1 = FLOODED	

PROGRESS AND PRODUCTION

FAY ARCA RAPID TRANSIT DISTRICT CONTRACT NUMBER IMBOBI PL TUNNEL - 24TH TO RAMEAUL STREET SAN FRANCISCO, CALIFORNIA

					00 61	HOURS -		WECK			REL	ATIVE	FREOL	THE N		11 1	Y PE (URING	
TATION T START F LCEK		CUMUL. FCET TO CATE		SHIELD	EXCAV EQUIF	CONVEYOR	MUCF TRANS	MISC	AUMIN	TOTAL LOWN Hours	1	11	111	Ιv	v	v1	vII	VIII	RUNNING BATER+
267.78	230.00	3510.00	92•E0	•00	21.00	.00	.00	6.00	•5c	27.50	.10	1.00	•10	•00	•00	.co	1.00	.00	•20
265 •28	285.30	3795.00	95 •CU	• ~0	7.00	.00	• C O	16.50	1.50	25.00	-10	1.30	1.00	1.00	.80	.00	1.00	.00	•50
262.42	325.00	4120.00	164.00	• u0	7.50	.00	.00	8.5C	• 30	16.00	•15	1.00	.15	•00	-00	•C0	1.00	•00	•\$ U
259.17	160.00	4280.00	106.00	•uC	7 • C O	•00	•C0	5.50	.00	12.50	.15	1.00	-15	• 00	.00	.00	1.00	•00	•50
257.58	110.00	4 39 C • C C	101.00	.00	.00	• C O	. 60	11.00	•0C	11.00	.15	1.00	-15	1.00	.80	.00	1.00	.00	.50

CAY AREA RAPID TRANSIT DISTRICT CONTRACT NUMBER 140003 FRIAL TUNNELS EERRELEY, CALIFORNIA

											551	T 1 1/5	CDE	(F v. e				00 TH.	
						HOURS - I BY C	AUSE						-	THE					
	TONNEL	CUMU	0000				======			TOTAL	====	=====			=====	====:	====	=====	
STATION AT START	RATE	FEET TO	HRS IN			CONVEYOR	MUCK	MISC	ADMIK		I	II	III	ΙV	٧	v I	V1 I	VIII F	RUNNING WATER+
OF WEEK		UATE	.EEF		EGUIP						=====	====			=====	====:			
1224.92	20.30	28.0€	76 • C-O	4.30	•00		•00	00.3	. 90	12.00	.00	•20	•50	.06	• 00		I.00	•	•00
1224.72	62.00	93.00	120.00	• .0	.00	.00	• 60	• 00	•90	•00	•60	•50	•50	.60	•ú0	.00	1.00	•00	•00
1724 - 10	73.00	163.00	118.00	• - 0	.00	.00	• 00	2.06	.00	2.00	• GD	•20	•50	.00	.00	.00	1.00	•00	•00
1223.37	49.00	212.00	111.00	•90	•00	•00	3.60	1-00	5.00	9.00	.00	.50	•50	• 00	.60	.00	1.00	.00	•00
1222 - 88	52.00	264.00	114.00	3,.00	•00	• 0 0	•00	•00	3.00	6.00	-00	-50	•50	.00	.00	.06	1.00	•00	•00
1222.36	56.00	220.00	119-00	•00	•00	•00	1.00	•00	.00	1.00	• 00	•50	.50	.00	.00	.00	1.00	.00	.00
1221.00	47.00	367.00	60.00	34.00	.00	•00	•00	3.00	3.00	40.00	.00	.50	.50	.00	• UO	•00	1.00	•00	.00
1221.33	76.95	443-00	118 . 03	- 10	.00	.00	.00	2.00	•.00	2.00	•G0	•5€	-50	.00	•C0	.00	1.00	.00	.00
1220.57	86.00	529.00	126.00	• 70	.00	.00	.00	.00	.00	•06	•00	.50	•5 D	•06	.00	.00	1.00	• 00	•00
1219.71	£7.00	616.00	116 -00	20	•00	.06	• 66	.00	.00	2.00	•00	•50	•50	•00	.có	.00	1.00	.00	.00
1213.84	96.00	712.00	111.00	2.00	•00	.00	4.00	3-00	•00	9.00	- CO	-50	-50	•00	-60	- 00	1.00	.00	.00
1217 -88	59.00	771.90	78.00	2.30	.03	.00	. 00	.00	.00	2.00	•G0	•50	•50	.00	•00	.00	1.00	.00	•00
1217.29	91.60	862.00	117.00	2.00	•C0	.00	.CO	1.00	•00	3 • 0 0	•00	•5 O	•50	-06	-00	.00	1.00	.00	.00
1216.38	87.00	944.EN	113.00	5.36	• O C	•00	1 - 00	1.00	.30	7.50	.60	.50	.50	•06	•00	.00	1.00	.00	•00
1215.56	72.00	1016-00	99.00	20.00	.06	•00	1.60	-00	.00	21.00	.60	•30	•00	•50	.00	.co	1.00	•00	•00
1214.84	83.00	1099.00	119.00	1.00	.00	•00	• 00	.00	.00	1.00	•00	•00	-00	.50	-00	. 60	1.00	.00	•00
1214.01	58.00	1157.06	94.00	2.00	.00	•00	•00	-00	•00	2.00	•00	•06	•00	•5 Ü	•06	.00	1.00	.00	.00
1213.43	69.00	1225.60	96.00	•10	•00	.00	.60	.00	•00	•00	-00	.00	-00	•50	-00	•C0	1.00	• 00	.00
1212.74	65.00	1290.00	120.00	•30	•00	-00	• 00	•00	•00	•50	co	-00		1.00	1.00	. 00	1.00	.00	•00
1212.09	84.00	1374.00	119.00	•40	•00	.00	1.00	•00	•00	1.00	-00	.00	•60	1.00	1.00	•00	1.00	•00	•00
FEY FOR S	.011 176	oF 5							*K	E Y TO V	ALDES	FOR	RUNN	ING a	TER				
1 - 511					v - cc	MENTEO GI	ROUND												
II - CLA						AT AND TE				= ORY					M ATE R				
III - SAN			PS			HESIVE GI				5 = MOI 0 = WET		1	= FL(10050					
			-																

PROGRESS AND PRODUCTION

'AY AREA RAPIG TRANSIT DISTRICT CONTRACT NUMBER 1RODE3 AR/AL TUNNELS EERAELEY, CALIFORNIA

STATION	TUNNEL	CUMUL.	2039			* RSUOH* * 8 * 0	AUSE		=====	TOTAL				THE !	OF SC	-			
AT START	RATE FT/WK	FEET TO			EQUIP	CCNVE YOR	TRANS			DOWN HOURS	1	11		ΙV	v				RUNNING WATER+
1211 - 25		1459.00	119.00	• 30	•00	•00	1.00	• 50	.30	1.00	• 00	•00			1.00		1.00		
1210.46	15.00	1474.00	120.00	• 10	-00	• 0 0	.00	.00	.00	.00	•G0	•0 D	•00	1.00	1.00	•G0	1 - 0 0	•00	•00
1210 - 25	5.00	1479.00	120.00	.10	.00	.00	•00	•00	•00	•00	+00	•00	•00	1.00	1.00	.00	1.00	.00	•00
1224.43	119.00	1598.00	115.00	•00	•00	.00	4 • i.O	1.00	.00	5.00	1.00	1.06	-00	-00	•00	•00	1.00	• 00	•00
1223.24	74.00	1672.00	78.00	• 30	• 6 0	-00	2.00	•00	•00	2.00	1.60	1.00	.00	.00	•60	.00	1.00	•00	•00
1222.50	136.00	1 616 - 60	119.00	•40	-00	•00	1.60	.00	• 00	1.00	1.00	1.00	•60	.00	•00	.00	1.00	.00	.00
1221.12	133.00	1943.00	112.00	• 40	•00	•00	8 • 00	•00	.00	8.00	1.00	I .DC	.00	•90	-00	•60	1.00	.00	•00
1219.79	116.00	2659.00	103.GO	- 10	.00	.00	17.GO	• 00	•00	17.00	1.00	1 .00	•00	•00	• GD	.00	1.00	.00	.00
1218.63	140.00	2199.00	118.00	- 10	.00	.00	2.00	.00	•00	2.00	1.00	1.00	•00	- 00	.00	.110	1.00	.00	.00
1217.23	130.00	2329.00	112.60	.50	.00	.00	7.00	1.00	+00	8.00	1 - OĆ	1.00	-00	•00	.00	àő.	1.00	.00	
1215.93	39.OG	2368.00	69.00	-30	•00	• C O	51.00	.00	.00	51.00	1.00	1.00	•OD	•00	•00	•00	1.00	.00	.00
1215.54	94.00	2462.00	117.00	1.00	•00	•00	1.00	1.60	• 00	3.00	+00	-00	-00	1.00	I . ÖÖ	.00	1.00	.00	00
1214.60	84.00	2546.00	116 •CO	• 00	•00	•00	4 • 00	•00	.00	4.00	-06	•00	•00	1.00	I +00	.00	1.00	.00	-00
1213.76	104.30	2650.00	119.00	.00	.00	•00	• 00	1.00	•00	1.00	•00	•00	•00	1.00	1.00	.00	1.00	•00	•00
1212.72	96.00	2746.60	120.00	•00	.00	•00	•00	.00	•00	•00	•00	•00	-00	1.00	1.00	.00	1.00	.00	.00
1211.76	64.00	2810.00	77.00	43.00	•00	.00	• 00	•00	•00	43.00	• 00	•00	.00	1.06	1.00	•00	1.00	• 00	•D0
1211 - 12	78.00	2888.00	118.00	1.00	•00	.00	.00	1.00	•00	2.00	•00	•00		1.00			1.00		•00
		2903.00		•30	•00	.00	•00	•00	•00	•00	•00	•00			1.00		1.00		
				• 50	*00	-00	• 00	•00	.00	• 00	•00	•00	-00	00	1.00	-00			-50

Appendix A-2. (Continued)

EAY AREA RAPTO TRANSIT OISTRICT CONTRACT NUMBER 150511 TR TUNNEL SAN FRANCISCO, CALIFORNIA

						HOURS -	AUSE					AT 1VE		ENCY THE W	EEK			LR1NG	
STATION AT START CF beek	TUNNEL RATE FI/WK	CUMUL. FEET TO CATE		SH1ELO		C UNVE YOR	MUCK TRANS	M1 SC	AUM1N	TOTAL DOWN HOURS	1	11	111		v				RUNNING WATER+
46286.52	47.43	47.43	63.08	.50	.00	.00	.50	.00	• • • • • • • • • • • • • • • • • • • •	1.00									
48333.95	147.30	194.73	114.84	. 10	-00	-60	1.75	1.83	- 00	3.58	-00	1.00	.00	.00	.00	.co	1.00	.00	•00
48481.45	167.34	362.07	112.76	1.15	1.25	.50	.50	.00	.00	3 - 4 G	.00	1.00	•00	.00	. 00	.00	1.00	.00	•13
46648.79	204.78	566.85	115.59	1.32	1.50	.67	.00	• 2 S	.30	3.74	• G0	1.00	-00	.00	• CO	•00	.90	.00	•29
48853.57	129.89	696.74	99.44	8.93	5.56	. 25	• 42	3 - 38	•00	18.56	-00	1.00	•00	.00	.00	.00	• 00	1.00	•33
46983.48	192.22	888.96	99.37	5.59	8 • 6 7	1.42	.25	-50	.00	16.43	• 00	1.00	.UC	• 30	•00	•C0	. 40	•60	.00
49175.70	227.27	1116.23	102.36	.50	2 • 2 9	1-25	8 - 67	.30	•00	12.92	• CC	1.00	.00	.00	• 00	•00	1.00	•00	•00
45462.97	237.15	1353.38	168.40	.00	6.59	75	2.02	.83	.00	10.19	• 60	1.00	.00	.00	.00	.00	1.00	.00	.00
49640-12	109.83	1463.21	118.66	• 10	•00	.00	-00	•00	.00	.00	.00	1.00	-00	.00	-20	.00	. 45	•55	•10
49749.95	52.28	1515.49	97.62	7.41	3 - 17	.00	-00	4.67	.00	15.25	• 00	1.00	.00	.00	.00	.00	.00	1.00	•00
49802.23	34.99	1550.48	103.95	1-17	•00	.00	• 00	.00	.00	1.17	.00	1.00	•00	.00	-00	.00	.00	1.00	.00

PEY FOR SOIL TYPES

1 - SILT AND CLAY

V - CEMENTED GROUND

11 - CLAY AND SAND

VI - PEAT AND TRASH

0 - ORY

.75 = RUNNING WATER

111 - SAND AND GRAVEL

VII - COMESIES AND BOULDERS

VIII - RUNNING GROUND

.25 - MOIST

1 - FLOODED

PROCRESS AND PRODUCTION

FAY AREA RAPIO TRANSIT DISTRICT CONTRACT NUMBER 150G11 TIL TUNNEL SAN FRANCISCO, CALIFORNIA

						NHOURS - 8 Y C	AUSE						FPEOU	THE W	EEK				
STATION AT START CF week	-	CUMUL. FLET TO CATE		SH1EL0	EXCAV EOU1P	CONVEYOR	HUCK TRANS	MI5C	ADMIN	TOTAL DOWN Hours	1	11	111	1 V	٧	V1	VII	v111 #	RUNN IN WATER
48264.02	44.76	44.76	97.85	دى.	•60	.00	1.40	3.00	•00	4.40	.00	1.00	•00	.00	•co	.00	.00	.80	.40
48230.03	92.59	137.34	112.67	9.67	.00	.00	.00	2.16	.00	6.83	.00	1.00	.00	.00	. 34	.00	•60	. 90	.00
48421 - 36	172.27	309.61	114.59	٥٤.	.00	.00	1.91	• 00	.00	1.91	.00	1.00	.OC	.00	.35	.00	1.00	•00	•00
46593.63	159.82	469.43	93.00	•00	• 5 6	.50	. 00	.00	-00	1.00	• 00	1.00	.00	. 30	.00	.00	1.00	.00	.00
46753.45	159.88	629.31	93.58	1.25	.00	.50	• 00	•00	.00	1.75	• 00	1.00	.00	.00	.co	.co	. 90	•10	•10
48913.33	197.37	826 • 68	111.70	.38	2.25	3 • 4 2	.83	.00	.00	6.88	.00	1-00	-00	•00	•00	. CO	• 90	•02	.08
49113.19	227.36	1054.04	102.59	2.42	• 5 G	4 - 33	7.66	•00	• 0 0	14.91	.00	1.00	.00	.00	• 00	•00	1.00	.00	•00
49340.55	227.37	1281 - 41	105 • 10	3 • 1 6	5.43	2.16	2.27	. 38	.00	13.4C	.00	1.00	•00	.00	.00	•00	.80	.10	.30
49567.92	169.95	1451.36	92.24	5 • 55	2.5C	2.25	13.67	2.09	.00	26.06	.60	1.00	•00	.00	.00	• CO	.60	•13	•50
9737.87	64.93	1516.29	116.50	.30	.00	.00	• 00	1.00	-00	1.00	•00	ī.00	.00	.00	.00	.00	00	1.00	-15
9802.80	35.00	1551.29	75 . 66	.60	.00	.00	• 00	2.92	.00	2.92	- 00	1.00	۰00	.00	•00	•00	.00	1.00	•00

(AY ARFA RAPIO TRANSIT DISTRICT CONTRACT NUMBER 150011 SR TUNNEL SAN FRANCISCO, CALIFORNIA

FELATIVE FPEQUENCY OF SOIL TYPE OURING THE WEEK DOWNHOURS - HOURSZWEEK DOWNHOUSS - HOURS/WE'R FELATIVE FREQUENCY OF SOIL TYPE DURING THE WEEK STATION TUNNEL CUMUL PROF. TOTAL AT START RATE FEET TO HRS IN SHIELD SACAV CONVEYAR MUCK MISC AGMIN COWN I 11 11 11 IV V VI VII VIII PUNNING CF WEEK FT/WK GATC -EEK CUUIP TRANS HOURS WATER-46284.00 42.50 42.5° 55.42 .33 .CO .CO 20.00 1.50 .00 21.83 .90 1.00 .00 .00 .50 .90 1.00 .00 .CO 48328.87 122.6J 165.10 112.08 .00 .00 .CD 3.I7 2.91 *00 6.38 *00 1.36 *C0 *30 *50 *C0 *70 *20 .31 .33 .00 .00 .59 .67 .00 1.59 .00 1.00 .00 .00 .50 .00 1.00 .00 48451.47 47.53 212.63 44.24 .12 .50 6.33 .67 .00 10.17 .00 1.00 .00 .00 .50 .00 .70 .20 4 E 499 . CC 112 . 40 325 . D3 84 . 83 .00 2.67 .00 .75 .00 -00 46611.4U 164.88 489.91 113.C3 .50 4.42 .00 5.67 .00 1.00 .00 .00 .60 .00 .70 .10 +C0 .00 46776.28 164.84 654.75 106.81 1.73 4.50 .00 I.94 1.08 .00 9.27 .00 1.00 .00 .00 .40 .00 .30 .70 46941.12 184.57 839.32 100.83 2.58 5.50 .00 5.92 .00 .00 I4.00 .00 1.00 .00 .50 .70 .00 49125.69 192.29 1031.61 91.23 1.23 .00 .CO 26.86 .on .00 28.69 .00 1.00 .00 .00 .60 .PO 1.00 .00 .00 49317.98 204.73 1236.34 117.00 .42 .60 •00 •00 •00 •00 •42 •00 I•00 •00 •48 •00 •96 •00 .00 49522.71 179.41 1415.75 95.42

4970C.12 137.19 1552.94 54.08 .00 .00 .00 .00 .25 12.25 .00 12.50 .00 1.00 .00 .00 .00 .60 .00 1.00 .00

FEY FOR SOIL TYPES
I - SILT AND CLAY
II - CLAY AND SAND
III - SAND AND GRAVEL
IV - COBBLES AND BOULOERS

V - CEMENTEO GROUND
VI - PEAT AND TRASH
VII - COHESIVE GROUND
VIII - PUNNING GROUND

*MEY TO VALUES FOR RUNNING WATER

.00

PROGRESS AND PRODUCTION

EAY AREA RAPIO TRANSIT DISTRICT CONTRACT NUMBER 150011 SL TUNNEL SAN FRANCISCO, CALIFORNIA

						NHOURS - BY C	AUSE				_		FREQU	THE W	EEN				
STATION AT STAPT CF WEEK	FT/4K	CATC			EQUIP	CONVEYOR	TRANS		AUMIN	TOTAL COWN HOURS	1	11		IV	v				RUNNING SATER*
48277+05			109.33		.00	.00	٠٤٥	.00		.00		1.00		•00	.00		1.00		•00
48306.98	79.66	109.53	116.16	•>0	.00	• 00	.00	.00	. 00	• 5 0	۰۵۰	1.00	• E G	.90	.00	. 10	.00	1.00	• C O
46366.64	99.92	209.45	112.17	. JO	1.00	.50	1.50	1 • 25	2.50	6.75	.00	1.00	• O C	• 00	.00	.00	.00	1.00	.50
48486.56	117.50	326.95	112 • 42	• 30	.00	• 7 5	• 00	• 5 0	2.25	3.50	.00	1.00	•00	.00	.00	.00	• O C	1.00	.50
46604.06	59.98	386.93	57.67	.00	.00	2.50	• 00	5 • 5 0	.00	8.00	•00	1.00	.00	.00	.00	.00	• 00	1 • 00	.00
46664.04	138.90	525 + 83	108.50	1 + 25	•50	6.75	.00	.25	-00	8.75	. 00	1.00	.00	.00	.00	.00	.00	I + OC	.00
46862.94	113.40	639.23	81.17	1.58	4+50	3 • 3 3	• 00	•00	•00	9.41	.00	1.00	.00	.00	•00	•00	1.00	.00	•00
46516.34	157.48	796 • 7 Z	105.58	•50	• 5 C	2.00	2.00	.75	• 00	5.75	. 30	1.00	.00	.00	.00	.00	1.00	.00	.25
49073.83	54.89	851.61	88.90	• 00	2.00	2.00	• 00	+00	.00	4.00	.00	1.00	•00	• 00	• CO	.00	1.00	• 00	.00
49128.72	129.64	981.25	92.08	2.10	19.83	2.16	.00	1 + 3 3	•00	25.42	• 00	1.00	.00	. O G	.00	.00	1.00	•00	.00
49258.36	134.84	1116.09	98.42	.33	21.75	• 00	• LO	.00	.00	22.08	• 00	1.00	.00	.00	.00	.CO	• 0 0	1.00	.00
49393.20	179.65	1295.74	112.09	4.16	2 • 25	• D O	• CO	.00	.00	6.41	.00	1.00	.00	.00	.00	•00	1.00	.00	.00
99572 .85	162.12	1457.86	63.95	9 - 8 3	.5D	1.50	16.56	.50	.00	28.89	.00	1.00	•00	• 0 0	• 00	• CO	1.00	.00	•00
49734.97	107.33	1565.19	74 -83	. 40	.00	1.50	.00	3.83	.00	5.33	• CO	1.00	.00	.00	.00	.00	1.00	.00	.00

EAY AREA RAPIO TRANSIT CONTRACT NUMBER 1500:14 SR TUNNEL - MARKET STREET SAN FRANCISCO, CALIFORNIA

OGWNHOURS - HOURS/WCEK BY CAUSE RELATIVE FREQUENCY OF SOIL TYPE DURING THE WEEK STATION TUNNEL CUMUL. PRCC AT START RATE FEET TO HES IN CHIELD EXCAV CONVEYOR MUCK HISC AUMIN DOWN 2 II 111 IV V VI VII VII FUNNING THE WEEK FELATIVE FREQUENCY OF SOIL TYPE DURING THE WEEK TH 00. 00. 9L. .00 .00 1.00 .00 .00 .40 .00 .60 .38 .E0 51352 .14 22 .50 27 .46 66 .Cd .00 .00 .00 1332.06 67.50 94.96 110.25 1.25 .00 .00 3.25 3.00 .00 7.50 .00 1.00 .00 .00 .00 .00 .40 51262.08 42.50 137.46 52.34 7.83 .00 .00 .00 2.50 .00 10.33 .00 1.90 .00 .00 .00 .00 .20 .20 .75 \$1219.58 52.78 190.24 74.67 2.30 .00 .00 .33 .00 .00 2.33 .00 1.00 .00 .00 1.00 .00 1.00 .00 £1166.80 87.22 277.46 106.69 4.24 .00 .CO 3.50 1.0A .33 9.15 .C0 1.00 .CC .00 .00 .00 .30 .40 •32 51079.58 107.50 384.96 100.64 8.99 .00 1.67 2.95 2.42 1.25 17.28 .40 1.00 .00 .00 .00 .50 .50 .50 .34 \$C879.58 97.50 \$64.96 73.26 .92 .CC .00 2.17 4.25 .00 7.34 .00 I.00 .00 .00 1.00 .CO I.00 .00 .00 50792.08 122.50 687.46 1u5.52 .00 .CC 1.33 2.25 5.58 .00 9.16 .CC I.00 .00 .00 .00 .70 .00 50669.58 22.50 709.96 37.75 .00 .00 .00 .00 11.75 .00 11.75 .00 1.00 .00 .00 .50 .00 .70 .00 .10

KEY FOR SOIL TYPES

1 - SILT AND CLAY

II - CLAY AND SAND

III - SANC AND GRAVEL

IV - COBBLES AND BOULDERS

V - CEMENTEO GROUND
VI - PEAT AND TRASH
VII - COHESIVE GROUND
VIII - RUNNING CROUND

*KEY TO VALUES FOR RUNNING WATER

C = ORY .75 = RUNNING WATER
.25 = MOIST I = FLGODED
.50 = WET

PROCPESS AND PRODUCTION

TAY AREA RAPID TRANSIT DISTRICT CONTRACT NUMBER 150051A IL TUNNEL - MARKET STREET IAN FRANCISCO, CALIFORNIA

				LOPE	HOURS -		MEEK			REL	TIVE		ENCY The W		11 11	PE U	THIND	
						======	=====			::::	:::::				=====		:: :: :	
CF SEEK FT/WK	FEFT TC	HRS IN		EQUIP	CONVE YOR	MUCK TRANS		ADHIN	TOTAL TOWN HOURS	_	11							RUNNING BATER+
																		
1342.00 52.42	85.00	112.36	1.60	.00	.00	2.17	1.05	•00	4 - 17	- CO	1.00	•00	•00	•50	•60	.80	.10	•40
51269.58 67.50	152.50	94.08	1.15	•00	.00	16.38	- 25	.00	17.78	.00	1.00	•00	• 20	• 3C	•00	.70	•20	•75
51222.08 67.50	22C.OC	96.44	6.80	.00	.00	7.25	3.09	• 00	17.14	.00	1.00	•00	•00	. 30	•00	•90	.10	•25
£1154.58 60.00	280.00	78.36	1.08	•00	.00	2.50	.00	.00	3.58	. 00	1.00	•00	• O C ·	-20	•00	1.00	•00	•20
£1094.58 7C.00	350.00	79.50	1.00	•00	.00	1.08	•00	.00	2.08	• CO	1.00	•00	.00	•00	•00	1.00	•00	•15
1024.28 107.20	457.20	106.03	3.00	•00	•00	3.25	3.92	.30	10.17	•00	1.00	•00	•00	•00	•00	•90	•00	.16
5C 917 . 08 107 . 50	564.70	110.10	2.32	•00	• 00	2 • 25	1.75		6.32									
50809.58 125.00	689.70	103.49	3.58	•00	-00	4 • 68	3.22	.00	11.68	•00	1.00	.00	.00	.50	.00	1.00	•00	•00
£0664.58 40.00	729.70	49.46	•00	•00	•00	• 75	6.26	•00	7.0I	• 00	1.00	.00	•00	-50	•00	1.00	•00	•00

LFPER SALT CREEK #1 CONTRACT NUMBER 68-404-25 CHICAGG, ILLINOIS

						HOURS - 1	AUSE							THE V					
ACITAT2	THANKEL	COMUL	DECT				=====			TOTAL			=====			====		=====	
				SHIELO	EKCAV	CONVEYOR	HU CK	HISC	AUMIN			11	III	ΙV	٧	VI	VII	VIII	RUNN1NG
CF .EEK		EATE	w E E ⊬		EwUIP		TRANS			HOURS									WATER*
							=====	:====:								=====			======
432 .GC	24.00	24.00	25.50	• 10	• D C	8.00	. 60	• O C	•00	6.10	1.60	.00	•0C	.33	.00	.00	.00	00.1	1.00
456.00	14.00	36.00	16.00	0	.00	4.00	• 60	24.00	. 46	28.00	1.00	.00	• C O	• 00	-00	.00	.00	1.00	1.00
470.00	92.00	130.00	44.00	•36	6.00	• 0 0	• CO	• 00	.00	6.00	1.00	.00	•00	•00	•60	.00	.00	.75	1.00
562 - 10	60.00	210.00	25.60	0ن.	4.00	• O O	- 00	20.00	.00	24.00	1.00	• O D	.00	1.00	.00	• 00	1.00	•00	.00
642.00	4.00	214 • O C	3 oC D	- 70	5.00	- C O	.00	.00	.00	5.00	1.00	•0C	.00	1.00	-00	.00	1.00	.00	•C0
646.00	26.00	242.00	14.00	.JC	32.00	4-00	- 00	-00	-00	36.00	1.00	•00	.00	1.00	.00	•-C 0	.00	1.00	-00
674 - 00	23-00	265.00	16.00	•30	4.00	.00	.00	. U O	.00	4.00	1.00	.OG	•00	•00	.00	.00	1.00	.00	.00
697 .CC	19.00	284.00	10.00	.00	.00	. 00	• CO	6.00	.00	8.00	1.00	.00	.00	-00	۰00	.00	1.00	•00	.00
714 - 00	74.00	356 - 60	30.00	•00	4.00	16.00	• CO	• UD	.00	20.00	1.00	•00	.00	. 4 L	.00	.00	1.00	.00	+C0
788.GC	52.00	416.00	18.00	.00	6.00	15.00	• CO	-00	.00	21.00	1.00	•00	- D C	1.06	.00	.00	1.00	•00	•00
840.00	160.00	590.00	40 .CO	. JD	.00	8.00	.00	.00	.00	6.00	1.00	.DC	.00	1.00	.00	.00	1.00	.00	.00
1020.00	116.30	706.00	25.50	.00	10.00	10.50	.00	2 - 5 0	.00	23.00	1.00	.00	• C O	1.06	•00	•00	1.00	.00	.00
1136.00	132.00	838.00	28.00	.30	13.00	.00	•00	5.00	.00	18.30	1.00	.00	.00	1.00	.00	.00	1.00	.20	•20
1029.00	256-00	1094.00	38.00	• '00	2.00	6.50	.00	3.50	•00	12.00	1.00	•00	•00	۰26	-00	•00	- 80	.00	.00
1485.00	268.00	1 36 2 • 0 0	38 • CO	.30	.00	.00	•00	12.00	.00	12.00	.90	.10	.00	.00	.00	.00	1.00	.00	.00
1753-00	104.00	1466.00	16.50	0 ل ه	17.00	5.50	.00	5.00	.00	27.50	• 00	·20	•8 D	1.00	•00	.00	1.00	. O Ó	•00
1857.00	44.00	1510.00	12.00	- 60	.00	6.50	.00	.00	23.00	29.50	1.50	•00	1.00	1.00	.00	.00	•00	•00	.00
1901.00	20.00	1530.00	12.00	.00	.00	4.00	• 00	.00	.00	4 • 00	1.00	•00	1.00	.00	•00	.CO	•00	1.00	.00
1921.00	56.00	1586.00	41.50	•00	2.50	• 0 0	.00	6.00	.00	8.50	• 00	•00	1.00	•20	.00	.00	.00	•5C	.00
1977.00	82.00	1668.00	33.00	• u 0	8.00	• O O	.00	5 • 0 0	.00	13.00	.00	.00	1.00	1.00	- 00	.00	.00	.50	.00
FEY FOR S					V - 65	:⊭ENTEO GF	OWITO		* K	EY TO	ALUES	FOR	RUNN	ING #A	TER				
11 - CLA 111 - SAN	Y AND S	RAVEL	RS	A 1	/I - PE	INDING GRO	RASH		. 2	= OR1 5 = MOI 0 = WEI	TZI		= RUI = FL0		WATER				

LPPER SALT CREEK \$1 CONTRACT NUMBER 68-404-2S CHICAGO, ILLINOIS

PROGRESS AND PRODUCTION

RELATIVE FREQUENCY OF SOIL TYPE OURING THE WEEK CONNEGURS - HOURSZWEEK BY CAUSE STATION TUNNEL CUMUI AT START RATE FEET CF REEP FT/WK LATE STATION TUNNEL CUMUL. PROE
AT START RATE FEET TO HRS IN CHILLO EXCAV CONVEYOR MUCK HISC ADMIN DOWN I II III IV V VI VII VIII RUNNING
F "EEP FT/AM CATE "EEK EQUIP TRANS HOURS "ATER» 2659.00 154.00 1622.00 38.5J .00 5.50 .00 6.0₀ 11.50 .00 .00 1.60 1.00 .00 .CO .70 .DG -00 2213.00 180.00 2002.00 37.00 -00 -00 • C D .00 3.00 IO.00 13,00 -50 -2 D .50 .2ú . 00 .CO 1.DO . 00 -00 2393.00 73.00 2075.00 34.60 1.00 .00 .00 14.00 .00 .20 1.00 .CO .00 2466.00 164.00 2239.00 41.00 4.00 • UD 2.50 .CO I.DO - 00 7.00 -40 -10 .60 .1G .00 ٠.00 - 00 . 50 .00 2630.00 35.00 2274.00 19.00 .6D 3.00 . C O +00 .00 25.00 .40 -10 .10 .00 .00 .00 .00 . 50 2665.00 64.00 2338.00 23.00 . 10 .00 .00 .00 2.00 19.00 21.00 1.00 .90 .00 .00 .00 .00 .00 1.00 -0.0 2729.90 175.00 2513.00 31.00 •00 .00 16-00 1-00 ۵0ء .00 .00 .00 1.00 6.00 6.00 -00 .00 2.00 • 0.0 .00 2904.00 320.00 2833.00 45.00 5.00 1.00 .00 .50 -00 .00 3224.00 208.00 3041.00 25.00 11.00 1.00 .00 1.00 •00 .00 6.00 .00 a C.D 5.00 •00 -00 ann 1ann • 00 .00 3432.00 308.00 3349.00 .00 .00 .00 .00 8.00 11.00 . ŝŪ •00 .20 .00 .00 .00 1.00 .00 3740.00 276.00 3625.00 37.00 - 0.0 3.00 - 0.0 .CO 10.00 .00 13.00 .90 •1G .OC 1.OC +C0 .C0 .OC 1.00 ۰00 .00 4016.00 228.00 3853.00 31.00 .00 1.00 .00 .00 .00 .00 9.00 10.00 19.50 . B Ö .20 .00 .00 .00 4244.00 376.00 4229.00 45.00 .uo .00 .00 . u0 .00 .00 .co 1.00 .00 .00 .00 .70 .90 -10 .00 .00 4620.0C 216.00 4445.00 22.CO .00 .50 .50 :00 a di D - 00 a C O - 60 6.00 10.00 16.00 - 80 -nn -20 • 00 . DD 4836.00 280.00 4725.00 34.00 .00 2.00 .00 6.00 .20 - 25 .00 .00 .00 .80 .00 .00 5116.00 152.00 4877.00 23.50 .30 -00 nn .00 3.50 11.00 14.5Ô .80 .00 .20 ۰00 •00 .00 .00 . 00 .25 5268.00 300.00 5177.00 37.60 .JO .00 .00 .CO 1.DO .00 .00 10.00 • 00 1.00 11.00 1.00 .OC .00 .00 .00 .00 5568.06 304.00 5481.00 37.00 .40 .00 2.00 13.00 1.00 .00 1.00 . OG 5872.00 400.00 5681.00 45.00 .00 .00 •C0 • 00 .00 • C O 1.00 4.00 .00 5.00 1.00 .00 . DÓ •00 .00 1.00 6272.00 286.00 6167.00 33.50 - 00 .00 .00 .00 6.50 10.00 16.50 1.00 -00 .00 .00 .00 .00 .00 .20 .40

Appendix A-2. (Continued)

LPPER SALT GREEK #1 CCNTRACT NUMBEP 68-404-2S CHICAGO, ILLINOIS

						HOURS - I	AUSE	/WEEK			FELA	3v1T		ENCY THE W		IL T	PE O	UR I NG	
STATION AT START CF WCEK	FT/wK	FEET TO	HRS IN	SHIELO	EXCAV EQUIP	CONVEYOR	HUCK TRANS	HISC	AOMIN	TOTAL COWN HOURS	ı	11	111						RUNNING WATER+
		6345.DC		عد.		•00		19.00		19.00			1.00				•00		
6736.00	100.00	6445.DC	30.00	•00	3.00	•00	. 60	12.00	5.00	20.00	•00	•00	1.00	.00	• GO	.00	.00	1.00	•60
6836.00	46+00	6493.00	25.00	3 + 10	7.00	.00	• 06	13.00	.06	23.00	•60	.00	1.00	.00	•00	.00	•00	1.00	•60
6864.00	26.00	6519.UC	17.CO	• 00	12.GO	•00	•60	7.00	6.00	27.00	•00	•00	1.00	-20	-60	•00	•00	1.00	•00
6910.00	46.00	6565.00	26.CO	•70	•00	12.00	•60	8.00	•00	20.00	•00	•00	1.00	. OL	•00	.00	.00	1.00	•00
6956.00	98.00	6663.00	33.00	• 99	•00	3.00	• 00	4.00	8.00	15.00	• 00	•00	1.00	•00	•00	•00	•00	1.00	•00
7054 •00	162.00	6825.00	36.CD	.00	•00	•00	• 00	12.00	•00	12.0G	-00	•00	1.00	.00	•00	.00	•00	1.00	•00
7216.00	246.00	7673.00	44.CO	•00	.00	.00	.CO	6.00	•00	6.00	• ÓO	.00	1.00	•00	•00	.00	1.00	•0Ó	•00

PEY FOR SOIL TYPES

I - SILT AND CLAY

II - CLAY AND SAND

VI - PEAT AND TRAS:

III - SAND AND GRAVEL

VII - COMESS VE GROUND

IV - COBBLES AND BOULDERS

VIII - RUNNING GROUND

VIII - RUNNING GROUND

**EY TO VALUES FOR RUNNING WATER

0 = ORY **75 = RUNNING WATER

1 = FLOODED

**SD = WET

LPPER SALT CREEK #2 CONTRACT NUMBER 66-405-25 CHICAGO, ILLINOIS

PROGRESS AND PRODUCTION

					6081	HOURS -	AUSE			_		A T1VE		UFNCY THE N	EEK				
STATION AT START CF WEER	FT/#K	CUMUL. FEET TO LATE		SHIELO	EXCAV	CONVEYOR		нісс	AUMIN	TOTAL LOWN FOURS	1	11	111	Ιv	٧	٧I	VII		RUNNIN WA TER
75 - 00	46.00	46.00	40.00	•60	.00	.00	.00	•00	.00		1.00	•00	•00	•90	•00		1.00		.00
27.00	23.00	69.00	17.CO	• 30	-00	.00	•00	•00	•30	.00	1.00	•00	.00	•00	.00		1.00		•00
75 +00	103.00	172.00	3C • GO	. 10	.00	B.00	• 00	8.UO	•00	16.00	1.00	•00	•00	•00	.00	.00	1.00	•00	•00
173.00	213.00	385.0C	41.00	•00	5.00	.00	• 60	.00	•00	5.00	1.00	•00	•00	• 30	•00	.00	1.06	•00	•00
351.00	578.00	963.00	55.60	0 ب	6.00	•00	-00	2.00	•00	8.00	1 • GO	•90	•00	.20	.00	.00	1.00	• 00	•00
969 •N n	159.30	1122.00	14.00	- 00	6.00	•90	.00	18.00	.00	26.70	1.00	.00	•00	•00	•00	.00	1.00	.00	.01
1129.00	549.00	1671.00	41.00	•30	•00	•00	• 00	26•00	•00	26.00	1.00	1.00	1.00	1.00	•00	•00	1.00	•00	•50
1665.00	218-00	1889.00	16.00	• 10	•00	.00	•00	9.50	18.50	28.00	1.00	•00	•50	•50	•00	.00	1.00	.00	.0
1963.00	495.00	2384.00	36.00	• 30	•00	•00	•00	6.00	11.00	17.00	1.00	•00	•00	.10	-00	•00	1.00	• 00	•Î
2406.00	622.00	3006.00	51.00	.00	•00	.00	• 00	9.00	.00	9.00	• 00	1.00	•10	•20	.50	.00	1.00	•00	•00
3028.00	104.00	3110.00	5.00	•00	13.00	•00	•00	•00	•00	13.00	• 00	•50	•00	•00	•00	•00	1.00	.00	•00
3132.00	570.00	3660.00	39.00	• u0	•00	•00	0 ن	5.00	•00	5.00	• 00	•50	•00	.00	•60	•00	1.00	•00	. •00
3710.00	411.00	4091+00	31.00	•00	• 00	•00	.00	10.00	1.00	17.00	1.00	•00	•00	• 30	• 00	•00	1.00	.00	•00
4129.00	513.00	4604.00	35.00	••0	•00	•00	•00	8.00	•00	8.00	1.00	•00	•00	•00	•00	•00	1.00	-00	•00
4650.00	368.00	4972.00	25.00	•00	.00	• 00	•00	8.00	7.00	15.00	1.00	•00	•00	•70	•00	.00	.00	.00	•00
5303.00	341.00	5 31 3 • 00	24.00	•110	•00	.00	. CO	10.00	.00	10.00	1.00	•00	•00	•00	.00	•00	•00	•00	.80

UPPER SALT CPEEK #3 CONTRACT NUMBER 68-406-25 CH1CAGO, 1LLIND15

					DOWN	HOURS - 1		WEEK			REL	AT1 VE	FRED	JENCY THE &		IL T	YPE O	UR1NG	
				======				=====	=====		====				=====	====		=====	
STATION		CUMUL.		51/3510	E V C A V		MILEN	W7.56		TOTAL				1	٧				
OF WEEK		DATE	WEEK	241FF0	EQUIP	CONVEYOR	TRANS		AUMIN	HOURS	1	11	111	1.4	٧	A I	AII	ATII	RUNN1NG WATER*
				======			=====	=====			=====	====:	:===:	=====	=====	====			
4681.00	20.00	20.00	10.00	.00	6.00	۰00	•00	24.00	.00	30.00	1.00	.00	•00	.00	.00	.00	1.00	,00	.00
4701.00	84.00	104.00	28.00	• 00	.00	8 - 00	.00	3.00	1.00	12.00	1.00	۰00	-00	1.00	•00	.00	1.00	•00	.00
4785.00	164.00	268.00	30 +00	.00	2.00	.00	•00	8.00	.00	10.00	1.00	.00	•00	•50	.00	.00	.00	.00	.00
4949.00	120.00	388.00	23.00	.00	15.00	•00	•00	2.00	.00	17.00	1.00	•00	•00	1.00	.00	.00	1.00	.00	.00
5069.00	138+00	526+00	31.00	.00	•00	.00	.00	9.00	.00	9.00	1.00	•D0	.00	1.00	•00	•00	1.00	.00	.00
5207.00	152.00	678.00	22.00	•00	•00	.00	•60	1.00	.00	1.00	1.00	•00	-00	.40	• D O	.00	1.00	.00	.00
5359.00	164.00	842.00	31.00	•00	•00	.00	.00	1.00	8.00	9.00	1.00	•00	•00	•20	• 00	•00	•00	.00	.00
5523.00	268.00	1110.00	36.00	•00	•00	-00	- 00	3 • 00	1.00	4 - 00	1.00	.00	•00	.70	•OO	•00	1.00	.00	.00
5791.00	120.00	1230.00	14.00	.00	.00	.00	•00	2.00	24.00	26.00	•20	1.00	.00	- 40	• 00	+00	•00	.00	•00
62.00	107.00	1337.00	13.00	• 00	.00	•00	.00	27.00	.00	27.00	•50	•00	•50	.00	.00	.00	.00	.00	.00
169.00	80.00	1417.00	17.00	.00	7.00	16.00	•00	• 00	.00	23.00	. 90	.00	-10	.00	.00	•00	1.00	.00	.00
249.00	164.00	1581.00	30.50	.00	•00	5.50	.00	4 • 00	•00	9 - 50	1 • 00	.00	.00	.00	.00	.00	1.00	.00	.00
413.00	200.00	1781.00	29.00	• 00	•00	•00	•00	8.00	.00	8.00	1.00	.00	•00	.00	•00	٥٥٥	1.00	.00	.00
613.00	112.00	1893.00	20.00	• 00	•00	4 - 0 0	•00	2.00	6.00	12.00	I.00	.00	.00	.00	.00	•00	1.00	•00	•00
725.00	260.00	2153.00	29.00	•00	•00	•00	•00	3.00	.00	3.00	1.00	.00	•00	.00	.00	.00	1.00	.00	•00
985.00	324.00	2477.00	40.00	•00	•00	•00	.00	.00	.00	.00	1.00	.00	.00	.00	•00	•00	1.00	.00	.00
1309.00	252.00	2729.00	27.00	.00	•00	.00	.00	5.00	8.00	13.00	1.00	•00	•00	.00	.00	•00	1.00	•00	•00
1561.00	300.00	3029.00	34.50	•00	•00	•00	• 00	5.50	.00	5.50	1.00	.00	.20	.00	.00	.00	.80	.00	+00
1861.00	280.00	3309.00	31.00	.00	.00	1.00	•00	-00	8 •00	9.00	1.00	٠00	•16	.00	•00	.00	.96	•00	+00
2141.00	376.00	3685.00	38.00	•00	1.00	1.00	.00	.00	.00	2.00	1.00	.00	•00	.00	.00	•00	1.00	.00	.00
KEY FOR S					V - CE	MENTED G	ROUND		÷Κ	EY TO	/ALUES	FOR	RUNN	ING WA	TER				
II - CLA III - SAN IV - COP	O AND 6		R5	V 1	I - CO	AT AND TE HESIVE GE UNNING GRO	ROUND			= 0R1 5 = M01 0 = WE1	I S T		= RUP = FL0	INING OODEO	WATER				

PROGRESS AND PRODUCTION

UPPER SALT CREEK #3 CONTRACT NUMBER 68-406-2S CH1CAGO, ILL1NOIS

STATION	TUNNEL	CUMUL	PROÓ		00₩1	HOURS - 8 Y C		===== WEEK		TOTAL	REL	1 T 1 VE	FREQU	ENCY THE W		IL T	YPE O	UR1NG	
AT START OF WEEK	RATE FT/WK	FEET TO DATE		SH1EL0	EXCAV EQUIP	CONVEYOR	MUCK TRANS		AOMIN	DOWN HOURS	1	11	111	1 V	٧	٧I	VII	VIII	RUNNING WATER*
2517.00	212.00	3897.00	24.00	.00	.00	3 • 00	.00	•00	13.00	16.00	1.00	.00	.00	.00	.00	.00	1.00	.00	.00
2729.00	400.00	4297.00	37.00	• 00	.00	3.00	.00	.00	.00	3.00	I.00	.00	.00	.00	.00	.00	1.00	.00	.00
3129.00	288.00	4585.00	38.50	•00	•00	•00	.00	1.50	.00	1.50	1.00	.00	.00	.00	.00	.00	1.00	.00	.00
3417.00	141.00	4726.00	24.00	• 00	.00	•00	.00	-00	16.00	16.00	1.00	.00	.00	•00	-00	.00	1.00	.00	•00
3558.00	80.00	4806.00	15.00	4.00	.00	.00	.00	5.00	16.00	25.00	.50	.50	.00	.00	.00	.00	1.00	.00	.00
3638.00	168.00	4974.00	32.00	•00	.00	•00	.00	8.00	.00	8.00	1.00	. 30	.00	.00	•00	.00	1.00	.00	•00
3806 • 00	292.00	5266.00	37.00	.00	.00	.00	.00	3.00	.00	3.00	1.00	.00	.00	.00	.00	-00	1.00	.00	.00
4098.00	316.00	5582.00	36 • 50	•00	.00	.00	- 00	3.50	- 00	3.50	1 • 0 0	.00	.00	.00	.00	•00	1.00	.00	.00
4414.00	256.00	5838.00	31.00	.00	.00	۹.00	.00	5.00	.00	9.00	1.00	.15	.15	.00	• 00	.00	1.00	.00	•00

*ASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMBER 1FOG21 FZA PENTAGON OUTBOUNF NASHINGTON, 9.C.

						- 29U04P	AUSE	_						THE W	EEK				
							=====	=====			===:		:		=====	====		=====	
STAT10N	TUNNEL	CUMUL.	PPCC							TOTAL									
IT STAPT	RATE	FEET TO	HRS IN	SHIELD	EXCAV	CONVEYOR	MUCK	MISC	ACHIN	DO2N	1	11	111	1 V	٧	V 1	V11	V111	RUNN1NG
CF WEEK	FT/hK	CATE	₩ C E F		E CU 19		TEANS			HOURS									WATER
FEEDERS	======:	==== = ====	======		:-:	=======	=====			======		=====	=====		=====	====:		=====	
7050 • 5 7	67.00	67.00	78.49	•60	.05	.00	. 33	9.68	•00	10.01	1.00	1.00	•00	•00	•00	•00	1.00	•00	•00
6963.57	46.19	113.19	27.28	•50	3.00	.70	•00	2 • 5 2	•00	6.72	1.00	1.00	•00	•00	-00	•60	1.00	•00	•00
6927.38	174.89	288.08	83.68	•58	.58	2.42	1.42	3 - 5 7	• 25	8.82	•00	1.00	-00	•00	•00	•00	•00	•00	•00
6762.49	51.42	339.50	21-65	•30	- 30	• G O	•25	5 - 10	•00	5.35	•c0	-00	1.00	1.00	-00	.00	-00	1.00	1.00
6711.07	213.94	553.44	69.83	1.50	. 75	-00	•25	1.17	•30	3 - 6 7	1.00	•00	1.00	1.00	.00	.00	1.00	•00	.00
6497.13	54.37	607.81	23.34	•30	•00	.33	1.00	1.50	•25	3.16	1.00	•00	1.00	1.00	•00	•00	1.00	1.00	.00
6442.76	2.47	610.28	7.25	•00	.00	• 2 5	•00	•00	•00	•25	1.00	1 -00	-60	• 96	-00	•00	1.00	1.00	•00
6440 - 79	91.74	702.02	37.15	4.00	•00	1.10	•60	6.00	•25	11.35	1.00	1.00	1.00	1.00	•00	•60	1.00	•00	-00
6348.55	133.57	635.57	77.55	3.20	3.00	•00	•00	10.75	•00	16.95	1.00	.00	1.00	1 •00	•00	•60	1.00	1.00	-00
6214.98	261.95	1097.52	97.42	•00	•00	•30	1.00	9.08	•50	10.58	1.68	•00	1.00	1.00	•00	.00	1.00	•00	1.00
5953.03	293.27	1390.79	95.76	5.33	•25	. 5 0	.33	8.08	٠2 °	14.74	1.00	-00	1.00	1.00	•00	-00	1.00	•00	1.00
5659.76	17.47	1408.25	16.92	•00	•00	•00	.00	.33	.25	•58	1.00	•00	1.00	1.00	•00	•00	1.00	.00	-00

PROGRESS AND PRODUCTION

WASHINGTON METROPOLITAN AREA TRANSII AUTHORITY CONTRACT NUMBER (FOO2) FZA PENTAGON INBOUND WASHINGTON, O.C.

				-4		MHOURS - 8Y C	AUSE							THE	OF SO				
STATION	TUNKEL	CUMUL.	P 20 0			=======	=====	=====	=====			====	:	====	*****	====	====	=====	
AT START	FT/WK	FEET TO	HRS 1K		FAIITA	CONVE YOR	TOAM				1	11		14	٧				RUNN ING
							=====	======	=====		=====	====	:====	=====	=====	====	====		=======
7141.90	7.50		9.50	•00	•00	-00	• 00	-00	-00		1.00						1.00		
7139.90	6.80	14.30	8.28	•00	•22	1.00	•00	•00	.00	1.22	1.00	1.00	-00	.00	.00	- 00	1.00	.00	.00
7127.60	24.96	39.26	30.11	•22	-67	-00	•00	.00	.00	.89	1.00	1.00	.00	.00	•00	.00	1.00	.00	- 00
7102-69	2.42	41.68	R.90	1.60	-00	-00	-00	-00	-00	1.60	1.00	1.00	-00	.00	.00	- 00	1.00	.00	1.00
7100.22	17.21	58.89	28.50	11.50	2.00	2.30	• 00	۹.00	.00	19.80	1.00	1.00	•00	-00	-00	.00	1.00	.00	- 00
7083.01	39.45	98.34	3R-20	•00	•00	.00	•00	2.80	-00	2.80	1.00	1.00	•00	•00	•00	•00	1.00	.00	1.00
7043.56	61.96	160.30	38.00	•00	•00	-00	•00	4.50	.00	4.50	1.00	1.00	.00	. 00	-00	.00	1.00	.06	1.00
6981:60	38 - 30	198.60	22.70	-00	1.90	.00	.00	.90	-00	2.80	1.00	1.00	.00	.00	•00	.00	1.00	.00	1.00
6943.30	49.63	248.23	26.68	9.60	-00	.00	• 00	2.20	.00	6.80	1.00	1.00	-00	•00	•00	-00	1.00	•00	1.00
6893.67	41:07	ZR4-30	38.60	1.00	-00	1.00	.30	-10	.00	2.40	1.00	1.00	-00	-00	.00	•00	1.00	•00	1.00
6852-60	47.19	336.99	38.42	.75	.92	.00	-00	4.91	•00	6.5R	1.00	1.00	-00	.00	•00	.00	1.00	.00	1.00
6805.46	146-66	483-10	79.95	2.75	.00	1.25	-00	16.80	.25	21.05	•00	1.00	-00	.00	•00	.00	.00		1.00
6658.80	189.84	672.94	72.42	1 - 30	-00	.50	.53	1.75	.00	4.08	. 00	1.00	1.00	•00	.00	•00	. 00	.00	1.00
6468.96	167.03	839.97	72.05	5.70	1.00	5.00	•00	5.25	.00	16.95	• 00	1.00	1.00	1.00	•00	•00	•00	1.00	
6301.93	69.22	909.19	44.55	•00	.00	-00	-00	4.75	•20	4.95	.00	1.00	1.00	1.00	•00	.00			1.00
6232.71	104.07	1013-26	61.77	.00	.20	1.33	• 00	8.20	.00	9.73	1.00	1.00	1.00	1.00	.00	.00			1.00
6128.64	27.17	1040.43	17.50	•00	•00	•00	.00	1.00	.00	1.00	1.00	•00	1.00	1.00	•00				1.00
6101.47	2.51	1042.94	6.50	•00	•00	-50	-00	2.00	.00	2.50	1.00	.00	1.00	1.00	•00				1.00
6098.96	106-37	1149.31	63.03	1.80	.00	8.00	2.75	19.42	-50	32.47	1.00	.00	1.00	1.00	.00				1.00
5992.59	170.31	1319.62	89 - 90	1.20	1.00	1.80	3.05	2.35	.20	9.60	1.00	1.00	1.00	1.00	•00				1.00
KEY FOR S	60 IL TWO	FS																	
1 - SI	T AND	LAY			V - CE	MEN7ED GR	OHED		486	EA 10 A	AL UES	FOR	RUNNI	ME NI	TER				
II - CLA	V AND	ANO				AT AND TR			٥	= DRV		. 75	= 815	MINE	WATER				
10 - COS		RAVEL 10 BOULDE	RS			MESIVE GR NNING GRO			-25	S = MO1	57		= FL0						

WASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMBER 1F0021 F2A PENTAGON INBOUND WASHINGTON, O.C.

OUNHOURS - HOURS/WEEK RELATIVE FREQUENCY OF SOIL TYPE OURING BY CAUSE THE WEEK STATION TUNNEL CUMUL. PROD AT START RATE FEET TO HRS IN SHIELD EXCAV CONVEYOR MUCK MISC ADMIN DOWN I II III IV V VI VII VIII RUNNING OF WEEK FIJUK OATE WEEK EQUIP TRANS HOURS WATER®

PROGRESS AND PRODUCTION

WASHINGTON METROPOLITAN AREA TRANSIT AUTHORIȚY CONTRACT NUMBER 1F0021 FCA BRANCH ROUTE GUTCOUNC WASHINGTON, C.C.

	_=:	C O W	NHOURS - EY C =======	AUSE							ENCY THE W	EEK				
STATION TUNNEL CUMUL. AT START RATE FEET TO CF.EER FT/WM CATE	HRS IN JHI	E UU1P		TRANS			TOTAL LOWN FOURS	1	11 =====	111		v =====				UNNING MATER*
8605.69 69.89 69.89	54.C8	00. 0ن	.00	.00	1.92	.50	2.42	. 20	•50	.30	.00	•00	.00	.20	.00	•00
8535.86 136.63 206.52	73.67	.00 5.50	2 • 8 3	1.42	9.08	.00	18.83	• 1 Ū	•5 G	.30	.10	.00	.00	.10	.00	.00
8399.17 27.32 233.84	33.08	.ou .co	.42	- 17	. 3 3	.5r	1.42	۰ ۵0	.70	.20	-10	.00	.00	.00	.00	.00
8371.85 19.92 253.76	16.50	-30 -00	• C O	. CO	.00	.00	• 70	• 1G	.70	e 2 0	.00	.00	.00	٠10	.00	.00
8351.93 202.84 456.60	62.00	.50 .33	4.25	1 + 67	3.75	.5C	12.00	.00	.86	.20	.00	.00	.00	.00	.00	.00
6149.09 154.17 610.77	48 - 67 4	.00	• 3 3	. 40	1.50	.00	5 . 8 3	-10	•60	.20	.01	.00	.10	-10	.00	.00
7994.92 265.54 876.31	87.42	.63 .00	1.00	• CO	4.00	.75	6.58	.00	.5 C	.30	•1G	•00	- 10	.00	•00	.00
7729.38 178.93 1055.24	66 - 47 2	2 - 5 3 - 0 0	15.92	• £C	5.58	.00	24.03	.00	.7C	-20	•10	.00	.CO	.00	.00	.00
7550.45 311.93 1367.17	96 • 00 1	1.50 4.17	Z. C8	• OC	4.75	.00	12.50	.00	.60	+3 G	.19	.00	.00	۰00	• OC	.00
7238.52 28C.90 1648.07	87.58	.50 .75	.OC	+ 41	. 75	.50	2.41	• 60	.50	.30	.2C	.00	.CO	• 0 0	•00	.00
6924.85 269.76 1917.83	62.25	.75 .00	3.50	1.33	.17	.30	5.75	.00	.80	-20	.00	.00	•€0	.00	.00	.00
6655.09 324.66 2242.49	65.84	0 1.00	1.08	4.08	3.25	.25	9.66	• 60	.70	.20	.10	.00	.CO	.00	.00	.00
6330.43 324.53 2567.02	7 C • 5 8	•30 1•17	• 0 0	.42	1.33	.00	2.92	+ CO	.5 C	• 3 O	.20	.00	.CO	.00	.00	.00
6005.90 244.58 2811.60	75.84 5	.33 .50	.00	2 . 83	7.50	.5C	16.66	.40	.40	.10	• 1 0	.00	.00	.40	• 00	•00
5761.32 52.20 2863.80	42.25 5	3.58	.00	+42	1.58	·•50	11.25	•60	-10	•20	• 1 0	.00	.00	.60	.00	.00
5709.12 74.40 2938.20	31 + 25 5	3.00 3.00	.00	• 50	5.25	.00	13.75	.90	-90	-10	.00	•00	.00	• 90	.00	+00

KEY FOR SOIL TYPES

1 - SILT AND CLAY

V - CEMENTED GROUND

11 - CLAY AND SAND

VI - PEAT AND TRASH

111 - SAND AND GRAVEL

VII - COMESIVE GROUND

1V - COBBLES AND BOULDERS

VIII - RUNNING GROUND

**KEY TO VALUES FOR RUNNING WATER

D = ORY

.75 = RUNNING WATER

1 = FLOODED

**TO VALUES FOR RUNNING WATER

.75 = WINNING WATER

.75 = WINNING WATER

.75 = WINNING WATER

.75 = WINNING WATER

VASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMBER 1FOCO1 FZA BRANCH ROUTE 1ABOUND VASHINGTON, S.C.

							AUSE							JENCY THE W	EEK				
							=====	=====			===:				=====	====:			
	TUNNEL T RATE FT/WK				EQUIP	CONVE YOR	TRANS			HOURS	1	11		1 v	٧				RUKNIN WATER
						-													
6613 -5	3 17.31	17.31	14.92	• .0	• 00	1.00	•00	1.58	•0C	2 • 5 8	.03	1.00	1.00	1.00	• CC	- CO	• 00	•00	•00
8596 • 2	84.73	102-04	75 - 91	- 50	.00	2.17	•00	8 • 4 2	•00	10 •5 9	- 30	1 -00	•50	•2b	•00	.00	. 20	•00	•co
8457.9	37.27	139.31	26.09	•33	.00	2.00	4.68	2.58	.25	8.91	.SC	•6 D	-30	.00	-00	•00	. 40	•00	•00
6420 •6	7 188.24	327.55	65.50	1.25	.00	4.67	2 • 58	4 • 25	•25	13.00	1.00	•5 C	-4C	.5 ī	.00	•00	.79	• 00	-00
8232.4	3 194.61	522-16	66 - 25	6.60	1.83	, • 2 5	. 91	2.75	.sr	12.24	.83	.40	-30	• 2 C	•00	- 30	. 80	•00	•00
8037.8	2 164.88	687.04	55.42	• 90	.25	• 6 0	- 33	7.5C	•0C	8.08	•85	-20	.40	• 9 C	.00	.30	. 80	.00	•00
7872.9	4 306.93	993.97	103.83	•00	.00	3.50	.75	2.92	•5 e	7.67	• 70	•20	•50	-50	•00	-10	.70	.20	.00
7566.0	287.49	1261.46	99.33	•80	.00	1.00	• CO	7 - 67	•5 C	9.17	.sc	-40	•60	•7 C	•00	•C0	• 5 0	.00	•00
7278 -5	300.15	1581.61	97.75	• 30	.00	.00	1.67	8.58	•5n	10.75	• 30	•60	.80	•8 C	•00	-00	.30	•90	.00
6978.3	7 98.05	1679.66	64 .8 2	• 30	• 00	1.00	• 75	4 • 9 3	1.50	8.18	-20	.e C	•50	•1C	•C0	. CO	. 20	- 00	-10
6860.3	2 236.32	1915.98	89.83	•00	3.00	- 42	.00	6.00	1.25	10.67	.40	.70	•6 D	-26	•00	•00	.40	• 40	-20
6644.00	223.54	2139.52	96.92	• ü0	•00	1.50	1.00	9.08	•00	11.56	•40	•70	•60	• 4 C	• CO	.00	.40	.00	-50
£426.1	2 252.05	2391.57	82.49	•~D	•00	1.42	2.17	3.92	.00	7.51	•40	.EO	.50	.30	•c0	.co	.48	.00	- 760
6174.0	7 169.37	2560.64	80.58	1.58	.00	1.17	2 • 00	7 - 6 7	•00	12-42	• 10	•90	•60	.80	.00	.00	.10	.60	1.00
6005.00	34.74	2595.38	38.16	•67	•00	.00	•00	3.67	.00	4.34	• 70	•40	.80	•90	+00	•00	.70	.00	•50
5970 •2	5 249.63	2645.01	119.07	2.18	•00	-75	- 58	11-17	•0C	14 - 68	•90	-30	.80	• 9 G	.00	- CO	. 80	.00	.00
5720 -6	3 89.66	2934.87	51.17	• 30	.00	.33	•C0	1.25	•25	1.83	1.00	•00	•30	.90	•00	•00	1.00	.00	•00

KEY	FO	R	SOI	LT	YPE	s		
1	-	SI	LT	AND	Ct	. AY		
11	-	CL	AY	AND	1 5/	NO.		
111	-	SA	NO	AND	GF	2 A V	EL	
T W	_		001				0111	0505

V - CEMENTED GROUND
VI - PEAT AND TRASH
VII - COHESIVE GROUND
VIII - RUNNING GROUND

*KEY TO VALUES FOR RUNNING MATER

0 = DRY .75 = RUNNING WATER .25 = MOIST 1 = FLOOGED .50 = WET

PROGRESS AND PROCUCTION

NASHINDTON HETROPCLITAN AREA TRANSIT AUTHORITY CONTRACT NUMBER 152012 FIE NORTH OUTBOUNU NASHINGTON, 2.C.

					-	1HOURS - 1							FF L Q U	THE W	EEK				
STATION AT START CF meek	TUNNEL RATE FT/WK	CUMUL. FEET TO CATE			E GU1P	C GNVE YOR	TRANS		ACH1N	TOTAL COWN POURS	I	11	111		v				RUNNING WATER+
========			=======	======	=====		=====			======									
1352.00	18-00	16.05	39.00	- 10	•00	•00	.CO	.00	•00	•00	-50	-10	•40	•00	•00	•00	.50	• 00	.00
1334 - 00	21.00	39.00	38.90	• 00	•00	• 00	3 • D ö	3 - 00	•00	6.36	•50	.1 C	• 4 0	•00	• CO	•C0	• 5 0	.00	•00
1313.06	101.00	140.00	74 - 30	•00	.00	.00	1.00	.67	•00	1 • 6 7	•\$0	-10	•40	.30	•00	•00	.50	.00	•00
1212.00	142.30	282.00	79.40	9.65	.00	• C D	-00	.00	6.92	16.57	•30	•20	.40	.10	.00	.00	.30	•00	•00
1070.00	84.00	366.00	74.80	9.33	.00	.00	- 60	8.33	•00	17.66	.40	•30	•30	• oc	.cc	.CO	. 40	•20	•20
986 .00	52.On	918.00	41.30	•00	•00	.00	• 60	2.17	•00	2.17	•8C	-00	-10	•0c	• 00	.10	.80	.20	•00
934 •00		•	77.80	1.50	•00	• 0.0	• 00	6.67	.00	8.17	.80	•0ċ	•2°C	•00	•00	•00	-80	.10	•00
											•70	•00	•30	•00	.00	.00	.70	-16	-10
852.00	105-00	605.00	95 •80	5 • 25	•00	.00	•00	2.50	•00	7.75									
747 .OC	31.00	636.00	44.70	2.42	• CO	. C O	• CO	9.92	-00	12.34	•70	•20	•00	• 10	• CO	.10			
716 -00	73.00	709.00	62.60	• ≎0	•00	.00	.00	3.91	•00	3.91	•70	•Ī0	•20	• O C	.co	.00	. 70	.10	.10
643.00	24.00	733.00	41.80	0 ن ه	.00	•00	• 00	7.67	•50	8.17	.40	•00	•6 0	• O C	•C0	•00	- 40	-10	•00
619.00	67.00	800.00	48.30	7.08	.00	.00	•00	1.67	•00	8.75	-6 O	 •10	-30	.00	.00	.00	.60	.10	•00
552 .CO	74.03	874.00	49.13	1.50	.00	.00	5.50	.92	.00	7.92	-60	10	.30	. OC	00	•00	.60	: :10	.00
						•00	•00	3.08	7.33	11.58	. Sn	•20		•30	-60	.00	.50	•10	00
478.CO	76.00		45.40	1.17	•00											•00			
402.00	25.00	975.00	19.00	• 30	•00	•00	•00	•00	.00	•00	. 50	•10	•40	•00	•00	•00	•50	•10	-00

WASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMBER 150012 F16 NORTH 1820UNO WASHINGTON, 0.C.

						HOURS -	AUSE					TIVE		THE W	EEK				
				======	======		=====	=====			====	=====	=====			====			
STATION AL START	RATE	CUMUL.	PPOE	CHIELD	EVEAU	CONVEYOR	MILCK	MIEC	ACMIN	LOWN	I	II	111	7 M	v	VΙ	u T T	UTTT	RUNNING
CF LEEV		EATE	WELF	SHILLO	EGUIP	CONTETOR	TRANS		AOFIN	HOURS	1	11	111	1.4		4.7	411	*111	#ATER*
========	======	. = = = = = = :		======			=====				=====		=====	=====	=====	====		=====	
1353.00	32.00	32.00	55.00	.00	- G O	.00	.00	1.00	• 10	1.00	. 50	*CC	» 4 D	· 10	-30	+00	- 50	• no	1.00
1326.00	143.00	175.00	65.60	0 ب •	.CO	.00	.00	6 • 42	- 00	6 • 42	.50	-10	-40	.10	.00	.00	.50	.00	.50
1163.00	109.00	284.00	77.20	.00	.00	.00	-00	3 - 33	- 00	3 - 33	-50	-06	.49	.10	.00	.00	.50	•00	1 -00
1074.00	69.00	353.CC	49.10	• 10	• C D	.06	۰00	ь.58	.83	7 - 4 1	•10	.2C	.70	.06	.00	.CG	.10	.20	.50
1065.00	81.00	434.00	58.50	6.25	. C C	- 00	• 00	1.75	• JC	8.00	• CO	. B C	.00	.00	.00	.10	.00	·IG	1.00
924 .Cu	32.00	466.00	64.80	.00	.00	• 0 6	. GU	11.20	. 10	11.20	.00	• 9 C	.00	.30	۰00	.00	.00	-10	1.00
892 + 60	55.00	521.00	61.50	1.25	.00	.00	.00	3.90	2 • 5 8	7 - 73	. CO	1.00	. G O	.00	-00	- CO	-00	.50	•50
837.00	81.00	602.60	62 •20	1.00	• 60	.00	.60	2.15	.00	3.75	• UO	1.00	• G O	• D G	• 00	.00	.00	.20	.10
756.00	136.00	738.00	92 • 20	2.50	.00	.00	.75	• 00	.00	3.25	. CO	1.00	-00	.00	.00	+00	• O C	• 10	•00
620.00	112.00	85 G . D O	60.70	3 - 60	+ O C	.00	.00	-00	.00	3.80	-30	1.00	.00	.OL	.CO	- 00	.00	.00	00.
508.00	98.00	946.00	58 - 10	. 10	-00	.00	. 60	4.65	1.75	6.40	.20	• 5 0	» U N	.00	- 00	•00	. 2 C	• 10	•00
410.00	27.00	975-00	24.50	.00	.00	• O O	« CO	.00	3.00	3.00	.20	نا ۵ ه	.20	.00	.00	٥٥،	.20	.10	• G O

PROGRESS AND PRODUCTION

LASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMBER 1F0012 F1P SOUTH OUTBOUNL LASHINGTON, 5.C.

	GOWNHOURS - HOURS/WEEK By CAUSL											TIVE	FREOL	ENCY THE W		CIL T	YPE O	URINE		
					======			=====	=====		====	====				=====		=====		
ADITATS TRATS TA				HIELD	EYCAV	CONVEYOR	HILEK	4155	ACHTH	TOTAL										
OF LEEP	FTZEK	EATE	WEEF	SHILLU	EGUIP	CONVETOR	TRAN		AUMIN	HOURS	I	11	III	1 V	٧	VI	VII	VIII	FUNNING MATER*	
========			:				=====	=====	======	======	=====	====		=====	====	=====			======	
3973.00	7 - 50	7.50	6.60	. 92	.00	.00	.00	8.00	.5r	9 = 42	• 00	•00	1.00	.00	-00	.00	.00	.00	.00	
3965.50	15.00	26.50	25.20	1 - 57	.00	• fi 0	.00	13.25	+00	14.82	.10	.00	.90	-00	- 00	.00	- 10	.00	.00	
3946.50	16.00	42.50	18.50	• 10	.00	.00	1.50	4.00	-00	5.50	·20	.00	03.	.00	.00	.00	.20	.00	-00	
3930.50	36.50	79.00	31.00	•00	+00	.00	• 00	2.00	.00	2.00	. 30	.00	• 70	.00	.00	.CO	. 3 Ô	. 20	.00	
3894.06	56.00	135.00	51.50	8.50	.00	-00	3 - 00	1.00	.00	12.50	-60	.00	.40	.00	•00	.00	. 50	.00	.00	
3838.00	60.00	195.00	57.40	12.30	• G O	• G G	.00	7.80	. 00	20.10	•63	-90	· 4 O	.00	•00	.00	. 50	.00	.00	
3778 -60	82.00	277.00	61.40	7 - 30	.00	• 0.0	2 • 00	7 • 1 0	.00	16.10	.80	.00	.20	.00	• G O	• G O	. 80	• 00	•00	
3696.00	76.00	353.60	78 . 60	19-60	. 3 3	.00	.00	5.00	.00	24 • 93	.70	.00	.30	.00	• 00	.00	.70	.00	.20	
3620.00	66.00	419.60	59.70	. 33	• 0 0	.00	• 00	11.50	• 00	11.83	.60	.00	.40	.00	.00	.00	o 6 0	.00	.00	
3554 • CO	I1.50	430 • 5 C		6.00	.00	- 0 0	. 00	2 • 30	.00	8.30	·60	•Û0	o 4 O	-06	.00	.00	.60	.00	•00	
3542.50	16.50	449.UD	25.70	• 60	3.00	.00	• 00	.00	.00	3.00	.50	.00	• 5 0	.00	.00	.00	.50	.00	.00	
3524.00	61.00	510.0C	62.10	•67	4.65	- G O	• 58	1.50	.00	7.40	·60	.00	.30	.10	.00	.00	·60	.00	-00	
3463.00	69.00	579.00	68.70	7 . 8 3	.00	-00	.00	1.00	.00	8.83	. 70	•00	.20	• i 0	• GO	•00	.70	· 6 0	.40	-
3394.00	17.00	596.00	16.10	6.50	.00	.00	.00	.96	• Ô O	7.40	.70	.00	.30	.00	• 00	.00	• 70	.60	.00	
3377.00		631.5C	53.70	5 - 25	.00	.00	3.58	•00	.00	8.83	.70	•00	.30	.00	•00	.00	.70	.00	.00	
3341,50		704.00	65.50	1.25	11.00	• 00	• 00	7 - 75	۰00	20.00	.60	.00	.30	• Ö O	•10	.00	- 60	-00	-50	
3269.60		804.50	77.70	.00	1.00	- 00	• 00	8.83	-00	9 - 83	- 60	.00	.30	.00	.10	.00	• 6 0	.00	1.00	
3168.50		858.00		.00	2.50	.00 1	4 - 50	1.00	.00	18.00	.60	.00	· 20	.00	-20	.00	.60	.00	1.00	
3115.00				6.33	2.50	.00	7.18	3.00	.00	19.01	•70	•20	.00	.00	.10	• G O	.70	.00	• 50	
3013.50			126.80	• 00	• 00	- 00	3.33	7.83	.00	11.16	•50	-30	.10	. 10	.00	.00	.50	.00	.00	
I - SIL	T AND C	LAY			v - cε	MENTEO GR	OUNO		0 K E	Y TO V	LUES	FOR	RUN N 1 I	4G wAY	ER					
II - CLA	Y AND S	A ND				AT AND TR			0	= ORY		.75	RUNA	ING E	ATER					

III - SANO AND GRAVEL
IV - COBBLES AND BOULDERS

VI - PEAT AND TRASH VII - COHESIVE GROUND VIII - RUNNING GROUND

WASHINGTON HETROPCLITAR AREA TRANSIT AUTHORITY CONTRACT NUMBER 1FOU12 FIE SOUTH OUTSOUNG WASHINGTON, D.C.

					COW	HOURS - BY C		WEEK			FELA	1146	F PE OL	ENCY THE W		11 1	YPE C) UR 1 NG	
STATION AT START CF meek				_H1ELO	E XCA V EGUIP	CONVE YOR	MUCK TRANS		AOM1N	TOTAL LOWN HOURS	1	11	111	Iv	v	VI.	VII	V11I	RUNNING HATER+
Z868 . 00	124.00	1209.0(86.70	3.00	8.50	.00	1.75	3.00	•00	16.25	•50	.36	.10	.10	•00	•00	.50	•00	• • • • • • • • • • • • • • • • • • • •
2764 .00	97.00	1306.00	66.50	2.00	2.00	.00	2 • 50	3.00	•00	9 • 5 U	•50	•3C	•20	.03	•00	.00	. 50	.00	1.00
2667.00	96.00	1404.00	68.70	14.50	.00	.00	.50	2.33	•00	17.33	•50	-10	•30	•10	.00	.00	.50	•00	1.00
2570.00	125.50	1529.50	83.40	5 • 42	1.00	.00	•00	5.67	.00	12.09	•50	-10	•30	•1C	•00	•00	• 50	•00	1.00
2444 •50	129.50	1659.UC	84.79	•u0	2.25	•00	•60	6.60	•00	10.85	.40	•20	.20	.2C	.co	•00	. 40	.00	•50

KEY FOR SOIL TYPES

I - SILT AND CLAY

II - CLAY AND SAND

VI - PEAT AND TRASH

III - SAND AND GRAVEL

VII - COMESIVE GROUND

IV - COBBLES AND BOULDERS

VIII - RUNNING GROUND

*KEY TO VALUES FOR RUNNING MATER

0 = 0RY .75 = RUNNING WATER .25 = MOIST 1 = FLOODED .50 = WET

PROGRESS AND PRODUCTION

NASHINGTON METROPELITAN AREA TRANSIT AUTHORITY CONTRACT NUMBER 1FC012 F18 SOUTH INCOUNO LASHINGTON, O.C.

F = 2417 110 1	0.00	•																	
					00 WHOURS - HOURS/WCEK									ENCY THE W	EEK				
					- -	:==== = ==		=====	=====		====			=====	=====	====:	:::::	=====	
STATION AT START CF WEEK	FT/WK	CATE	HRS IN	SHIELO	EXCAV EQUIP	CONVE YOR	MUCK TRANS	M1 SC	AUM1N	TOTAL LOWN HOURS	1	11	111		v 				RUNNING WATER®
:::::::	======		::::																
3971 •GC	72.00	72.00	64.00	•00	•00	.00	•00	7.50	•00	7.50	•50	.10	•20	• 2 C	• CO	•00	•50	•20	.00
3899.CO	67.00	139.00	73.90	•30	•00	•00	18.42	5.73	•00	24.15	•50	•00	•30	•20	.00	.00	.50	. 86	•00
3832 • 00	113.00	252.00	82.00	0ن.	.00	.00	•00	5.50	•00	5.50	• 70	•00	•20	-10	.00	•00			•00
3719.00	146.00	398.00	76 - 10	- 58	•00	• C O	•00	6.00	1.33	9.91	•70	-10	•20	•06	-00	•00	.70		•00
3573 •00	17C.OU	568.C0	85.60	.00	.cc	.00	•00	1.92	•00	1.92	•6.)	.00	.20	.oc		.00			•00
3463 •00	93-00	661.00	54 -40	•50	•25	•50	•00	1.33	•0C	2.08	•70					•00			
3310.00	141.00	802.00	83 .CU	• 00	•50	• 00	1.50	3.00	•00	5.00	-	.30					•60		•00
3169.00	162.00	964.00	89.20	2.83	.50	.00	•00	1.00	•00	4.33					•00	•00	.70		•50
		1114.00		• 00	•00	•00	•00	2.00	•00	2.00			-	•00 •10					
		1247.00			•00	•00	•00	.00	.00	1.00				.20				.00	
		1376.00	-		.25	•00	1.10	.83	•00 5•00	3.68				.10			.50		
•		1485.00				•00	2 • 00	.75		11.67								.00	
		1582.00					5.00	1.00		4.17						•00		.00	
2389.00	72.00	1654.00	62.30	1.17	•00	.00	2.00	1.00	• 00	4.11	-50	-20							

WASHINGTON METPOPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMBER 100091 0-9 SOUTH INCOUND WASHINGTON, O.C.

						NHOURS - By c	AUSE							THE W		IL T	YPE O	URING	
STATION AT STAPT OF WEEK	TUNNEL RATE FT/WK	CUMUL. FEET TO DATE				CONVEYOR	MUCK TRANS	HISC		TOTAL ODWN HOURS	1	11	111	ΙV					RUNNING WATER#
22168.00	28.00	28.00	94.75	.00	.00	•00													
22140.00	84.90	112.90	105.00	•00	4.00	•60	-00	8.00	.00	12.00	1.00	-00	-00	+00	.00	.00	1.00	.00	•00
22079.00	105.00	217.90	111.33	+00	4 • 17	•00	2.00	2.00	•00	8.17	.80	•00	.00	•00	.20	.00	.80	.00	•00
21974.00	83.00	300.90	106.00	1.00	4.00	.00	11.00	8.00	+00	24.00	• 90	-00	+00	.00	.10	.00	• 90	.00	.00
21891.00	78.00	378.90	93.00	•00	•00	•00	14.00	.00	.00	14.00	1.00	•00	•00	.00	.00	•00	1.00	•10	• 30
21813.00	123.00	501.90	110.00	• 00	.00	•00	21.00	4.00	+00	25.00	1.00	.00	.00	.00	•00	•00	1.00	•00	•30
21690.00	106.00	607.90	110.00	7.50	5.50	•00	2.00	5.00	.00	20.00	1.00	•00	.00	•00	•00	.00	1.00	•00	-10
21584.00	92.00	699.90	107.00	•00	•00	-00	•00	8.75	.00	8.75	1.00	•00	.00	•00	• 00	•00	1.00	•00	•00
21492.00	25.00	724.90	30.00	• 00	.00	.00	8.00	.00	.00	8.00	1.00	•00	.00	.00	.00	.00	1.00	•00	•00

KEY FOR SOIL TYPES

I - SILT AND CLAY

11 - CLAY AND SAND

III - SAND AND GRAVEL

III - SAND AND GRAVEL

VII - COMESTVE GROUND

IV - COPSLES AND BDULOERS

VIII - RUNNING GROUND

*KEY TO VALUES FOR RUNNING WATER

0 = ORY .75 = RUNNING WATER .25 = MOIST 1 = FLOODED .50 = WET



Appendix A-3

Rate of advance calculations vs. measured rate for each data set of each tunnel.

The calculation procedure includes the estimate of the learning curve exponent, equation (6.1), the intercept, equation (6.2) and their substitution in the RoA equation (6.3).



RAY AREA RAPIO TPANSIT OISTRICT CONTRACT NUMBER IMCOSI MR TUNNEL - 24TH TO FANOALL STREET SAN FRANCISCO, CALIFORNIA

WEEK	CUMPLATIVE FEFT	DOWN HOURS		SHIELO CORRECTION	EXCAVATING EWUIPMENT CORRECTION	=========	5 HOURS N SUMMATION	CUMULATIV	========	======	L MOURS CUMULATIVE
1	1 00	1.00	.75	9 • 9 3	1.50	30.15	26.22	30 • 15	26.22	8.00	6.07
2	47.50	1 + 12	.75	9.93	1 . 5 0	43+10	42.31	73 + 25	60.53	32.00	40.00
3	230.00	1.00	.75	9.93	1.50	145.82	141+14	219.07	209.67	110.00	150.00
4	737.50	1 • 9 3	.75	9.93	1.50	61.73	61.62	280.80	271.28	41.00	191.00
5	552.50	1.02	• 7 3	9 . 9 3	1 + 5 0	118.63	118.17	399.44	389.46	111.00	₹92+06
6	680.00	1.03	. 73	9.93	1 - 5 0	63.48	63.43	462.91	452.89	56.00	353.00
7	825.00	1.01	• 77	9.93	1.50	69.75	69.71	532.66	¢27.60	54.70	412.03
ρ	1385.00	1.02	.77	9.93	1.50	118+20	118.37	650.87	640.67	94.00	F06.00
9	1377.50	1.70	.76	9.93	1.50	119.01	118.90	769.P7	759.57	94.00	600.00
10	1502.50	1 • 12	.7€	9.93	1 + 5 0	54+76	54.76	824 + 14	817.83	84.00	654.00
11	1657.53	1.15	.76	9.93	1.50	67.14	67.13	891.28	880.96	77.00	761.00
12	1950.00	1 . C 4	.76	9.93	1.50	73.02	73.01	964.30	953.96	90.00	851.00
1 *	1960.00	1 - 38	.79	9.93	t • 5 0	57.28	57.2P	1021.58	1011.24	50.00	901.00
14	2050.00	1.03	.79	9.93	1.50	34.30	34.30	1055.98	1045.54	112.90	1013.00
15	2300.00	1.05	.79	9.93	1.50	95.02	95.00	1150.90	1140.54	86.00	1899.00
16	2557.50	1.76	. 79	9.93	1.50	95.92	95.91	1246 . 82	1236 - 45	82.00	1101-50
1 7	2 0 5 7 . 5 0	1.02	.79	9.93	1 + 5 0	104.19	104.17	1351.02	1340.62	95.00	1276.00
1 5	3107.50	1.05	.76	9.93	1 +5 0	81 + 35	81.34	1432.36	1421.96	100.00	1376.00
19	3340+00	1.08	.76	9 • 9 3	1 • 5 G	79.32	79.31	1511.68	1501 • 27	88.73	1464.00
20	3557.50	1.02	.9C	9.93	1.50	94.33	94.32	1606.71	1595.59	04.00	1558.00

PAY ARFA RAPIO TPANSIT DISTRICT CONTRACT NUMBER 1M0031 MR TUNNEL - 24TH TO RANCALL SIREET SAN FRANCISCO, CALIFORNIA

WEEK	CUMULATIVE FEET	OOWN HOURS CORRECTION	50IL CORRECTION	SHIELO CORRECTION	EXCAVATING EDUIPMENT CORRECTION	WEEK'S		CUMULATIV ======== INTEGRATION		======	L HOURS
21	385 - 00	1 - 0 4	.76	9.93	1.50	79.16	79.17	1685.19	1674.76	95.00	1653.00
22	4107.50	1.07	.76	9.93	1.50	76.63	76.62	1761.81	1751.39	92.00	1745.00
2 3	4297.50	1.09	.76	9.93	1 • 5 0	60.75	60.74	1822.56	1812.13	83.00	1828.00
24	434±.00	2 • 1 6	.76	9.93	1 . 5 0	20.04	29.34	1851.60	1841.17	41.00	1869.00
25	4425.00	1 . 0 1	.78	9.93	1.50	23.28	23.28	1874.87	1864.45	56.00	1925.00

Appendix A-3. Rate of Advance Calculations.

MAY AREA RAPIO TRANSIT DISTRICT CONTRACT NUMBER 1M0031 ML TUNNEL - 24TH TO PANDALL STREET SAN FRANCISCO, CALIFORNIA

WEEK	CUMULATIVE FEET	OOWN HOURS CORRECTION	SOIL CORRECTION	SHIELO CORRECTION	EXCAVATING EQUIPMENT CORRECTION		S HOURS	CUMULATIV		======	L HOURS
1	20.00	1 - 0 4	. 75	9.93	1.50	39.25	34.45	39.25	34.45	32.00	32.00
7	52.50	1.08	. 75	9.93	1.50	41.41	40.90	80.66	75.35	34.00	66.00
3	175.00	1.27	. 75	9.93	1.50	134.94	132.92	215.60	237.77	76.00	142.00
4	33 < . 00	1.15	.75	9.93	1.50	125.79	125.35	341.40	332.82	89.00	231.00
5	55.00	1.02	.73	9.93	1.50	128.52	128.06	469.92	460.87	113.00	344.CC
6	797.50	1.00	.77	9.93	1.50	127.47	127.24	597.39	58ª.11	102.00	446.00
7	1167.50	1.01	.77	9.93	1.50	180.39	180.71	777.78	768.11	112.00	558.00
B	1359.00	1.02	.76	9.93	1.50	84.87	84.94	862.65	852.96	60.00	618.00
9	1487.50	1.01	.76	9.93	1.50	59.31	59.71	921.96	912.20	63.90	6º1.00
13	151 - 50	1.09	.76	9.93	1.50	12.85	12.52	934.81	924.66	10.00	691.00
11	1695.30	1.06	.76	9.93	1.50	78.86	79.37	1013.67	1003.95	84.00	775.00
17	1070.00	1.07	.76	9.93	1.50	75.65	75.64	1089.32	1079.59	93.00	A68.00
1.3	1935+00	1.66	.79	9.93	1.50	44.84	44.84	1134.16	1124.43	59.00	927.00
14	1987.50	3.49	.79	9.93	1.50	75.62	32.34	1209.78	1156.77	28.00	955.00
15	2167.53	1.21	.79	9.93	1.50	86.20	86.70	1295.98	- 1242.97	66.00	1021.00
16	2495.00	1.02	.79	9.93	1.50	132.86	132.82	1428.85	1375.79	104.00	1125.00
1 7	2577.50	1.53	.79	9.93	1.50	48.61	48.61	1477.45	1424.40	56.00	1181.00
1 9	2787.03	1.04	.79	9.93	1.50	82.31	92.30	1559.76	1506.70	101.00	1282.00
19	3080.00	1.02	.76	9.93	1.50	105.01	105.30	1664.78	1611.70	94.00	1376.00
23	3285.00	1.06	.76	9.93	1.50	74.81	74.81	1739.59	1686.5C	95.00	1471.00

PAY AREA RAPIO TRANSIT DISTRICT CONTRACT NUMBER 1M0031 ML TUNNEL - 24TH TO RANDALL STREET SAN FRANCISCO, CALIFORNIA

	CUMULATIVE	DOWN HOURS	501L	SHIELO	EXCAVATING	WEEK'5	HOURS	CUMULATIV	E HOURS	ACTU	AL HOURS
WEEK	FEET	CORRECTION	CORRECTION	CORRECTION	CORRECTION	INTEGRATION	SUMMATION	INTEGRATION	SUMMATION	WEEKS	CUMULATIVE
21	3510.00	1.08	.76	9.93	1.50	81.68	83.50	1821 - 26	1770.01	92.00	1563.00
22	3795.00	1.03	.90	9.93	1.50	115.00	114.99	1936 - 27	1885.00	95.00	1659.00
2 3	4120.00	1.02	.76	9.93	1.50	107.42	107.41	2043.68	1992.40	104.00	1762.00
24	4280.00	1.04	.76	9.93	1.50	52.48	52.88	2096.56	2045.26	108.00	1870.00
25	4390.00	1.00	.78	9.93	1.50	35.78	35.78	2132.34	2081.06	101.00	1971.00

PAY AREA RAPID TRANSIT DISTRICT CONTRACT NUMBER 1R0053 PR/RL TUNNELS BERKELEY, CALIFORNIA

WEEX	CUMPLATIVE FEET	DOWN HOURS CORRECTION	STIL CORRECTION	SHIELO CORRECTION	EXCAVATING ECUIPHENT CORRECTION		HOURS	CUMULATIV			L HOURS
1	29.00	1.09	. 8 8	10.77	• 5 2	153.23	91.99	153.23	91.99	76.00	76.00
2	90.00	1.00	. P. 8	10.77	. 8 2	198 + 67	195.58	351.90	287.58	120.00	196.00
3	16 7 . 00	1.90	. 8 8	10.77	.82	191.87	191.04	543.78	478 - 61	119.00	314.00
4	212.00	1 + 1 3	99.	10.77	* 8 Z	131.75	131.63	675.52	610.25	111.00	425 • CO
5	254.00	1.39	.88	10.77	. 8 2	127.02	126.94	802 • 55	737.19	114.00	539.00
6	320.00	1.31	.88	10.77	* 8 Z	120.11	120.35	922.65	857.24	119.00	658.07
7	367+90	. 1.39	. A 8	10.77	• 8 2	133.41	133.38	1056.06	990.62	80.00	7 78 . CC
я	03.F##	1.89	.88	10.77	.82	149.42	149.36	1205 • 49	1139.97	118.00	856.00
9	529.00	1.33	. A 8	10.77	. 8 2	161.53	161.46	1367.01	1301-44	120.00	976.00
17	614.00	1.71	. A 8	10.77	. 8 2	158 + 79	158.75	1525 + 81	1460.18	119.00	1094.00
1 1	717.00	1.03	. 6 6	19.77	. 8 2	171.56	171.53	1697 + 39	1631.71	111.00	1205.00
1,2	771.20	1.72	* b 8	10.77	. A 2	101.58	101.57	1798.97	1733.29	70.00	1263.60
1.3	967.00	1.01	8	10.77	+82	152+14	152.11	1951 - 10	1885.40	117.00	_1400.00
14	040.00	1.74	. я. е	10.77	.82	136.96	136.95	2088.06	2022+35	113.00	1513.00
1 %	1016.00	1 - 1 4	• P C	10.77	• 6 2	110.18	119.17	2206.24	2140.52	99.00	1612.00
16	1390.00	1 • 0 1	* B D	10.77	• P 2	117.97	117.96	2324 - 21	2258.47	119.00	1731.30
17	1157.00	1.02	• 9.0	10.77	٠٩2	82.06	82.36	2406.27	2340+53	94.00	1825.00
1 F	1225.00	1.30	• R C	10.77	• P Z	93.28	94.65	2499.55	243 - 19	96.00	1921.00
19	1297.00	1.00	. 90	10.77	. 8 2	99.46	99.46	2599.01	2534.64	120.30	2041.00
21	1374.00	1.00	.90	10.77	. 8 2	127.35	127.34	2726.35	2661.98	119.00	2160.00

BAY AREA RAPIO TRANSIT OISTRICT CONTRACT NUMBER 180053 RR/RL TUNNELS BERKELEY, CALIFORNIA

₩EEK	CUMULATIVE	OOWN HOURS CORRECTION	SOIL CORRECTION	SHIELO CORRECTION	EXCAVATING EQUIPHENT CORRECTION	WFEK®S	=========	CUMULATIV		======	L HOURS
21	1450.00	1.00	. 90	10.77	• • 2	126.92	126.91	2853.27	2788.96	119.00	2279.00
22	1474.00	1.00	.90	10.77	.82	22.10	22 • 10	2875.37	2811.00	120.00	2309.00
23	1479.00	1.00	•90	10.77	• 8 Z	7.35	7.35	2882.72	2818.35	120.00	2519.00
24	1599.00	1.01	.66	10.77	. R 2	127.85	127.94	3010.58	2946.19	115.00	2634.00
2.5	1677.00	1 - 0 1	.66	10.77	. 6 2	78.10	78.10	3088.68	3024.29	7 4 . 0 0	2712.00
26	1817.00	1.00	.66	10.77	• 8 2	142.29	142.28	3230.97	3166.57	119.00	2871.00
27	1947.00	1.72	.66	10.77	.82	137.47	137.47	3368.44	3304.03	112.00	2943.00
29	2059.00	1.36	•66	10.77	• 8 2	121.87	121.96	3490.31	3425.90	103.00	3046.00
29	2199.00	1.01	.66	10.77	.82	137.76	137.76	3628.07	3563.65	118.00	3164.00
30	2320.00	1.02	• 6 6	10.77	.82	128.00	128.30	3756.08	3691.65	112.00	3276.00
3 1	2369.00	1.41	.66	10.77	.82	52.45	52.95	3909.53	3744.10	69.00	3345.00
32	2467.00	1.01	• 90	10.77	.82	123.73	123.73	3937+26	3867.83	117.00	3462.00
3.3	2546.00	1.02	.00	10.77	.82	110.58	110.58	4042.83	3978 • 40	116.00	3578.00
34	2650+00	1.00	.90	10.77	• 8 2	133 • 15	133.15	4175.99	4111.55	110.00	3697.00
35	2746.00	1.00	• 9 0	10.77	.82	121.74	121.73	4297.72	4233.29	120.00	3817.00
36	2810.00	1 • 31	•90	10 - 77	. 8 2	105.17	105.17	9402.89	4338.45	77.00	3894.00
37	2889.00	1.01	.90	10.77	. A 2	98.27	98.27	4501-16	4436.73	118.00	4012.00
3 P	2903.00	1.00	. 90	10.77	+82	18.69	18.69	4519.86	4455.42	120.00	4132.00

PAY AREA RAPIO TRANSIT OTSTRICT CONTRACT NUMBER 150011 TR TUNNEL SAN FRANCISCO, CALIFORNIA

	CUMPLATIVE	OOMN HOURS	S01L	SHIELO	EXCAVATING EQUIPMENT	WEE#*5	HOURS	CUMULATIV	E HOUPS	ACTU	AL HOURS
WEEK	FEET	CORRECTION	CORRECTION	CORRECTION	CORRECT 104	INTEGRATION	SUMMAT 1 CN	INTEGRATION	SUMMATICH	WEEKS	CUMULATIVE
1	47.43	1.01	.73	9.11	1.09	77.98	66 • 1 2	77.98	66.12	63.38	63.08
2	194.73	1.01	• 75	9.11	1.09	128.04	124.20	206.02	190.32	114.84	177.92
3	367.07	1.01	.75	9.11	1.49	149.09	148.11	355.11	338.42	112.76	290.68
4	564.85	1.01	.76	9.11	1.49	155.81	155.27	510.93	493.69	115.59	406.27
5	694.74	1.07	.75	9.11	1 • 6 3	102.73	102.66	613.66	596.35	99.44	505.71
6	960.09	1.06	•73	9.11	1.49	123.71	123.58	737.37	719.93	99.37	605 - 08
7	1114.23	1 • 0 3	.75	9.11	1.49	135.36	135.24	872.74	P55.17	102.36	707.44
9	1357.38	1.53	.75	9.11	1.49	132.08	132.30	1004.82	987.17	108.40	R 15 . 94
ş	1467.21	1.00	• 7 3	9.11	1 - 4 9	55.59	55.59	1060.41	1042.76	118.66	934.50
10	1510.49	1.12	• 75	9.11	1.63	32.69	32.69	1093-11	1075.45	97.62	1032.12
11	1557-48	1.02	.75	9 • 1 1	1.63	34.54	34.54	1127.65	1169.99	103.95	1136.07

PAY AREA RAPIO TPANSIT DISTRICT CONTRACT NUMBER 150011 TL TUNNEL SAN FRANCISCO, CELIFORNIA

WEEK	CUMPLATIVE FEET	OONN HOURS CORRECTION	SOIL COPRECTION	SHIELO CORRECTION	EXCAVATING EQUIPMENT CORRECTION		HOURS	CUMULATI THE GRATION			L HOURS
1	44.76	1.01	.77	9.59	• A Z	71.71	62.23	71.71	62.23	97.85	97.85
2	137.34	1.73	.79	9.59	.82	90.46	88.86	162.17	151.10	112.67	210.52
3	330.61	1.00	.81	9.59	.82	129.36	128.10	291.53	279.19	114.59	325.11
4	469.43	1.00	.75	9.59	1.49	170.18	169.73	461.71	448.92	93.00	418.11
5	527.31	1.91	.74	9.59	1.45	152+66	152.40	614 - 31	601.32	93.58	511.69
6	824.68	1.02	.76	9.59	1.49	179.88	178.57	793.19	779.99	111.70	623.39
7	1054.04	1.03	.75	9.59	1.49	191.68	191.51	984.98	971.50	102.59	725.98
8	1281.41	1.03	.75	9.59	1.49	161.42	181.31	1166.29	1152.81	105.10	P31+C9
9	1451.36	1.07	• 7 7	9.59	1.51	139.24	138.21	1304.54	1291.02	92.24	923.32
10	1516.29	1.00	.75	9.59	1.49	46.47	46.47	1351.01	1337.49	116.5C	1039.82
11	1551.29	1.33	.75	9.59	1.49	43.51	43.51	1394.52	1381.00	75.66	1115.48

PAY AREA RAPIO TRANSIT CISTRICT CONTRACT NUMBER 150011 SR TUNNEL SAN FRANCISCO, CALIFORNIA

wEEK	CUMULATIVE FEET	OOWN HOURS Correction	501L CORRECTION	SHIELO. CORRECTION	EXCAVATING EQUIPMENT CORRECTION		HOURS	CUMULATI TETTETT THEGRATION	VE HOUPS		L HOURS
1	42.°0	1 - 1 7	.83	9.59	1.09	83.56	73.02	83.56	73.02	55.42	55.42
2	164.10	1.00	.83	9.59	1 + 9 9	117.81	115.32	201.36	188.04	113.08	168.50
3	212.63	1.01	. A 3	9.59	1.39	38.18	38.14	239.54	226.18	44.24	212.74
4	325.03	1.04	.9.7	9.59	1.49	114.96	114.65	354.50	34C+84	84.83	297.57
5	480.91	1.01	.86	9.59	1.49	151.06	150.68	505.56	491.52	113.08	410.65
6	654.75	1.03	.80	9.59	1.49	130.14	129.98	635.70	621.50	108.81	519.46
7	839.32	1.04	.79	9.59	1.49	134.80	134.67	770.50	756.17	100.83	620.29
	1031.61	1.06	.85	9.59	1.49	143.36	143.27	913.86	899.44	91.23	711.52
9	1234.34	1.00	.83	9.59	1.49	134.26	134.19	1048.12	1033.63	117.00	828.52
10	1415.75	1.00	.83	9.59	1.49	112.59	112.55	1160.70	1146.19	95.42	923.94
11	1552.94	1.00	.85	9.59	1.54	153.42	153.40	1314 - 12	1299.58	84.08	1008.02

PAY AREA MAPIO TRANSIT DISTRICT CONTRACT NUMBER ISODII SL TUNNEL SAN FRANCISCO, CALIFORNIA

CUMULATIVE CONN HOURS SOIL SHIELD EXCAVATING COUINENT CORRECTION CO												
1 20.93 1.00 .75 8.71 1.49 75.73 63.41 75.73 63.81 2 109.53 1.00 .75 8.71 1.49 105.35 102.63 181.09 166.44 3 200.45 1.04 .75 8.71 1.49 102.64 101.48 283.72 268.31 4 326.95 1.02 .75 8.71 1.49 99.36 99.20 383.08 367.32 5 386.93 1.02 .75 8.71 1.49 45.81 45.79 429.89 413.10 6 526.83 1.03 .75 8.71 1.49 45.81 45.79 429.89 413.10 6 526.83 1.03 .75 8.71 1.49 98.81 98.64 527.70 511.74 7 639.23 1.05 .75 8.71 1.49 76.11 76.06 603.81 587.80 8 796.72 1.01 .75 8.71 1.49 95.74 95.15 699.05 682.96 9 851.61 1.04 .75 8.71 1.49 32.62 32.62 731.68 715.58 10 981.25 1.14 .75 8.71 1.49 81.11 81.28 812.79 796.66 11 1116.09 1.13 .75 8.71 1.49 80.22 80.20 893.02 876.86 12 1296.74 1.02 .75 8.71 1.49 92.22 92.18 985.23 969.04 13 1457.86 1.08 .75 8.71 1.49 92.22 92.18 985.23 969.04 13 1457.86 1.08 .75 8.71 1.49 92.22 92.18 985.23 969.04						E OU 1 PMENT					ACTUAL HOURS	
2 109.53	WEEK	FEET	CORRECTION	CORRECTION	CORRECTION	CORRECTION	INTEGRATION	SUPMATION	INTEGRATION	SUMMATION	MEEKS	CUMULATIVE
3 20°.45 1.04 .75 8.71 1.49 102.64 101.48 283.72 268.31 4 326.95 1.02 .75 8.71 1.49 99.36 99.00 383.08 367.32 5 386.93 1.02 .75 8.71 1.49 45.81 45.79 429.89 413.10 6 52°.83 1.03 .75 8.71 1.49 98.81 98.64 527.70 511.74 7 639.23 1.05 .75 8.71 1.49 76.11 76.06 603.81 587.80 8 796.72 1.01 .75 8.71 1.49 95.74 95.15 699.05 682.96 9 851.61 1.04 .75 8.71 1.49 32.62 32.62 731.68 715.58 10 981.25 1.14 .75 8.71 1.49 81.11 81.28 812.79 796.66 11 1116.09 1.13 .75 8.71 1.49 80.22 80.20 893.02 876.86 12 129°.74 1.02 .75 8.71 1.49 92.22 92.18 985.23 969.04 13 1457.86 1.08 .75 8.71 1.49 92.22 75.18 985.23 969.04	1	20.93	1.00	•75	e.71	1.49	75.73	63.91	75.73	63.81	109.33	109.33
4 326.95 1.02 .75 8.71 1.49 99.36 99.20 383.08 367.32 5 386.93 1.02 .75 8.71 1.49 45.81 45.79 427.89 413.10 6 52°.73 1.03 .75 8.71 1.49 98.81 98.64 527.70 511.74 7 639.23 1.05 .75 8.71 1.49 76.11 76.26 603.81 587.80 8 796.72 1.01 .75 8.71 1.49 95.74 95.15 699.05 682.96 9 851.61 1.04 .75 8.71 1.49 32.62 32.62 731.68 715.58 10 981.25 1.14 .75 8.71 1.49 81.11 81.27 796.66 11 1116.09 1.13 .75 8.71 1.49 80.22 80.20 893.02 876.86 12 1295.74 1.02 .75 8.71 1.49 92.22 92.18 985.23 969.04 13 1457.86	2	109.53	1.00	.75	8 • 71	1 + 4 9	105.35	102.53	181.09	166.44	116.16	225.49
5 386.93 1.02 .75 8.71 1.49 45.81 45.79 422.89 413.10 6 52°.93 1.03 .75 8.71 1.99 98.81 98.64 527.70 511.74 7 639.23 1.05 .75 8.71 1.49 76.11 76.06 603.81 587.80 8 796.72 1.01 .75 8.71 1.49 95.74 95.15 609.05 682.96 9 851.61 1.04 .75 8.71 1.49 32.62 32.62 731.68 715.58 10 981.25 1.14 .75 8.71 1.49 81.11 81.28 812.79 796.66 11 1116.09 1.13 .75 8.71 1.49 80.22 80.20 893.02 876.86 12 1295.74 1.02 .75 8.71 1.49 92.22 92.18 985.23 969.04 13 1457.86 1.08 .75 8.71 1.26 76.50 1061.75 1045.54	3	200.45	1.04	.75	8 • 7 1	1 • 4 9	102.64	101 • 9 8	283.72	260.31	112.17	337.66
6 52°.P3 1.03 .75 8.71 1.09 98.81 98.64 527.70 511.74 7 639.23 1.05 .75 8.71 1.49 76.11 76.06 603.81 587.80 8 796.72 1.01 .75 8.71 1.49 95.74 95.15 699.05 682.96 9 851.61 1.04 .75 8.71 1.49 32.62 32.62 731.68 715.58 10 981.25 1.14 .75 8.71 1.49 81.11 81.08 812.79 796.66 11 1116.09 1.13 .75 8.71 1.49 80.22 80.20 893.02 876.86 12 129°.74 1.02 .75 8.71 1.49 92.22 92.18 985.23 969.04 13 1457.86 1.08 .75 8.71 1.26 76.°2 76.50 1061.75 104°.54	4	326.95	1 • 0 2	.75	8 • 71	1.49	99.36	99.00	3 8 3 . ↑8	367.32	112.42	450.CF
7 639.23 1.05 .75 8.71 1.49 76.11 76.26 603.81 587.80 8 796.72 1.01 .75 8.71 1.49 95.24 95.15 699.05 682.96 9 851.61 1.04 .75 8.71 1.49 32.62 32.62 731.68 715.58 10 981.25 1.14 .75 8.71 1.49 81.11 81.28 812.79 796.66 11 1116.09 1.13 .75 8.71 1.49 80.22 80.20 893.02 876.86 12 1295.74 1.02 .75 8.71 1.49 92.22 92.18 985.23 969.04 13 1457.86 1.08 .75 8.71 1.49 92.22 76.50 1061.75 1045.54	5	386.93	1.02	.75	8 - 71	1 • 4 9	45.81	45.79	420.89	413+10	57.67	507.75
F 796.72 1.01 .75 8.71 1.49 95.24 95.15 699.05 682.96 9 851.61 1.04 .75 8.71 1.49 32.62 32.62 731.68 715.58 10 981.25 1.14 .75 8.71 1.49 81.11 81.08 812.79 796.66 11 1116.09 1.13 .75 8.71 1.49 80.22 80.20 893.02 876.86 12 1295.74 1.02 .75 8.71 1.49 92.22 92.18 985.23 969.04 13 1457.86 1.08 .75 8.71 1.26 76.52 76.50 1061.75 1045.54	6	525.83	1.73	.75	0.71	1 • 4 9	98 + 81	98.64	527.70	511.74	108.50	616.25
9 851.61 1.04 .75 8.71 1.49 32.62 32.62 731.68 715.58 10 981.25 1.14 .75 8.71 1.49 81.11 81.08 812.79 796.66 11 1116.09 1.13 .75 8.71 1.49 80.22 80.20 893.02 876.86 12 1295.74 1.02 .75 8.71 1.49 92.22 92.18 985.23 969.04 13 1457.86 1.08 .75 8.71 1.26 76.52 76.50 1061.75 1045.54	7	639.23	1.05	. 75	8 • 7 1	1.49	76.11	76.36	603.81	587.80	81.17	697.42
10 981.25 1.14 .75 8.71 1.49 81.11 81.08 812.79 796.66 11 1116.09 1.13 .75 8.71 1.49 80.22 80.20 893.02 876.86 12 1295.74 1.02 .75 8.71 1.49 92.22 92.18 985.23 969.04 13 1457.86 1.08 .75 8.71 1.26 76.52 76.50 1061.75 1045.54	e	796.72	1.01	• 75	8 • 71	1.49	95.24	95 • 15	699.05	687.96	105+58	803.00
11 1116.09 1.13 .75 8.71 1.49 80.22 80.20 893.02 876.86 12 1295.74 1.02 .75 8.71 1.49 92.22 92.18 985.23 969.04 13 1457.86 1.08 .75 8.71 1.26 76.52 76.50 1061.75 1045.54	9	951-61	1.04	• 75	8.71	1.49	32+62	32.62	731.68	715.58	88.90	891.90
12 1295.74 1.02 .75 8.71 1.49 92.22 92.18 985.23 969.04 13 1457.86 1.08 .75 8.71 1.26 76.52 76.50 1061.75 1045.54	10	981.25	1 - 1 4	. 75	8 • 71	1 - 4 9	81.11	81.28	R12.79	796.66	92.08	993.98
13 1457.86 1.08 .75 P.71 1.26 76.52 76.50 1061.75 1045.54	11	1116.09	1 • 1 3	.75	8 . 71	1.49	80 + 22	80.20	893.02	876.86	98.42	1082+40
	12	1295.74	1.02	.75	8 . 71	1.49	92.22	92.18	985.23	969.04	112.09	1194.49
14 1565-19 1.01 .75 8.71 1.49 88-11 88-10 1149.86 1133.64	1 3	1457.86	1.08	. 75	P • 71	1 • 2 6	76. 42	76.5N	1061.75	104 - 54	83.95	1278.44
	1 4	1565.19	1.01	.75	8 . 7 1	1.49	88 + 11	88.10	1149.86	1133.64	74.83	1353.27

BAY AREA RAPIO TRANSIT DISTRICT CONTRACT NUMBER 150051A SL TUNVEL - MARKET STREET SAN FRANCISCO, CALIFORNIA

5 277.46

6 384.96

8 564.96

9 687.46

10 759.96

477.46

1.04

1.07

1.01

1.02

1.01

1.01

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. 93

.93

.86

8 . 8 4

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0.84

6.84

WEEK	CUMULATIVE FEET	ODWN HOURS CORPECTION	501L CORRECTION	SHIELD CORRECTION	EXCAVATING EQUIPMENT CORRECTION	WEEK*5		CUMULATIV	========		L HOURS ======= CUMULATIVE
1	8 - 30	1.02	. 43	8 • 7 1	1 • 1 7	279.96	130.39	279.96	130.39	112 - 36	112.36
2	152.50	1.10	. 9.0	8.71	1 • 1 7	138+03	137.19	417.99	267.58	94.08	296+44
3	720.00	1.09	.79	8 . 71	1 - 17	116.65	116.37	534.64	383.94	96.44	302.28
4	280.00	1.03	.79	8 . 71	1 - 1 7	e7.49	87.40	622.13	471.34	78.36	391.24
5	350.00	1.01	. 75	F . 71	1 +1 7	89.23	89.15	711.36	560.49	79.50	460.74
6	45 7.20	1 + 0 3	.76	8 - 71	1 • 1 7	129.00	128.83	840.36	680.72	106.03	566.77
7	564.73	1.02	. 75	8 . 71	1 • 1 7	117.41	117.32	957.78	806.64	110.10	676.87
4	580.70	1 + 9 3	. 8 3	8 - 71	1.17	142.61	142.51	1100 - 39	949.15	107.49	789.36
9	720.70	1.21	. R 3	8 - 71	1 - 1 7	75 • 17	75.17	1175.57	1024.22	49.46	129.82
CONT SR T	AREA RAPIO I RACT NUMPEP UNNEL - MARI FRANCISCO, (150051# FT STREET									
WEEK	CUMILATIVE FEET	DOWN HOURS CORRECTION		SHIELD CORRECTION	EXCAVATING EQUIPMENT CORRECTION	WFEK*5	S HOURS	CUMULATI CUMULATI COMPLETED COMPLETED			AL HOURS
1	27.46	1.00	• e D	6 + 6 4	1.09	67.74	43.51	67.74	43.51	66.00	66.00
2	94.96	1.03	.74	0.84	1.09	00.86	78.73	148.60	122 + 24	110.25	176.25
3	137.46	1.79	.81	8.84	1.09	45.76	45.64	194.36	167.88	52.34	228.59
4	190.24	1 + 0 2	.89	8 . 8 4	1 • 6 3	78 + 21	78.95	272.57	245.93	74.67	303.26

Appendix A-3 (continued)

1.63 100.33 100.36

117.94

90.71

86.10

33.65

104.99

118.09

90.29

86.15

104.97

33.65

345.99 106.69

463.03 100.64

554.04 78.25

745.03 105.52

778.68 37.75

640.14 73.26

377.90

490.99

581.28

667.43

772.40

806.05

409.95

510.59

5 9 8 . 8 4

662.10

767.62

805.37

1.63

1.63

1 • 6 3

1.63

UPPER SALT CREEK #1 CONTRACT NUMBER 68-404-25 CHICAGN, ILLINDIS

WEEK	CUMPLATIVE	OOWN HOURS	SOIL CORRECTION	SHIELO CORRECTION	EXCAVATING EQUIPMENT CORRECTION	WEEK'S		CUMULATIVE			L HOURS
1	24+00	1.13	.72	6.92	1.50	28.59	23.99	26.6	23.99	25.50	25÷50
:	30.70	1.07	.75	6.92	1.50	10.27	10.23	36 * 86	34.22	16.00	41.50
3	130.00	1.05	.77	6.92	1.50	49.84	48.60	88.70	62.62	44.00	P5+50
4	210.00	1.04	.67	6.92	1.50	28.58	28.46	117.28	111.28	25.00	110.50
ι	214.03	1.99	.67	6.92	1.50	2.46	2.46	119.74	113.74	3.00	113.50
6	242.03	1.92	.67	6.97	1.50	16.58	16.58	136.72	130+32	14.00	1.27 + 50
7	264.03	1.27	.75	6.92	1.5C	9.82	9 • 9 2	146.14	140.14	10.00	144.50
÷	284.03	1.01	.75	6.92	1.50	6.70	6 + 3 0	152.44	146.44	10.00	155.50
9	*5°.33	1.13	.71	6.92	1.53	24.42	24.46	176.02	170.89	37.00	1 05 - 50
10	417.00	1.20	+67	6 • 92	1.50	16.22	16+21	193.13	167.10	1 0 .00	2 ~3 • € .
11	F90+00	1.02	.67	6.92	1.50	43.63	43.52	236.76	230.62	40.00	243.50
12	734.00	1.11	.67	6.92	1.50	27.93	27.92	264.70	258.54	25.50	10.692
1 7	c 3 o + C O	1.08	.64	6.92	1.50	28.14	28.13	292.84	284.66	28.00	257.00
14	1094.00	1.02	• 7 S	6 • 92	1.50	55.60	55.53	349.44	342.19	3A+CC	335.00
1.5	1757.00	1.00	.75	6.97	1.50	52.89	52.94	401.32	395.03	38.00	373.00
16	1464.23	1+15	. A.S.	6.97	1.50	25.60	25+60	426.92	420.63	16.50	72.045
17	1510.00	1.62	.92	6.92	1.50	16.21	16.21	443.14	436.84	12.00	471.50
1 8	1530.00	1.78	.89	6.92	1 • 2 0	4.73	4.73	447.86	441.57	12.00	413.50
19	1584.20	1.04	1.05	6.92	1.50	14.91	14.91	462.77	456.47	41.50	455.00
27	1565+00	1.08	-96	6 • 9 2	1.50	20.45	20.95	487.22	476.92	33.00	488.05

UPPER SALT CPEER #1 CON19ACT NUMPER 66-404-25 CHICASO, ILLINOIS

WEEK	CUMBLATIVE FEET	DOWN HOURS CCA9ECTION	SOIL CORPECTION	SHIELD CORRECTION	EXCAVATING EQUIPMENT CORRECTION	WFEK*S		CUMULATIV		=======	L HOURS
2 1	1927.00	1.02	.94	6.92	1.50	34 - 34	34+33	517.56	511.25	38.50	526.50
2.2	2337.00	1.06	• 9 2	6.92	1.50	35.65	35.55	553-21	546.90	37.00	563.50
23	2075.00	1.04	.76	6.92	1.50	12.79	12.79	566.00	559.69	34.00	597.50
24	2230.00	1.05	. 93	6.92	1.50	33.95	33.95	599.95	593.64	41.00	638.50
25	2274.00	1.36	•93	6.92	1.50	9.54	9.59	609.49	603.18	19.00	657.50
2.5	2335.00	1.31	.75	6.92	1.50	13.51	13.51	623.00	616.69	23.00	680.50
27	2513.00	1.05	• 75	6.97	1.50	29.20	29.19	652.19	64c.86	31.00	711.5C
29	2933.00	1.00	.82	6.92	1.50	53.49	53.48	705.68	699.36	45.00	756.50
29	3741.00	1.02	•67	6.92	1.50	27.98	27.98	733.67	727.34	25.00	781.50
30	3349.00	1.03	• A [6.92	1.50	46.90	46.90	782.57	776.23	39.00	#20.50
31	3652.00	1.91	.66	6.92	1.50	34.29	34.28	816.85	A1C.51	37.00	857.50
32	3957.00	1.05	.74	6.92	1.50	32.18	32.18	949.03	842.68	31.00	888.50
3 3	4729.00	1.00	.78	6.92	1.50	51.83	51.92	900.06	894.51	45.00	933.50
34	4444.00	1.05	.76	6.92	1+5 C	30 • 6 9	30.69	931.55	925.20	22.00	955.50
3 %	4725.00	1.90	.90	6.92	1.50	42.91	42.91	974.47	968-11	34.00	989.50
36	4977.00	1.08	.93	6.92	1.50	25.59	25.59	1000.06	99*.70		
37	5177.00	1.01	.75	6.92	1.50	37.68	37.68	1037.74	1031.38	23.50	1013.00
3 €	5481.00	1.04	.75	6.92	1.50	38.33	38.32	1076.07		37.00	1050.00
3 %	5081.00	1.00	.75	6.92	1.50	47.65	97.64	1123.71	1069.70	37.00	1087.00
40	6167.00	1 - 0 4	.84	6.92	1.50	38.71	38.71	1162.93	1117.35	95.00 33.50	1132.00
										22.30	,

UPPER SALT CREEK #1 CONTRACT NUMBER 68-4C4-2S CHICAGO, ILLINOIS

WEEK	CJMULATIVE FEET	OOWN HOURS CORRECTION	SC1L CORRECTION	SHIELD CORRECTION	EXCAVATING EQUIPMENT CORRECTION	WEEK'S		CUMULATIN		=======	L HOURS
41	634	1.00	1.72	6.92	1.50	27.86	27.88	1190.30	1183.93	31.00	11°6.50
42	6444.00	1.78	1.02	6.92	1.50	16.71	16.71	1207.01	1200.64	30.00	1226.50
43	6457.00	1.14	1.02	6.92	1.50	8.46	8.46	1215.47	1209.10	25.00	1251.50
44	6510.00	1.70	.99	6 • 9 2	1.50	6.59	6.59	1222.05	1215.66	17.00	1268.50
4 5	6565.00	1.09	1.02	6.92	1.50	7.72	7.72	1229.77	1223.40	26.00	1294.50
4 4	6667.00	1.10	1.02	6.92	T.S.D	16.49	16.49	1746.76	1239.89	37.00	1327.50
4 7	605.2849	1.00	1.02	6 • 9 2	1. " C	24.72	24.72	1270.98	1264.61	36.00	1363.SC
4.8	7077.00	1.00	1.02	6.92	1.00	37.41	37.41	1308.39	1302.02	44.00	1477.50

PPPER SALT CREEK #2 CONTRACT NUMBER 68-405-25 CHICAGO, ILLINOIS

WEEK	CUMPLATIVE FEE1	OOWN HOURS CORRECTION	SOIL CORRECTION	SHIELD CORRECTION	EXCAVATING EQUIPMENT CORRECTION	MEEK'S		CUMULATIVE TINTEGRATION	=======================================	=======	L HOURS
1	46.00	1.00	.75	6 • 2 9	1 • 6 3	23.46	19.63	23.48	19.63	40.00	40.00
2	60.00	1.00	۰7٤	6.29	1.63	7.22	7.19	30.70	26.83	17.00	57.00
3	177.00	1 - 0 3	.75	6 + 2 9	1 • 6 3	26.24	25.85	56.04	\$7.68	36.00	°7.00
4	385.00	1.02	•75	6.29	1.50	36 • P1	36.38	93.75	89.06	41.00	129.00
5,	c 6 7 • 0 0	1.01	• 7 3	6.29	1 • S C	71.18	70 -12	164.93	159.19	55.00	183.CC
6	1127.00	1.04	. 75	6.29	1.50	17.76	17.75	182.69	176.94	14.00	197.00
7	1671.00	1.00	.69	6 • 29	1.50	49.21	49.36	231,90	226.01	41.00	236.00
p	1089.00	1 - 0 9	.77	6 • 2 9	1.50	21.85	21.95	253.75	247.85	16.00	254.00
9	2384.00	1 • 0 2	. 74	6.29	1.5C	41.89	41.05	295.65	289.70	36.00	290.00
10	3006.00	1.00	.75	6.29	1.50	47.95	47.90	343.59	337.60	\$1.00	341.00
11	3110.00	1 - 10	.79	6.29	1.50	9.00	9.00	3\$2.60	346.60	5.00	346.00
12	3480.00	1.00	.79	6.29	1 + 5 0	43+27	43.25	395.87	389.85	39.00	385.00
1.3	4091.00	1.02	•72	6.29	1.50	27.02	27.41	423.29	417.27	31.00	416.00
1 4	4534.00	1.00	. 75	6 - 29	1 - 5 0	33.89	33.98	457.17	451-14	35.00	451 + 00
15	4972.00	1.02	• a C	6 • 2 9	1 • S C	25.46	25.45	482.63	476.60	25.00	476.00
1 4	S * 1 * + 0 0	1.00	. 4 8	6 • 2 9	1.50	24.78	24.78	507.41	501.38	24.00	.00.00

UPPER SALT CREEK #3 CONTRACT NUMPER 68-406-25 CHICAGO, ILLINOIS

WEEK	CUMULATIVE FEET	DOWN HOURS CORRECTION	SOIL COPRECTION	SHIELD CORRECTION	EXCAVATING EQUIPMENT CORRECTION	WEEK'S		CUMULATIV		*******	HOURS
1	2~.00	1.20	.75	5.77	1.63	22.59	19.15	22.59	19.15	10.00	10.00
7	134.00	1.05	.67	5.77	1 • 5 C	32.94	31.66	55.53	50.82	20.00	*8.00
3	26 . 33	1.01	• A 2	5.77	1 + 5 3	53.20	52.42	108.73	103.23	30.00	00.83
4	76°.CO	1.10	.67	5.77	1.50	27.82	27.76	136.55	130.99	23.00	91.00
ς,	526.00	1.00	•67	5.77	1.50	26.15	26 -11	162.70	157.10	31.00	172.00
6	67°.CC	1.00	.71	5.77	1.50	28.00	27.97	190.70	185.07	22.00	144.00
7	842+00	1 • 🖸 \$	• 9 5	5.77	1.50	35.24	35 - 21	225.95	220.28	31.00	175.00
F	1110.00	1 • 0 C	.64	5.77	1.55	41.03	40.97	266.97	261.25	36.00	211.00
9	1230.00	1.21	• a C	5 + 7 7	1.5C	24.28	24.27	291.25	285.53	14.00	225 • CO
10	1337.00	1.01	1.02	6.92	1.50	26.90	26.99	₹18+15	312.42	13.00	238.00
11	1417.00	1.15	.78	6.92	1 • ° C	17.03	17.23	335.18	329.45	17.30	255.00
12	1561.00	1.01	.75	6.92	1.50	29.04	29.23	364.22	357.48	30.50	295.50
1 3	1781.00	1.00	.75	6.97	1.56	33.70	33.59	397.92	397.16	29.00	314.50
14	1997.00	1.07	.75	6.92	1.50	19.62	19.51	417.54	411.79	20.00	334.50
15	2157.00	1.00	.75	6.92	1.50	41.24	41.73	45#.78	453.02	29.00	163.50
16	2477.00	1.00	.75	6.92	1 • • 0	49.20	49.18	567.98	502.21	40.00	403.50
17	2720.00	1.03	.7 °	6.92	1.50	38.09	38.39	546.07	540.29	27.00	4 30 • 5 C
1 5	3020.00	1.00	. • 0	6.92	1.55	45.49	95.90	591.56	ER 5.77	34.5C	465.00
19	3309.00	1.03	.78	6.92	1.50	41.30	41.70	632.87	627.07	31.00	996.00
23	36500	1.00	.75	6.92	1.50	50.16	50 • 1 5	683.03	677.22	38.00	534.00

UPPER SALT CPEEK #7 CONTRACT NUMBER 66-406-25 CHICAGO: ILLINOIS

	CUMULATIVE	OOLN HOURS	SOIL	SHIELO	EXCAVATING EQUIPMENT	WEEK'S	HOURS	CUMULATIV	E HOURS	ACTUA	L HOURS
WEEK		CORRECTION		CORRECTION	CORRECTION	14TEGRATION	SUMMATION	INTEGRATION	SUPMAT 10%	WEEKS	CUMULATIVE
21	3897.00	1.07	.75	6.92	1.50	29.4C	29.40	712.43	706.62	24.00	558.00
22	4297.00	1.70	.70	f • 92	1.50	50.70	50.70	763.13	757.32	37.00	595.00
23	4565.00	1.00	.75	6.92	1.50	35.47	35.46	798.60	797.78	39.50	633+50
24	4726.00	1.12	.75	6.92	1.50	19.15	19.15	817.75	811.93	24.00	657.5C
25	4904.00	1.23	.73	6.92	1.50	11.62	11.62	829.37	823.55	15.00	672.50
26	4974.00	1.00	• 7 1	6 • 92	1.50	19.10	19.10	848.47	842.65	32.00	704.50
27	5764.00	1.00	•75	6.92	1.50	34.76	34.35	882.92	877.00	37.00	741.50
2 6	KE67.00	1.00	.7°	6.92	1.50	36.50	36.50	919.32	913.50	36.50	778.00
29	5938.00	1.01	.76	6.92	1.50	29.50	29.50	948.82	947.00	31.00	£79.00

WASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY CONTRACT MUNER TEODZI FZA PLAITAGON OUTSOUNO WASHINGTON, O.C.

WEEK	CUMULATIVE FEET	DOWN HOURS CORRECTION	SOIL CORRECTION	SHIELO CORRECTION	EXCAVATING EQUIPMENT CORRECTION	WEEK®S		CUMULATIVE			CUMPRATIAE
1	67.00	1.01	.66	10.40	1.36	94.67	84.01	94.67	84.01	78.49	78.49
2	113.19	1.06	•66	10.40	1.36	47.66	47.49	142.34	131.51	27.28	175.77
3	280.08	1.02	88	10.40	1.36	187.64	185.59	329.98	317.09	83.68	189.45
4	339.50	1.60	.90	10.40	1 - 3 6	49.62	49.60	379.60	366.73	21.65	211-10
r	57.44	1.01	.79	10.40	1.36	165.88	165.36	545.48	537.06	69.93	280.91
6	607.81	1.02	.68	10-40	1.36	34.01	34+00	579.49	566.06	23.34	104.27
7	610.28	1.04	.57	10.40	1.36	1.30	1.70	580.79	567.76	7 . 2 5	311.52
٥	7002	1 • 9 3	.69	10.40	1.76	57.54	57.52	630.73	124.85	37.15	348.67
,	P3 - 57	1 • 0 3	•68	10.40	1.36	78.98	76.96	717+31	707.84	77.55	426.22
10	1097.52	1.70	.79	10.40	1.36	165.66	165.49	882.97	860.33	97.42	523+64
1.1	1390.79	1 - 0 1	.79	10.40	1.36	175 - 15	175.02	1058 • 12	1044.75	95.76	+19.4"
12	1400.25	1.02	.79	10.40	1 • 3 6	10.14	10.14	1068.25	1054.50	16.92	636+32

WASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMBER 150021 F2A PETIAGON INBOUND WASHINGTON, O.C.

1 7.50 1.00 .66 10.40 1.36 20.98 16.59 20.98 18.59 9. 2 14.30 1.01 .66 10.40 1.36 13.00 12.93 33.98 31.51 8. 3 39.26 1.03 .66 10.40 1.36 38.52 38.03 72.50 69.54 38. 4 41.68 1.30 .66 10.40 1.36 4.20 4.20 76.70 73.73 8.	8 17.78 1 55.89
3 3°.26 1.03 .66 10.40 1.36 38.52 38.03 72.50 69.54 38.	1 55.89
h h146 7 70 44 10 h0 1 77 h 20 h 20 74 70 77 77 9	
4 41.00 1.50 .00 10.40 1.50 4.50 10.10 15.13 0.	C 64+29
5 58.89 1.09 .66 10.40 1.36 23.69 23.65 100.39 97.39 28.	0 92.79
6 90.34 1.00 .66 10.40 1.36 44.47 44.31 144.96 141.70 38.	0 170.99
7 165.30 1.00 .66 10.40 1.36 61.33 61.13 206.19 202.93 38.	0 168.99
8 198.60 1.04 .66 10.40 1.36 36.05 36.03 242.24 238.86 22.	C 191.69
9 248.23 1.05 .66 10.40 1.36 44.39 44.36 286.63 263.22 26.	e 218 · 37
10 289.30 1.03 .66 10.40 1.76 34.27 34.26 720.89 317.48 38.	256.97
11 334.44 1.03 .66 10.40 1.36 37.83 37.82 354.72 354.29 38.	2 295+39
12 48 7.10 1.02 .88 10.40 1.36 144.87 144.62 503.60 499.91 79.	5 375 . 34
13 677.94 1.01 1.04 10.40 1.36 201.14 200.94 704.77 700.75 72.	2 447.76
14 83°.97 1.03 .79 1C.40 1.36 128.92 128.84 833.65 829.58 72.	5 519.81
15 90 • 19 1 • 11 • 79 10 • 40 1 • 76 49 • 95 49 • 94 883 • 60 879 • 52 44 •	5 564.36
16 1017.26 1.01 .59 10.40 1.36 55.29 55.28 938.89 934.80 61.	7 626.1?
17 1040.43 1.00 .68 10.40 1.36 16.08 16.08 954.97 950.88 17.	5 643.63
1R 1047.94 1.06 .68 10.40 1.36 1.57 1.57 956.54 952.46 6.	0 650.13
15 1147-31 1.05 .68 10.40 1.36 65.04 65.03 1021.58 1017.49 63.	3 713.16
20 1319.62 1.02 .59 10.40 1.36 85.84 85.41 1107.42 1103.30 84.	0 798.06
21 1511+14 1+03 +69 10+40 1+36 109+53 109+50 1216+95 1212+RC 89+	0 887.46

WASHINGTON METPOPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMBER IFEO21 F24 KLANTH ROUTE OUTEOUND WASHINGTON, D.C.

¥85×	CUMPLATIVE FEET	OOWN HOURS CORRECTION	501L CORRECTION	SHIFLO CORRECTION	EXCAVATING EQUIPMENT CORRECTION	WEEK'S		CUMULATIVE			L HOURS CUMULATIVE
1	67.89	1.01	. 92	10.40	1.36	99.25	86.70	99.25	86.70	54.08	54 • OP
2	204.52	1.05	.93	10.45	1.76	123.72	121.74	722.97	20° • 45	73.67	127.75
*	237.64	1.03	.93	10.40	1.36	20.91	26.91	243.88	229.35	33.08	160.83
u	253.76	1.00	.91	10.40	1.36	14.09	14.08	257.97	243.44	16.50	177.33
5	454.60	1.02	.93	10.40	1.36	136.04	135.36	394.01	378.79	62.00	239.33
6	610.77	1.01	•92	10.40	1.36	89.87	89.76	483.88	46 P . 55	49.67	248.00
7	876.31	1.01	.97	10.40	1.76	147.89	147.40	631.77	616.16	87.42	375.42
P	1055.24	1.04	.93	10.40	1.36	91.65	91.60	723.42	707.76	66.47	441.89
9	1367.17	1.72	.96	10.40	1 • 3 6	150.93	150.78	874.34	858.53	96.00	537.89
10	1640.07	1.03	.96	10.40	1.36	129.21	129.14	1903.56	987.68	P7.58	625.47
I 1	1017.83	1.96	•93	10.40	1.36	119.79	118.74	1122.33	1106.41	62.25	607.72
17	2247.49	1.02	.93	10.40	1.36	131.12	131.07	1253.45	1237.48	65.84	753.56
12	2567.02	1.00	.96	10.40	1 • 36	127.40	127.36	1380.85	1364.85	72.58	824.14
14	2811.60	1.02	• P 2	10.40	1.36	81.30	P1.29	1462.14	1446.13	75.84	899.98
15	2861.80	1.12	• ^{p 7}	10.40	1.36	10.98	18.98	1461.12	1465.11	42.25	942.23
16	2939.20	1 • C 7	.79	10.40	1.36	24.27	24.27	1505.39	1489.38	31.25	973.48

WASHINSTON METROPOLITAN ARF& 1RANSIT AUTHORITY CONTRACT NUMBER 1F0021 F2A RRANCH POUTE INBOUND WASHINGTON, C.C.

WEEK	CUMULATIVE FEET	OCEN HOURS COPRECTION	501L CORRECTION	5HIELO CORRECTION	EXCAVATING EQUIPMENT CORRECTION	WEEK * 5		CUMULATIVE		=======	AL HOURS
1	17.31	1.02	.92	10.40	1.36	45.09	39.48	45.09	39.46	14.92	14.92
2	137.04	1.01	.86	10.40	1.36	107.94	104.02	153.04	143.51	75.91	00.63
₹	130.31	1.07	.84	10.40	1.36	30.93	35.07	191.96	162.38	26.09	116.92
4	727.55	1.72	•72	10.40	1.36	137.31	135.91	329.27	310.29	85.50	202.42
5	527.16	1.03	.76	10.40	1.36	125.45	125.05	454.72	447.34	86.25	288.67
6	687.C4	1.00	.76	10.40	1.36	95.76	95.55	550.48	539.00	55.42	344.00
7	997.97	1.01	.77	10.40	1.36	161.62	161.30	712.10	700.29	103.83	447.92
£	1781.46	1.00	+ P 1	10.40	1.36	146.51	146.37	858.61	846.66	99.33	547.25
9	1581.61	1.00	.86	10.40	1.36	151.29	151.19	1009.90	997.86	97.75	645.0C
10	1679.66	1.02	• 9 (10.40	1.36	SI.14	51.14	1061.03	1048.99	64.82	709.62
I 1	1915.96	1.02	.79	10.40	1.36	105.DR	105.06	1166.12	1154.05	89.83	799.65
12	2130.52	1.01	. 23	10.40	1.36	99.58	99.57	1265.70	1253.61	96.92	896.57
13	2391.57	1.01	• B Z	10.40	1.36	107.44	107.42	1373.14	1361.03	82.49	979.06
1 4	2560.64	1.01	.78	10.40	1.36	66.98	66.9R	1440.17	1424.01	80.58	1059.64
15	2595.78	1.01	.7 t	10.49	1.36	13.63	13.63	1453.74	1441.63	38.16	1697.80
16	2845.01	1.01	.76	10.49	1.36	94.06	94.05	1547.81	1535.68	119.07	1216.87
I 7	2934.57	1.00	.72	10.49	I • 3 6	31.20	31.20	1579.01	1566.89	51.17	1268.04

washington Hetrocolitan area transit authority contract number ifc012 fig. Notice outeous vashington, 0.c.

CUMULATIVE FEET	COPSECTION	JIO2 AOITJ39HOD	SHIELO CORRECTION	EXCAVATING EQUIPMENT CORRECTION				========		L HOURS ======= CUMULATIVE
10.00	1.00	. 90	12.19	.68	32.94	30.42	32.94	3 ∩ + 4 2	39.00	39.00
39.00	1.06	.90	12.19	.68	30.20	30.04	63.14	60.45	38.90	77.90
140.00	1.00	_ on	12.19	.68	111.96	110.44	175.10	170.89	74.30	152.20
287.DG	1.09	. 93	12.19	.68	146.89	146.24	321.99	317.13	79.40	231.60
366.00	1.06	. 8 5	12.19	.68	70.97	70.92	392.96	388.05	74.80	306 • 40
418.00	1.00	• 77	12.19	.68	36.56	36.55	429.52	424.61	41.30	347.70
500.00	1 + 0 1	. 90	12.19	.68	58.84	58+83	48P + 36	483.43	77.80	425.50
60.00	1 • 0 3	. 8 4	12.19	.68	77.01	76.98	565.37	560.42	95.80	521.30
636.00	1.04	.76	12.19	• 6 8	20.41	20.41	585.79	587.83	44.70	566.00
700.00	1.70	• A 1	12.19	.68	49.46	48.45	634.25	629.28	62.60	628.60
737.00	1+93	.91	12.19	• 6 B	19.13	19.13	653.38	648.41	41.80	670.40
P30.00	1.05	- 8.5	12.19	•68	47.68	47.68	701.06	696.09	48.30	718.70
A 74 . DO	1+04	.85	12.19	• 6 8	51.14	51.14	752.20	747.23	49.10	767.80
950.00	1 - 1 1	.85	12 - 19	.66	55.68	55.68	PG7.88	102.91	4 . 40	813.20
975.00	1.00	.88	12.19	•68	16.92	16.92	R24.80	819.83	19.00	832.20
	19.00 39.00 140.00 287.00 366.00 418.00 509.00 636.00 709.00 737.00 874.00 959.00	1°.CS 1.00 3°.CO 1.06 14°.CO 1.06 14°.CO 1.00 36°.CC 1.06 41°.CO 1.06 41°.CO 1.06 41°.CO 1.01 60°.CO 1.03 63°.CO 1.04 70°.CO 1.03 63°.CO 1.04 70°.CO 1.05 63°.CO 1.07 73°.CU 1.03 63°.CO 1.04 60°.CO 1.07	10.00 1.00 .90 30.00 1.06 .90 140.00 1.00 .90 262.00 1.06 .85 418.00 1.00 .77 500.00 1.01 .80 636.00 1.03 .84 636.00 1.04 .76 700.00 1.05 .87 870.00 1.05 .85 870.00 1.05 .85	10.00	CUMBLETIVE FEET DOWN POURS CORRECTION CORRECTION CORRECTION SOIL CORRECTION CORRECTION SHIELD FOURMENT CORRECTION FOURMENT CORRECTION 1°.CO 1.00 .90 12.19 .68 3°.CO 1.06 .90 12.19 .68 1°.CO 1.00 .90 12.19 .68 26°.00 1.00 .93 12.19 .68 366°.CO 1.06 .85 12.19 .68 41°.00 1.00 .77 12.19 .68 50°.CO 1.01 .50 12.19 .68 636°.CO 1.04 .76 12.19 .68 70°.CO 1.00 .81 12.19 .68 80°.00 1.03 .96 12.19 .68 80°.00 1.05 .85 12.19 .68 80°.00 1.05 .85 12.19 .68 80°.00 1.05 .85 12.19 .68 80°.00 1.01 .85 12.19 .68 <th>CUMPLETIVE PETT DC.N POURS CORRECTION CORRECTION CORRECTION SHIELD CORRECTION CORRECTION CORRECTION CORRECTION CORRECTION CORRECTION CORRECTION CORRECTION CORRECTION INTEGRATION 1º.CO 1.00 .90 12.19 .68 32.94 3º.CO 1.06 .90 12.19 .68 30.20 1º.CO 1.00 .93 12.19 .68 111.96 26º.CO 1.06 .85 12.19 .68 70.97 41º.CO 1.00 .77 12.19 .68 36.56 50º.CO 1.01 .60 12.19 .68 58.84 60º.CO 1.03 .84 12.19 .68 77.01 636.CO 1.04 .76 12.19 .68 20.41 70º.CO 1.03 .96 12.19 .68 19.13 80°.CO 1.05 .85 12.19 .68 19.13 80°.CO 1.05 .85 12.19 .68 19.13 80°.CO 1.</th> <th>THELTIVE CORPECTION CORRECTION CO</th> <th> 10.00</th> <th> 10.00</th> <th> 10.00 1.00 .90 12.19 .68 32.94 30.42 32.94 30.42 39.00 </th>	CUMPLETIVE PETT DC.N POURS CORRECTION CORRECTION CORRECTION SHIELD CORRECTION CORRECTION CORRECTION CORRECTION CORRECTION CORRECTION CORRECTION CORRECTION CORRECTION INTEGRATION 1º.CO 1.00 .90 12.19 .68 32.94 3º.CO 1.06 .90 12.19 .68 30.20 1º.CO 1.00 .93 12.19 .68 111.96 26º.CO 1.06 .85 12.19 .68 70.97 41º.CO 1.00 .77 12.19 .68 36.56 50º.CO 1.01 .60 12.19 .68 58.84 60º.CO 1.03 .84 12.19 .68 77.01 636.CO 1.04 .76 12.19 .68 20.41 70º.CO 1.03 .96 12.19 .68 19.13 80°.CO 1.05 .85 12.19 .68 19.13 80°.CO 1.05 .85 12.19 .68 19.13 80°.CO 1.	THELTIVE CORPECTION CORRECTION CO	10.00	10.00	10.00 1.00 .90 12.19 .68 32.94 30.42 32.94 30.42 39.00

WASHINGTON HETROPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMBER 150012 FIR NORTH INFOUND WASHINGTON, C.C.

					EXCAVATING	WEEK * S	HOURS	CUMULATIVE	HOURS	ACTUA	L HOURS
WEEK	FEET	CORRECTION	CORRECTION	SHIELO CORRECTION	EQUIPMENT CORRECTION	INTEGRATION	SUMMAT I ON	INTEGRATION	SUMMATION	WEEKS	CUMULATIVE
1	32.00	1 • 70	• 9 🛭	12.19	.68	56.76	51.19	56 • 76	51.18	55.00	55.00
2	175.00	1.00	.89	12.19	• 6 B	149.66	145.56	706.42	196.74	65.60	120.60
3	284.00	1.00	.90	12.19	.75	IC3.57	103.29	309.99	300.03	77.20	197.80
4	357.0	1.02	1.02	12.19	.75	69 • 13	69.39	379 - 12	369 - 13	49.10	246.90
ĉ	434.00	1.04	. 87	12.19	.75	68.06	65.32	447.18	437.15	58.50	3∩€•40
6	466.00	1 + 0 1	.87	12.19	•75	25.04	25.94	472.22	462.18	64.80	376.20
7	63.152	1.76	* E C	12.19	.75	40.98	40.97	513 - 19	503 • 15	61.50	431 + 70
q	602.00	1.01	. A 4	12.19	.75	58.54	58.53	571.73	561.68	82.20	513.90
9	730.00	1.01	.86	12 • 19	.75	96.34	96.29	668.07	657.97	92.20	606.10
10	950.00	1.02	. 98	12.19	.75	78.29	78.27	746.76	736.24	67.70	666 - 80
1 1	048.00	1.02	• F 1	12.19	.75	61.84	61.83	808.20	798.07	58.10	724.90
12	075.00	1.12	.87	12.19	.75	19.66	19.66	827.86	817.73	24.50	749.40

WASHINSTON HETROPOLITAN ARFA TRANSIT AUTHORITY CONTRACT NUMBER 150012 FIR SOUTH OUTCOME NASHINSTON, O.C.

WEEK	CUMPLATIVE FEET	OCEN HOURS CORRECTION	501L CORRECTION	SHIELD CORRECTION	EXCAVATING EGUIPMENT CORRECTION	WFEK*5		CUMULATIV		=======	HOURS
1	7.50	1 • 1 2	1.19	12.19	.68	23.70	21.99	23.70	21.99	6.60	6.60
2	24.50	1.05	1 - 1 3	12.19	+68	37.98	37.51	61.69	59.50	25 - 20	31.00
3	42.50	1.04	1 + 0 7	12.19	-68	26.27	26.22	87.96	65.72	18.50	50.30
4	79.00	1.00	.98	12.19	•68	47.92	47.76	135.88	133.48	31.60	81.30
5	13.400	1 • 10	• 9 I	12.19	.68	66.94	66.77	202.81	200.24	51.50	132.80
6	194.00	1.10	•91	12.19	-68	66.26	66.18	269.07	266.42	57.40	190.20
7	277.00	1.05	.82	12.19	.68	73.58	73.50	342.65	339.92	61.40	251.60
8	35 ₹.00	1 - 13	. P 6	12.19	-68	72.25	72.21	414.90	412.13	78.60	330.20
9	419.00	1.01	.90	12.19	.66	56.45	56.44	471.35	468.57	59.70	389.90
10	437.50	1.16	•90	12.19	.68	11.13	11.13	482.49	479.70	10.00	399.90
11	440.00	1.18	.94	12.19	.68	18.89	16.89	501.38	498.59	25.70	425.60
12	510.00	1.07	• • 6	12.19	94.	51.51	51.50	552.89	550+10	62.10	487.70
1 3	570.00	1.06	.75	12.19	•68	48.44	48.43	601.33	598.53	68.7C	E 56 - 40
14	596.00	1.18	.77	12.19	.68	13.60	13.60	614.93	612.13	16.10	572.50
1 4	631.50	1.11	. 86	12.19	.68	29.45	29.48	644.41	641.61	53.70	626.20
16	704.00	1.13	.90	12.19	•68	63.22	63.21	707.63	704.83	65.50	691.70
17	P34.50	1.01	• 9 0	12.19	•68	76.73	76.72	784 - 36	781.54	77.70	769.40
1 0	02:•40	1.14	• 90	12.19	•68	45.34	45.33	829.69	826.88	52.00	821.40
19	950.50	1.06	.79	12.19	.66	76.59	70.58	900.29	897.46	68.50	#49.9C
20	1095.00	1.01	. 81	12.19	.68	81.71	81.70	982.00	970.16	126.80	1016.79

WASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMBER 1F0012 FIR SCUIT OUTSOUND WASHINGTON, O.C.

WEEK	CUMPLATIVE FEET	OOWY HOURS CORRECTION	501L COPRECTION	5H1ELO CORRECTION	EXCAVATING EDUIPMENT CORRECTION	WEEK*5		CUMULATIV		ACTU: EERS	L HOURS
21	1200.00	1.57	•81	12.19	.68	83.85	83.84	1065.84	1063.00	86.30	1103.00
22	1706.00	1+04	. + 4	12.19	+68	64.79	64.78	1130.63	1127.78	66.50	1169.50
2 1	1454.00	1.78	.97	12.19	+68	69.28	69.28	1199.91	1197.06	69.73	1236+20
24	1520.50	1.03	.87	12.19	.68	83.70	83.70	1283.62	1280.76	63.40	1321.62
25	1655.00	1.02	.85	12.19	• 6 B	82.01	82.00	1365.62	1367.76	84.70	1476.30

KEEK	CUMPLATIVE	DOWN HOURS CORPECTION	SOIL CORRECTION	SHIELO CORRECTION	EXCAVATING EQUIPMENT CORRECTION	MEEK*5		CUPULATIVE TRANSPORTED TO A TRANSPORTED			L HOURS
1	77.00	1.00	. 81	12.19	.68	93.73	86.90	93.73	86.9G	64.00	64.00
7	130.00	I • 1 0	.77	12.19	.68	69.37	69.11	163.11	156.01	73.90	1 77.90
3	257.00	1.00	.7€	12.19	.68	93.54	93.29	256.69	249.30	62.00	219.90
4	394.00	1.01	.81	12.19	.68	116.91	118.68	175.59	367.98	76.13	296.Cr
4	560.00	1.00	• ° 2	12.19	.68	129.02	128.88	504.62	496.86	85.6C	391.60
6	661.03	1.01	.76	12.19	.66	63+11	63.10	567.73	-50.96	54.40	476.00
7	802.00	1.01	. R C	12.19	.66	97.54	97.50	665.26	657.46	87.00	519.00
e	964.00	1.01	. R G	12.19	.63	108+43	108.39	773.69	765.85	89.20	6 18 . 20
9	1114.00	1.00	.79	12.19	.68	95.60	95.5A	P69.29	861.44	97.00	775.27
13	1247.00	1.00	• R 1	12.19	.68	84.71	84.70	954.01	946.14	91.00	706.20
11	1376.00	1.01	+ 9.1	12.19	3 6.	81.19	81.18	1035.20	1027.32	80.30	876.5C
12	14800	1.09	.87	12.10	• f P	77.08	77.98	1113.10	110 30	73.40	949.90
1 3	1 6 8 7 . 00	1.04	. 9 4	12.19	. + 6	63-13	63.1?	1176.31	1168.43	7:.30	1020.20
14	1654.00	1.92	.84	12.19	.68	45.61	45.51	1221.92	1214.04	62.30	1082.50

WASHINGION METROPOLITAN AREA TRANSII AUTHORITY CCVTPACI NUMBER 100001
C-9 SOUTH INBOUND WASHINGION, O.C.

WEEK	CUMPLATIVE FEET	OOWN HOURS CORRECTION	SOIL CORRECTION	SHIELO CORRECTION	EXCAVATING EQUIPMENT CORRECTION		S HOURS ======== n SJMMAT10N	CUMULATIV	=========	======	AL HOURS CUMULATIVE
1	20.30	1.02	.75	11.40	.82	72.81	65.98	72.91	65.88	94.75	94.75
5	117.93	1.04	.75	11.40	.82	143.36	140.61	216.17	206.49	105.00	109.75
3	217.90	1 • 0 4	. 8 2	I1.40	.82	157.47	156.71	373.65	363.20	111.33	311.08
4	307.90	1.09	.79	11.40	• ₹ 2	112.70	112.57	486.35	475.77	106.30	417. 68
5	37 - 93	1.07	.74	11.43	. 92	91.17	91.11	577.51	566.88	97.00	110.00
6	501.90	1.07	.75	11.40	•92	137.93	137.90	715.44	704.68	110.00	f 20 + 0 P
7	637.90	1.08	.75	11.40	.82	114.77	114.72	830.21	819.41	110.00	7 *0 . 0 8
8	590.90	1.00	.75	11.40	.82	88.42	88.43	918.63	937.81	107.00	F 17. DE
ç	724.90	1.12	.75	I1.40	.82	26.40	26.40	945.04	934.21	30.00	967.LF



Appendix A-4

Total downtime hours for each data set of each tunnel are calculated from equation (6.4).



-AY A-EA KAPIO TPANSII OISTRICT CONTRACI NUMBER IMOOSI MR TUNNEL - 24TH TO RANDALL SIREET SAN FRANCISCO, CALIFORNIA

⊨ E f	CUMULATIVE K FEET	S01L	ECUIPMENT/ DISTANCE CORRECTION	0.0 M M	ULATED HOURS CUMULATIVE		TUAL HOURS CUMULATIVE
	15.00	2 • 21	22.18	3 - 31	3 - 31	•00	•30
	47.50	2.21	22.15	7.16	10.46	7.50	7.50
	35.00	2 • 2 1	21.98	40.97	51.43	10.50	18.00
	132.50	2 . 2 1	21.65	20.99	72.42	79.00	97.00
1	\$52.°0	2.42	21.17	50.70	123.12	9.00	106.00
	00.084	2 • 4 2	20.54	28.50	151.62	22.00	128.00
	7	2 + 8 5	19.97	37.20	188.82	66.50	194.50
	1085.00	2 . 85	19.04	63.62	252.44	26.00	220.50
	1 777 . 50	2 + 6 1	17.68	60.85	313.29	26.50	247.00
1	1 *02 • 50	2.61	16.62	24.45	337.73	36.00	283.00
1	1657.50	2.61	15.91	29.02	366.75	43.00	326.00
1	1 950 - 00	2 - 61	15.05	34.08	400.84	30.00	356.00
1	1960.00	3.21	14.32	22.80	423.64	66.10	425.50
1	2050.00	3.21	13.85	18.05	441.68	8.00	433.50
1	5 2 300 - 10	3.21	13.09	47.38	489.06	33.50	467.00
1	257.50	3 • 21	12.04	44.89	533.95	36.00	505.00
1	7 2°57.50	3.21	11.02	47.88	581.84	25.00	530.00
1	8 3102.50	2 + 8 4	10.18	31 + 92	613.76	20.00	550 +00
1	9 3740.00	2.84	9.55	29.03	642.79	31.50	581.50
2	3597.50	7.47	9.03	78.17	720.95	26.50	60A .00

RAY AREA RAPIO TRANSIT OISTRICT CONTRACI NUMBER IMOD31 MR TUNNEL - 24TH TO RANDALL STREET SAN FRANCISCO, CALIFORNIA

WEEK	CUMPLATIVE FEET		OUIPMENT/ OISTANCE CORRECTION	DOWN	ULATEO HOUR5 CUMULAIIVE	00 8 6	TUAL HOURS CUMULATIVE
2 1	3 9 5 5 • 70	2.84	8.61	28.40	749.35	25.50	633.50
2.2	4102.50	2 . 8 4	9.34	26.43	775.78	28.50	662.00
2 *	4 297 . 50	2 . 8 4	8 . 2 2	20.52	796.30	37.00	699.00
2 4	4345.00	2 + 84	8 + 20	4.98	801.28	79.00	778.00
25	4425.00	3.85	8.20	11.38	812.66,	16.50	794.50

Appendix A-4. Calculation of Downtime Hours.

BAY AREA RAPIO TRANSIT DISTRICT CONTRACT NUMBER IMODIS ML TUNNEL - 24TH TO RANDALL STREET SAN FRANCISCO, CALIFORNIA

			DU IPMENT/		ULATEO		TUAL
WEEK	FEET	SDIL CORPECTION	CORRECTION		HOURS CUMULATIVE	MEEK S	HOURS CUMULATIVE
1	20.00	2 • 2 1	22+18	4 • 4]	4.41	f+50	6.50
7	52.50	2.21	22.15	7.16	11.57	6 • 5 C	13.00
3	175.30	2 • 21	22.03	26.83	38.39	44.50	57.50
4	735.00	2.21	21.72	34.56	72.95	31.00	A8.50
5	555.00	2.42	21.16	50.68	123.63	7.00	95.50
6	792.50	2 . 8 5	20.30	61.96	185+56	19.50	114 +00
7	1162.50	2 . 8 5	18.94	90.02	275.60	8.00	122.00
8	1 *50 + 00	2 • 6 1	17.55	38.73	314.33	17.50	139.50
9	1487.50	2.61	16.73	27.06	341.40	15.00	154.50
10	1515.50	2.61	16.31	5.28	346.67	110.00	264.50
1 1	1695.00	2 • 6 1	15.7A	33.43	389.11	35.57	300.00
17	1 470 - 00	2.61	14.91	30 - 6 9	410.80	27.00	327.00
1 3	1 - 35 + 00	3.21	14.33	13.48	424.29	61.Dr	388 - 00
14	1067.50	3 - 21	13.08	4 • 5 5	420.84	92.50	48C.5D
15	2162.53	3.21	13.53	34 • 2 9	463.12	54.00	514.50
16	2495.00	3 • 2 1	12.44	59.89	523.02	16.50	551.0C
17	2577.50	3.21	11.63	13.89	536.91	63.50	614.50
19	2787.50	3.21	11.11	33.78	570.69	10.00	633.50
1 9	3780.00	2 + 8 4	10.31	38 - 61	609.29	26.50	660.00
20	3265.00	2.84	9.64	25.30	634.65	24.50	684.50

BAY AREA RAPIO TRANSIT DISTRICT CONTRACT NUMBER IMPOSI ML TUNNEL - 24TH TC PANDALL STPEET SAN FRANCISCO, CALIFORNIA

	CUMULATIVE	EQUIPMENT/ SOIL PISTANCE		CALCULATED Down Hours		ACTUAL OOWN HOURS	
MEEK	FEET	CORRECTION	CORRECTION	WEEK 'S	CUMULAT1VE	WEEK *S	CUMULATIVE
2 1	3*10.00	2 • 6 1	9.17	24.81	659.41	27.5C	712.00
2.2	3745.00	7.47	P.72	83.56	742.97	25.00	737.00
2 3	4120.00	2 - 64	8.36	34.79	777.76	16.00	753+00
24	4280.00	2.84	8 • 2 2	16.83	794.59	12.50	765.50
25	4.60.00	3.85	8.20	15.69	e10.23	11.00	776+50

PAY AREA RAPIO TRANSIT DISTRICT CONTRACT NUMBER 180053 PRIRL TUNNELS BERKELEY, CALIFORNIA

			EQUIPMENT/		ULATED	U D M M	TUAL
WEEK	CUMILATIVE FEET	50IL CORRECTION	CORRECTION		HOURS CUMULATIVE	WEEK 15	CUMULATIVE
1	28.00	2 • 3 ª	2.44	.52	•52	12.00	12.00
2	90.00	2.38	2.44	1.62	2 - 14	.00	12.00
3	163.00	2 • 3 8	2.42	1.90	4.04	2.00	14.00
4	212.90	2.38	2.41	1 + 27	5 + 3 1	9.00	23.00
5	264.00	2 • 3 °	2 + 4 0	1.34	6.65	6.00	29.00
6	*20.00	2 • 3 9	2 • 38	1 • 4 3	8.08	1.00	30.00
7	*67.99	2 • 3 P	2.37	1.19	9.27	40.00	70.00
я	043.00	2.39	2 + 3 4	1 • 9 1	11.18	5.00	72.33
ç	E29.00	2.38	2 • 31	2 • 1 4	13.32	• C D	72.00
10	616.00	2 • 3 8	2.28	2.13	15.45	2.00	74.00
11	717.GO	2 • 3 0	2.24	2 • 31	17.75	9.00	83.00
12	771.00	2.38	2.20	1.40	19.15	2.70	e - • 00
13	862.DO	2.36	2 • 17	2.12	21.27	7.50	0C • 8 9
1 4	044.00	2.38	2.12	1 . 8 7	23.14	7.00	95.30
15	1916.00	1.31	2.08	.88	24.02	21.00	116.30
16	1~99.00	1 + 3 1	2.04	1.00	25.02	1.00	117.30
17	1157.00	1.31	2.90	•68	25.70	2.00	119.00
18	1725.00	1 • 3 1	1.97	. 00	26.50	•00	119.00
19	1290.00	1.52	1.93	.86	27.36	.00	119.30
20	1 774 - 00	1.52	1.89	1 - 09	28.45	1.00	120.00

RAY AREA RAPIO TPANSIT DISTRICT CONTRACT NUMBER 1RODS3 PR/RL TUNNELS BERKELEY, CALIFORNIA

	CUMULATIVE	501L	OUIPMENT/		ULATEO HOURS		TUAL HOURS
WEEK	FEET		CORRECTION		COMPLATIVE	WEEK '5	
21	1459.00	1.52	1 - 8 4	1.07	29.52	1.00	121.00
2.2	1474.00	1.52	1.81	.19	29.71	.00	121.00
2 3	1479.00	1.52	1.81	.06	29.77	•0C	121.00
24	1598.0G	5 - 20	1 • 7 7	4.94	34 • 71	5.00	126.00
25	1672.00	5.20	1672	2.98	37.69	2.70	128.00
26	1910.00	5.20	1.66	5.37	43.06	1.00	129.00
2 7	1943.00	5.20	1.59	4.95	48.02	9.00	137.30
2.8	2759.00	5 • 2 0	1.53	4.15	52.16	17.00	154.00
29	2 199 • 00	5 + 2 0	1.46	4.80	56.96	2.00	156.30
30	2329.00	5.20	1.40	4.26	61.22	8.00	164.30
31	2 468 • 00	5.20	1 + 3 6	1 . 2 4	62.46	51.00	215.00
32	2462.00	1 • 5 2	1 • 3 3	.86	63.32	3.00	218.00
33	2546.00	1.52	1.29	.74	64.36	4.00	222.00
34	2650.00	1 • 5 2	1.26	.89	64.96	1.00	223 • 00
35	2746.00	1.52	1.22	.80	65.76	•00	223.00
36	2410.00	1.52	1.19	•52	66.28	43.00	266.00
3 7	2086.00	1.52	1.16	.62	66.90	2.00	26 A . 00
3 H	2903.00	1 • 5 2	1.15	.12	67.01	.00	268.00

BAY AREA RAPIO TRANSIT DISTRICT CONTRACT NUMBER 150011 TR TUNNEL SAN FRANCISCO, CALIFORNIA

	CUMPLATIVE	EQUIPMENT/ SOIL PISTANCE			ULATEO HOURS	ACTUAL COWN HOURS	
WEEK	FEET		CORRECTION		CUMULATIVE	WEEK 'S	CUMULATIVE
1	47.43	4.17	89.74	16.96	16.96	1.00	1.00
2	194.73	2.21	29.44	27.67	44.63	3.50	4.58
3	362.07	2.21	30.10	10.70	55.33	3.40	7.96
4	c.6.85	2.51	20.32	14.48	69.82	3.74	11.72
ţ	446.74	7.89	10.99	18.74	88.56	18.5	39.27
6	°68.96	4.74	27.50	24.12	112.68	16.43	46.70
7	1716-23	2 + 2 1	26.14	12.62	125.30	12.92	59.62
Ą	1353.38	2 • 2 1	24.54	12.36	137.66	10.10	69.81
Q	1463.21	4.45	23.32	10.96	148.62	.00	69.81
1.7	1 < 1 = . 4 9	7.89	15.18	6.03	154.65	15.25	85.06
11	1 = 50 - 48	7.89	14.99	3.98	158.63	1.17	96 • 2 3

FAY AREA RAPIO TRANSIT DISTRICT CONTRACT NUMBER 150011 TL TUNNEL SAN FRANCISCO, CALIFORMIA

CJMULAT1VF			EGUIPMENT/ OIL CISTANCE		ULATED HOURS	ACIUAL DOWN HOURS	
WEEK	FEFT		CORRECTION		CUMULATIVE	MEEK'S	CUMULATIVE
		* **					
1	44.76	7.89	12.80	20.37	20.37	4.40	4.40
2	137.34	3.67	12.75	19.53	39.90	6.83	11.23
3	309.61	2.21	12.59	21.56	61.47	I - 9 1	13.14
4	469.43	2.21	6.33	10.06	71.53	1.00	14 - 14
¢	629.31	2 • 5 1	6.17	11-14	82.67	1.75	15 - 8 9
6	#26.69	2.51	5.96	13.28	95.95	6.86	22.77
7	1054.04	2.21	5.67	12.82	108.76	14.91	37.68
ρ	1~41	2.94	۲.34	15.5P	124.34	13.40	51.08
ç	1451.36	3.67	4.69	13.19	137.53	26.06	77.14
13	1"16.29	7.85	7.29	16.83	154.35	1.00	78.14
11	1551.29	7.89	7.18	6.93	163.28	2.92	91.06

HAY AREA HAPIO TRANSIT DISTHICT CONTRACT NUMBER ISCOII SR TUNNEL SAN FRANCISCO, CALIFORNIA

			CUIPMENT/		ULATED	ACTUAL DOWN HOUPS	
#EE#	CUMI'L AT TVF FEET	S^IL CORRECTION	CORRECTION		CUMULATIVE		CUMULTIAE
1	42.50	2 • 2 1	19.03	8.04	8.04	21.83	21.83
2	165.10	3 - 2 3	18.92	33.80	41.84	1.17	25.00
3	212.63	2 + 2 1	10.78	8.87	5 C • 7 1	1 • 5 9	26.59
4	₹2€.N3	3 + 2 3	6.44	10.55	61.26	10.17	76.76
5	089.91	3 • 2 3	6.32	15.18	76.44	5.67	42.43
6	454.75	5 • 3 0	6.15	24.58	101.02	9.27	51.70
7	939.32	4.17	5.94	20.60	121.62	14.00	65.70
8	1031.61	2.21	5.68	10.86	132.48	28.69	94.39
9	1236.34	2.26	5 - 3 9	11.26	143.74	.42	94.81
13	1415.75	2 • 2 1	5 • 1 1	9 - 11	152.A5	.00	94.81
11	1 = 5 2 + 94	2 + 21	4.24	5 • 7 9	158.63	12.50	107.31

BAY AREA RAPIO TRANSIT DISTRICT CONTRACT NUMBER 150011 5L TUNNEL 5AN FRANCISCO, CALIFORNIA

	CUMULATIVE	EQUIPMENT/ SOIL DISTANCE			ULATEO HOURS	ACTUAL DOWN HOURS	
WEEK	FEET		CORRECTION		CUMULATIVE	MEEK 'S	CUMULATIVE
1	29.93	2.21	114.82	2.02	2.02	.00	•00
2	109.53	7.89	114.43	19.13	21.15	.50	•50
3	209.45	7.89	113.60	23.83	44.98	6.75	7.25
4	326.95	7.89	112.31	27.70	72.68	3.50	10.75
5	386.93	7.89	111.03	13.98	86.66	8.00	18.75
6	525.83	7.89	109.39	31.89	118.55	8.75	27.50
7	639.23	2 - 21	107.01	7.12	125.67	9.41	36 - 91
8	796.72	2.21	104.16	9.63	135.30	5.75	42.66
9	851 - 61	2.21	101.75	3.28	138.58	4.00	46.66
10	981.25	2.21	99.54	7.57	146.15	25.42	72.08
11	1116.09	7.89	96.25	27.24	173.40	22.08	94.16
12	1295.74	2.21	92.20	9.72	183.12	6.41	100.57
13	1457.86	2.21	131.41	12.50	195.62	28.89	129.46
14	1565.19	2.21	84.17	5.30	200.93	5.33	134.79

BAY AREA RAPIO TRANSIT DISTRICT CONTRACT NUMBER 150051A 5L TUNNEL - MARKET STREET 5AN FRANCISCO, CALIFORNIA

WEEK	CUMULATIVE FEET	501L	EOUIPMENT/ DISTANCE CORRECTION	DOWN	ULATED HOURS CUMULATIVE		TUAL HOURS CUMULATIVE
1	85.00	2.85	130.53	5.18	5.18	3.67	3.67
2	152.50	3 • 2 3	129.95	7.55	12.73	17.78	21.45
3	220.00	2.51	129.16	5.81	18.54	17.14	38.59
4	280.00	2,21	128.29	4.52	23.06	3.58	42.17
5	350.00	2 • 2 1	127.28	5.23	28.29	2.08	44.25
6	457.20	2.51	125.71	8.98	37.27	10.17	54.42
7	564.70	2.21	123.56	7.80	45.07	6.32	6D • 74
8	689.70	2.21	120.95	8.87	53.94	11.68	72.42
9	729.70	2.21	118.94	2.79	56.74	7.01	79.43

FAY AREA RAPID TRANSIT CONTRACT NUMBER 150051A SR TUNNEL - MARKET STREET SAN FRANCISCO, CALIFORNIA

WEEK	CUMULATIVE FEET	SCIL	EQUIPMENT/ DISTANCE CORRECTION	DOWN	ULATED HOURS CUMULATIVE		TUAL HOURS CUMULATIVE
1	27.46	3.67	319.73	7.03	7.03	•00	.00
2	94.96	4 - 17	318.85	23.89	30.92	7.50	7.50
3	137-46	6 • 1 2	317.56	21.96	52.88	10.33	17-83
4	190.24	2.21	73.02	2.26	55.14	2 • 33	20.16
è	77 7. 46	5 • 38	72.50	9.06	64.20	9.15	29.31
6	² 84.96	4 - 17	71 . 6 4	8.55	72.75	17.28	46.59
7	477.46	2 • 21	70.62	3.83	76.58	5.42	52.01
۴	564.96	2 • 2 1	69.58	3.57	80.15	7 . 34	59.35
9	687.46	3 . 2 ?	68.24	7.19	87.34	9.17	68.52
10	709.96	3.23	67.25	1.30	88.65	11.75	80.27

			OU 1PMENT/		ULATED	ACTUAL DOWN HOURS	
	CUMPLATIVE FEET	STIL	DISTANCE CORRECTION		HOURS CUMULATIVE	WEEK'S	CUPULATIVE
MEEK	, , ,	CONTENTED					
1	24.00	10.46	4.26	4.81	4.81	8.00	9.00
2	38.00	9.46	4.25	2.54	7 • 3 5	26.30	36.00
3	130.00	9.46	4 • 2 4	16.62	23.97	6.00	42.00
4	210.00	3.58	4 • 2 1	5.44	29.41	24.00	66.00
	714.00	3.50	4.10	.27	29.68	5.00	71.00
6	742.00	12.82	4 • 1 8	6.76	36.44	36.00	107.00
7	265.00	2.65	4.17	1.14	37.58	12.00	119.00
8	284.00	2 . 6 5	4.16	. 94	38 + 53	4.00	127.00
9	358.00	2.99	4.14	4.12	42.65	20.00	147.00
10	410.CD	3.5€	4.10	3.44	46.09	21.00	168.00
11	*90.00	3.58	4.03	11.70	57.79	8.00	176.00
17	706.00	3.59	7.92	7.34	65.12	27.00	109.00
13	638.00	3.58	2.82	8 • 1 4	73.27	18.30	217.00
14	1 F94.CD	3 • 6 3	3.65	15.25	88.52	12.00	229.30
1 5	1762.00	2 • 6 3	3.4G	10.66	99.16	12.00	241.00
16	1466.00	3.38	3.22	5.10	104.25	27.50	268.5C
17	1 4 1 0 + 00	29.37	3.14	18.31	122.58	29.50	298.00
1 6	1530.00	21.68	3.11	6.08	128.66	4.00	302.00
19	1 586 • 00	9.78	3.08	7.59	136.26	F.50	310.50
20	1668.CD	12.47	3.01	13.67	150.13	13.00	323-50

UPPER SALT CREEK #1 CONTRACT NUMBER 68-404-25 CHICAGO, ILLINOIS

WEEK	CUMULATIVE FEET	501L	CUIPMENT/ DISTANCE CORRECTION	DOWN	ULATED HOURS CUMULATIVE		TUAL HOURS CUMULATIVE
21	1,22.00	5.11	2.90	10.26	160.40	11.50	335+00
22	2002.00	3.17	2.74	7.06	167.46	13.00	348.00
2 7	2 175 . 60	12.75	2.63	11.03	178.49	14.00	362.00
24	2739.00	10.26	2 • 5 3	19.17	197.66	7.00	369.00
25	2274.00	10.26	2.45	3.96	201.62	25.00	394.00
26	2 * 38 + CO	9.46	2.41	6.56	208.18	21.00	415.00
27	2 - 1 - 00	9.46	2+31	17.26	225.44	16.00	431.00
2 ¢	2 9 3 3 • 00	7.67	2.14	24.28	249.72	5.00	436.00
2 3	3041.00	3.58	1.98	6.64	256.36	11.00	447.00
30	3749.50	2 • 6 3	1.85	6.74	263.10	11.00	458.00
31	3425.10	12.59	1.73	27.02	290.12	13.00	471.00
32	3 9 5 3 • 00	2.55	1.65	4 - 32	294.44	19.00	490.00
3 3	4729.00	2 • 6 4	1.59	7.12	301.56	.00	490.00
3 4	4445.00	4.99	1.57	7.62	309.18	16.00	506.00
35	4725.00	10 - 15	1.59	20.35	329.53	6 • G O	512.00
34	4 9 7 7 . 00	9.41	1.63	10.49	340.02	14.50	526.50
37	5177.30	2 • 65	1.70	6.08	346.11	11.00	537.50
3 %	5461.00	2 • 6 5	1.86	6.74	352.85	13.00	550.50
39	5 6 8 1 • 00	2.65	2.17	10.34	363.18	5.00	555.50
4 ~	6167.00	9.46	2.66	32.45	395.64	16.50	572.00

UPPER SALT CPEEK #1 CONTRACT NUMBER 68-404-28 CHICAGO: ILLINOIS

WEEK	CUMPLATIVE FEET	SDIL	DUIPMENT/ DISTANCE CORRECTION	DOMN	ULATED HOURS CUMULATIVE		TUAL HOURS CUMULATIVE
4 1	6745.70	9 + 2 1	3.17	23.37	419.01	19.00	501.00
42	6445.00	9 • 2 1	3.56	14.77	433.77	20.00	611.00
4 3	6493.00	9.21	3 + 8 1	7 + 5 8	441.35	23.00	634.00
44	0.10°00	9.78	3.94	4.52	445.87	27.00	661.00
45	6565.00	9 - 21	4.08	7.78	453.65	20.00	6 P 1 + D D
46	6663.00	9 • 2 1	4.38	17.81	471.46	15.00	696+00
47	6 0 25 + 00	9 • 2 1	5.02	33.75	505.21	12.00	708.00
48	7073.00	2 • 5 7	6.36	18.3C	523.51	6.00	714.00

UPPER SALT CREEK #2 CONTRACT NUMBER 68-405-2S CHICAGO, ILLINOIS

*EER	CUMULATIVE	S01L	EQUIPMENT/ DISTANCE CORRECTION	DDWN	ULATED HOURS CUMULATIVE	DOWN	TUAL HOURS CUMULATIVE
1	46.00	2 - 6 5	+31	•17	•17	.00	.00
2	69.00	2.65	.31	• C 6	.25	.00	.00
3	172.00	2 • 6 5	• ? 1	.38	.63	16.00	16.00
4	765.00	2.65	4.40	11.16	11.79	5.00	21.00
5	063.00	2.81	4.12	30 - 16	41.96	P. DD	29.00
ě	1122.00	2 • 6 5	3.78	7.16	49.12	26 • D C	55.00
7	1671.00	16.14	3 • 4 2	136.42	185.54	26.00	81.00
8	1089.00	4.66	3.03	13.86	199.40	28.00	109.00
9	2784.00	2.73	2.69	16.36	215.76	17.00	126.00
10	3006.00	2.55	2.25	16.04	231.80	9.30	135.00
11	3110.00	1.57	2.02	1 - 4 9	233+29	13.00	148.00
12	3680.00	1.57	1.96	7.52	240.81	5.00	153.00
13	4791.00	2.90	1 • 7 1	9.18	249.99	17.00	170.00
14	4604.00	2.65	1.66	10.17	260.16	8.00	176.00
1 5	4972.00	11.70	1.72	33.34	293.50	15.0C	193.00
1.6	5717.00	9.46	1.05	26.93	320.42	10.00	203+00
•							

	CUMULATIVE	501L	OUIPMENT/ OISTANCE	CALC	ULATEC HOURS		TUAL HOURS
w E E K			COPRECTION		CUMULATIVE	WEEK'S	CUMULATIVE
1	20.00	2 • 65	• 3 P	+09	.09	30.00	30.00
2	104.00	3.58	5.52	7.49	7.58	12.00	42+00
3	268.00	11.01	? • 2 1	26.08	33.66	10.0C	52.00
4	₹88.00	3 • 5 8	5.38	10.42	44.08	17.00	69.00
5	526.00	3.58	5.28	11.76	55.84	9.00	78.00
6	678.00	2.99	5.14	10.52	66.36	1.00	79.00
7	942.00	10.05	4.98	36.99	103.34	9.00	88.00
8	1110.00	3.27	4.73	18.69	122-04	4.00	92.00
0	1236.00	10.58	4.49	25.69	147.73	56+00	118.00
1 C	1 737.00	9 + 3 2	3 • 3 4	15.05	162.77	27.00	145.00
11	1417.00	2.64	3+25	3 + 0 9	165+87	23.00	163.00
12	1 481.00	2.65	3 - 1 3	6.12	171.99	9.50	177.50
13	1781.00	2 • 6 5	2.96	7.05	179.04	8.00	185.50
14	1993.00	2.65	2.81	3.75	182.79	12.00	197.50
15	2153.00	2 • 6 5	2 - 64	8.19	190.99	3.00	200.50
16	2477.00	2.65	7 • 4 0	9.27	200.25	•00	200.50
17	2729-00	2.65	2.19	6.57	206.82	13.00	213.50
18	3^29.00	4.03	2.01	10.95	217.77	5.50	219.00
1 9	3 70 9 + 00	3.18	1.06	7.45	225-22	9.00	228.30
20	3 f 8 5 • C D	2 • 6 5	1 - 7 ?	7.72	232.94	2.00	230.00

UPPER SALT CREEK #3 CONTRACT NUMBER 68-406-25 CHICAGO, ILLINO15

		CUMPLATIVE	EDUIPMENT/ 501L 01STANCE		CALC	ULATEO HOURS	ACTUAL OOWN HOURS	
	MEEK	FEET	CORRECTION	CORRECTION	WEEK * 5	CUMULATIVE	WEEK'S	CUMULATIVE
	21	3 9 7 . 00	2.65	1.64	4.14	237.08	16.0C	296.00
	22	4297.00	2.65	1.59	7.56	244.64	3.00	249.00
	2 3	4665.00	2.65	1.58	5 • 4 1	250.05	1.50	250.50
	24	4726.00	2.65	1.60	2.69	252.74	16.00	266.50
	2.5	406.00	2 • 42	1 • 6 2	1 - 4 1	254.15	25.00	291.50
	24	4074.10	3 • 2 4	1.65	4.05	258.20	8.00	299.50
	27	5~66.00	2 - 65	1.74	6.06	264.27	3.00	302.50
	2 A	5582.00	2.65	1.93	7.26	271.53	3.50	306.00
	2 ¢	5038.00	3.31	2.20	8 • 4 2	279.95	9.00	315.00

WASHINSTON METROPOLITAN AFFA TRANSIT AUTHORITY CONTRACT NUMBER 1F0021 F2A PENIASON OUTPOUND WASHINSTON, 0.c.

CUMPLATIVE		EOUIPMENT/ 5016 DISTANCE		CALCULATED DOWN HOURS		ACTUAL Down Hours	
WEEK	FEET	CORRECT 10N	CORRECT 10N	wEEK*5	CUMULAT 1 VE	WEEK *5	
1	67.00	5.20	1.65	2 • 5 9	2.59	10.01	10.01
2	113.19	5.20	1.65	1 - 78	4.37	6.72	16.73
3.	288.08	7.89	1.63	10.13	14.50	8 + 8 2	25.55
4	*39.50	12.47	1 • 6 1	4.65	19.14	5.35	30.90
5	553.44	8 + 21	1.56	12.49	31.63	7.67	34.57
6	407.81	8 • 21	1.54	3.10	34.73	3.16	37.73
7	£10.28	5.20	1 + 5 3	.09	34.82	• 25	37.98
۵	7 02.€2	16.14	1.52	10 • 13	44.95	11.35	49.33
9	935.57	8 . 2 1	1.48	7.33	52 • 2 ê	16.95	66.28
10	1097.52	8 + 2 1	1 • 4 2	13.72	66.01	10.58	76.86
1 1	1 790.79	6.21	1.31	14.25	80.26	14.74	91.60
12	1408.25	8 • 21	1.25	. 6 1	81.07	• 5 8	92 • 18
5 6 7 9 10	553.44 607.81 610.28 702.02 935.57 1097.52 1790.79	8.21 8.21 5.20 16.14 8.21 8.21 6.21	1.56 1.54 1.53 1.52 1.48 1.42	12.49 3.10 .09 10.13 7.33 13.72 14.25	31.63 34.73 34.82 44.95 52.26 66.01	5.35 7.67 3.16 .25 11.35 16.95 10.58 14.74	30.90 34.57 37.73 37.98 49.33 66.28 76.86

WASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMBE? 1F0021 F2A PENTAGON INBOUND WASHINGTON, C.C.

			EQUIPMENT/		ULATED		THAL
wEEK	FEET	501L CORRECTION	O15TANCE CORRECTION		HOURS CUMULATIVE	WEEK *5	HOURS CUMULATIVE
1	7.50	5 - 20	1.65	.29	.29	• 0 0	.00
2	14.30	5.20	1.65	.26	•55	.00	.00
3	39.26	5.20	1.65	.96	1.52	.89	.89
4	41.68	5.20	1.65	•09	1 • 6 1	1.60	2.49
5	58.99	5.20	1.65	.66	2 • 2 7	3 • 0 0	5.49
۴	90.34	5.20	1.65	1 • 52	3.79	2.80	8 . 2 9
7	160.30	5 • 20	1.64	2.38	6.17	4.50	12.79
p	198.60	5 • 20	1.63	1.46	7 + 6 3	2.80	15.59
9	748+23	5.20	1.63	1.89	9.52	6.82	22 • 4 1
10	289.30	5 • 20	1.62	1.55	11.07	2 - 40	24.81
1 1	₹36.44	5.20	1.61	1.77	12.85	6.58	31.39
1.7	483.10	7.89	1.59	8 • 27	21.12	21.05	£2.44
13	672.94	16.09	1.54	23.85	44.97	4 + 0 8	56.52
14	139.07	24.50	1.40	27.43	72.40	16.95	73.47
15	909.19	24.5C	1.45	11.06	83.47	4.95	78.42
16	1 ~ 1 3 • 26	16.14	1.42	. 10.72	94.19	9.73	88 + 15
17	1040.43	8 • 21	1.39	1.40	95.59	1.00	89.15
1 8	1742.94	8 • 2 1	1.79	• 1 3	95.72	2 • 50	91.65
19	1149.31	6.21	1 • 3 7	5.39	101.11	32 • 47	124 - 12
20	1*19.62	16.14	1.32	16.30	117.41	9.60	133.72
21	1511.14	16.14	1 • 25	17.38	134.79	11+10	144.82

WASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMEER 1F0021 F2A BRANCH ROUTE QUIRDUNO WASHINGTON, D.C.

	CUMULATIVE SOIL				ULATEO HOURS		TUAL
WEEK			CORRECTION		CUMULATIVE		
1	69.89	6 • 6 4	1 • 6 5	3.45	3.45	2.42	2.42
2	າດ6 + 52	7 - 14	1 • 6 4	7.20	10.65	18.83	21.25
3	733.84	7.84	1 • 6 3	1.57	12.22	1 • 4 2	22.67
4	753.76	7.3C	1.62	1.06	13.28	•00	22.67
45	456.60	8.14	1.60	11.89	25.18	12.00	34.67
6	610.77	6 + 8 ?	1.55	7.36	32.54	5.83	90.50
7	e76.31	7.44	1.49	13.28	45 + 8 2	6 . C R	47.38
9	1:55 + 24	7 . 8 4	1.42	8 • 95	54.77	24+03	71.11
9	1 767 - 17	7.96	1.37	14.84	69.61	12.50	83.61
10	1648.07	7.67	1.21	11.78	81.39	20.92	104.53
11	1017.83	6 - 14	1.11	10.99	92.38	40+25	144.78
17	2742.44	7.84	1.01	11.55	103.93	17.66	162.44
1 7	2567.02	7.67	.90	10.15	114.08	2.92	165.36
14	2 4 1 1 • 6 0	4.99	.83	4.54	119.62	16.66	182.02
15	2063.80	4.07	.79	.76	119.37	11.2 5	193.27
16	2938.20	3.00	.76	•7F	120.15	13.75	207.02

WASHINGTON METROPOLITAN ARFA TRANSIT AUTHORITY CONTRACT NUMBER 1FC021 F24 88AM-H ROUTE INFOUND WASHINGTON, O.C.

	CUMPLATIVE	SOIL	LOUIPMENT/ 01 STANCE		JLATEO		TUAL
⊯EEK	FEET		CORRECTION	WEEK "S	HOURS CUMULATIVE	WEEK *S	HOURS CUMULATIVE
						• E E F S	CO-0C#114E
1	17.31	24.50	1.65	3.16	3.16	2.58	2.58
2	102.C4	12.72	1.65	8 • 0 1	11.17	10.59	13.17
3	139.31	7.12	1.64	1.96	13.13	R . 91	22.08
4	*27.55	8 . 8 1	1 • 6 2	12 - 13	25.26	13.00	35.08
5	522.16	5.13	1 • 5 8	7.12	32.39	12.25	47.33
6	687.C4	5.18	1 + 5 3	5.90	38.29	P • O A	55.41
7	993.97	6.05	1.46	12.21	50.49	7.67	63.08
2	1251.46	8 . 6 9	1.35	15.23	65.72	9.17	72.25
9	1581.61	13.16	1.24	22.10	87.82	10.75	83.00
10	1679.66	9.90	1.17	5.10	92.92	8.18	91.18
1 1	1915.98	9 • 5 3	1.11	11.22	104.14	10.67	101.85
12	2139.52	10.13	1.02	10.45	114.59	11.58	113.43
1 3	2 791 - 57	9.67	•95	10.40	124.99	7.51	120.94
14	2 4 60 • 64	14.84	.88	9.99	134.98	12.42	133.36
15	2595.38	10.02	. 6 6	1 - 34	136.33	4.34	137.70
1 +	2545.01	9.70	• R 2	9.01	145.34	13.93	151+63
17	2934.97	4.46	.78	1.40	146.74	1.83	153.46

WASHINGTON METROPOLITAN AREA TPANSIT AUTHORITY CONTRACT NUMBER 150012 F13 NOPTH OUTBOUNG WASHINGTON, C.C.

			CUIPHENT/		JLATED	ACTUAL ODWN HOURS		
WEEK	CUMULATIVE	SOIL	O 1 5T ANCE CORRECTION		HOURS CUMULATIVE		CUMULATIVE	
1	18.00	4.86	4.33	1.71	1.71	.00	.00	
2	39.00	4.86	4 + 3 3	1.99	3.70	6 - 10	6.10	
3	140.00	4.86	4 . 31	9.53	13.23	1.70	7.80	
4	262.00	5.83	4.26	15.89	29.12	16.60	24.40	
s	766.00	5.34	4.21	8.50	37.62	17.70	42.10	
6	418.00	3.12	4.17	3.05	40.67	2.20	44.30	
7	<00.00	3.39	4.13	5 • 1 7	45.84	8.20	\$2.50	
8	605.00	3.85	4.06	7 - 38	53.23	7.70	60.20	
9	F36.00	3 . 4 3	4.01	1.92	55.15	12.30	72.50	
10	709.00	3.79	3.97	4.94	60.09	3.90	76.40	
11	733.00	5.59	3.93	2 . 37	62.46	8 • 2 0	84.60	
12	•00.00	4.29	3.89	S . C 3	67.49	8.70	93.30	
13	974.00	4.29	3 . P 3	S • 47	72.97	7.90	101.20	
14	050.00	4.78	3.76	6.16	79.13	11.60	112.80	
15	075.00	4.86	3.71	2.03	81.16	.00	112.80	

WASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMBER 150012 FIR NORTH INBOUND WASHINGTON, O.C.

	CUMULATIVE SOIL		CUIPMENT/ DISTANCE		ULATEO HOURS	ACTUAL DOWN HOURS		
WEEK	FEET		CORRECTION		CUMULATIVE		CUMULATIVE	
1	32.00	4.68	4,33	2.92	2 • 92	1.00	1.30	
2	175.00	5.01	4.31	13.90	16.82	6.47	7 + 4 C	
3	784.00	4.68	1.90	4.36	21.18	3 • 30	10.70	
4	₹53.00	7.88	1.88	4.60	25.78	7.40	18.10	
s	434.00	6 - 8 9	1 • 8 6	4 - 67	30.45	8.00	26.10	
6	466.00	7.38	1.84	1.96	32.40	11.20	37.30	
7	×21.00	7.89	1.83	3.57	35.98	7.70	45.00	
Ą	F02.00	7.89	1 . 9 1	S - 2 O	41.18	3 . 80	48.80	
9	738.CO	7.89	1.77	8 . 5 5	49.73	3 • 30	\$2.10	
10	°50.00	7.89	1.72	6.86	56.56	3.80	55.90	
11	948.30	6 • 3 4	1.68	4.70	61.29	6.45	62.30	
12	975.CO	6.54	1.65	1 . 32	62.60	3.00	65.30	

WASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMBER 1F0012 FIR SOUTH OUTBOUND WASHINGTON, C.C.

			OUIPMENT/		ULATED	ACTUAL DOWN HOURS		
HEEK	CUMULATIVE FEET	SOIL CORRECTION	OISTANCE CORRECTION		HOURS CUMULATIVE	WEEK * S	CUMULATIVE	
	• • • • • • • • • • • • • • • • • • • •							
1	7.50	9 • 2 1	4.33	1.35	1.35	9.40	9.40	
î	26.50	8 • 1 3	4 • 3 3	3.01	4.36	14.80	24.20	
3	42.50	7 • 1 7	4.33	2 • 2 4	6.60	5.50	29.10	
4	79.20	6.33	4.32	4.50	11.09	2.00	31.70	
ē	135.00	4.95	4.31	5.37	16.47	12.50	44.20	
ť	195.00	4.95	4.28	5.73	22.20	20.10	64.30	
7	277.00	3.39	4.25	5.33	27.53	16.10	A0 -40	
A	*53.00	3.85	4 • 2 1	5.55	33.08	24.90	105.30	
9	010.CO	4.36	4.17	5.40	38.48	11-80	117.10	
19	430.50	4 • 3 6	4.15	.94	39.41	6.00	123.10	
11	449.00	4.93	4.14	1.70	41.11	5.30	128.40	
17	10.00	4 • 1 3	4 • 1 1	4.67	45.78	7.40	135.80	
13	·79.00	3.65	4.07	9.61	50.39	28.9	144.60	
14	69.00	3 • 6 5	4.03	1.19	51.58	7.40	152.00	
15	631.50	3.05	4.01	2.47	54.05	8.80	160.80	
1 6	704.00	4.01	3.97	5.20	59.25	20.00	140.80	
17	PG4.50	4 - 0 1	3.90	7.08	66.33	9.80	190.60	
18	•58•↑0	3 - 6 9	3.83	3.41	69.73	18.00	208.60	
1 ¢	050.50	3 - 4 3	3.76	5.90	75.64	19.00	227.60	
20	1692-00	4.47	3.66	9.24	84.88	11.20	234.80	

NASHINGTON HETPOPOLITAN AREA TPANSIT AUTHORITY CONTRACT NUMBER 1F0012 FIF SOUTH OUTPOUNO NASHINGTON, C.C.

			EGU IPHENT/		ULATED	ACTUAL		
	CUMULATIVE	501L	T1STANCE		HOUR5	00 M M	HOURS	
HEEK	FLET	CORRECTION	CORRECTION	wEEK*5	CUMULATIVE	WEEK +5	CUMULATIVE	
21	1209.00	4.47	3.54	8 . 8 3	93.71	16.20	255.00	
22	1,06.00	4.71	3 • 4 3	7.06	100.77	9.50	264.50	
2 3	1404+00	4 - 6 1	7+33	6.78	107.55	17.30	281.80	
24	1 * 2 9 • 50	4 - 6 1	3.22	8.39	115.94	12.10	293.90	
2 -	1659.00	4.88	3.09	8.81	124.75	10.80	304.70	

WASHINGTON METPOPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMBED IFCOIZ FIR SCUIM INPOUND WASHINGTON, D.C.

			CU 1PMENT/		ULATED	ACTUAL DOWN HOURS		
WEEK	CUMPLATIVE SEE1		DISTANCE CORRECTION		HOURS CUMULATIVE			
							_	
1	72.00	4.37	4.33	6.14	6.14	7.50	7.50	
2	139.00	4.44	4.31	5.77	11.91	24.10	31.60	
?	752.00	3.65	4 • 2 7	7 + 9 3	19.84	5.50	37.IC	
4	196.00	3.79	4.21	10.46	30.32	0.90	47.00	
¢	569.00	3 • 3 9	4 • 1 1	10.68	41.01	1.97	48.90	
6	461.00	3.67	4 • 0 1	6 • 17	47.16	2.10	51.00	
7	F02.00	3.87	7.92	9.53	56.71	5+00	56.00	
9	n64.00	4.08	3.79	11.29	67.99	4.30	60.30	
9	1114.00	3.73	3.64	9 • 1 7	77.17	2.00	62.30	
10	1247.00	4.47	3.50	9.38	86.55	1 - 0 0	63.30	
11	1776.00	4.31	3.37	8.45	95.00	3.70	67.00	
12	1465.03	4.61	3.26	7 • 37	102 • 37	14.10	81.10	
1.7	1.85.00	4.54	3.15	6.26	106.63	11.70	92 + 80	
14	1654.00	4.54	3.07	4.52	113.15	4.20	97.00	

WASHINGTON METROPOLITAN AREA IPANSIT AUTHORITY CONTRACT NUMBER 100091 C-9 SOUTH INCOUND -ASHINGTON, O.C.

WEEK	CUMPLATIVE	SOIL	EOUIPMENT/ (ISTANCE	0.0 % M	HOURS HOURS		TUAL
		CC-RECTIEN	CORRECTION	WEEK*S	CUMULATIVE	MEEK 'S	CUMULATIVE
1	28.00	2.65	8.00	2.67	2 • 6 7	1.25	1.25
?	112.90	2 • 6 5	7.97	8 . 6 7	10.74	12.00	13.25
3	217.90	2 • 8 8	7.91	10.76	21.50	8 - 17	21.42
9	*00.90	2.76	7.84	8.08	29.58	24.00	45.42
5	378.90	2 • 6 5	7.76	7 • 2 1	36.79	14.00	59.42
6	°01.90	2 • 6 5	7.64	11.20	47.99	25.00	84.42
7	667.90	2 • 6 5	7.50	9.47	57.46	20.00	104.42
ë	K9c.90	2 • 6 °.	7.36	8.06	65.53	00.9	112.42
9	724.90	2.65	7 . 2 7	2 • 16	67.69	8.00	120.42



Appendix A-5

The calculated rate of advance data of Appendix A-3 is combined with the downtime estimates of Appendix A-4 to give an estimate of the total tunneling shift hours for each data set of each tunnel. The percent error of the tunnel's cumulative hours relative to the reported hours is shown.



BAY AREA RAPIO TRANSIT DISTRICT FONTRACT NUMBER IMOD31 MR TUNNEL - 24TH TO RAMDALL STREET SAN FRANCISCO, CALIFORNIA BAY AREA RAPIO TRANSIT OISTRICT CONTRACT NUMBEP IMDO31 ML TUNNEL - 24TH TO RANDALL STREET SAN FRANCISCO, CALIFORNIA

wE E	CUMULATIV CALCUL K INTEGRATION	ATEO	CUMULATIV Hours- actual	1 DIF	FERENCE ON SUMMATION	WEEK 1	CUMULATIV CALCUL INTEGRATION	DETA	CUMULATIV HOURS- ACTUAL	% OIFF	ERENCE IN SUMMATION
1	33.46	29.53	8.00	-318.24	-269.10	1	43.66	38.86	39.50	-13.40	94
2	P A3.72	78.99	47.50	-76.24	-66.30	2	92.23	86.91	79.00	-16.75	-10.02
2	270.50	261.10	168.00	-61.01	-55.42	3	254.00	246.16	199.50	-27.32	-23.39
	353.22	343.70	288.00	-22.65	-19+34	4	414.34	405.76	319.50	-29.69	-27.00
5	522.56	512 - 58	409.00	-2P+0P	-25.63	5	593.55	<84.50	439.50	-35.05	-32.99
6	614.53	604.51	486.00	-26.45	-24 + 3 8	6	782.97	773 - 69	560.00	-39.82	-38.16
7	7 721.48	711+42	606.50	-18.96	-17.36	7	1053.30	1043.72	680.00	-54.91	-53.49
6	903+30	893-10	726.50	-24.34	-22.93	8	1176.98	1167.29	757.50	-55.38	-54 - 10
	1003.16	1072.86	847.00	-27.88	-26.67	9	1263.36	1257.66	835.50	-51 - 21	-50.05
10	1161.87	1151.56	967.00	-20 • 15	-19.09	10	1281.48	1271.56	955.50	-34 • 12	-33.08
11	1256.03	1247.71	1067.00	-15.73	-14.76	11	1393.77	1364.06	1075.00	-29.65	~2 * . 75
12	1365.13	1354.80	1207.00	-13.10	-12+75	1?	1500 - 12	1490.39	1195.00	-25.53	-24.72
1.3	1445.22	1434.88	1326.50	-8.95	-0.17	13	1558 - 45	1548.72	1315.00	-18.51	-17.77
14	1497.56	1487.23	1446.50	-3 +5 3	-2.82	14	1638.62	1585.61	1435.50	-14.15	-19.46
1 4	1639.96	1629+61	1566.00	-4.72	-4.0€	15	1759.11	1706.09	1555.50	-13.39	-9.68
16	1780.78	1770+40	1686.00	-5 - 6 2	- c + O 1	16	1951.66	1898.81	1676.00	-16.46	-13.29
1 7	1972.85	1922.46	1906.00	-7.02	-6 • 4 5	17	2014.36	1961+31	1795.50	-12-19	-9 + 2 3
1 6	2046.12	2035.72	1926+00	-6.24	-5.7C	1.8	2130-45	2077.36	1915.50	-11.22	4 5
1 9	2154.47	2144.06	2045.50	-5 . 3 3	-4 + 8 2	19	7274.37	2220.99	2036.00	-11.69	-9.09
2.0	?326.96	2316.54	2166.00	-7.43	-6.95	2.0	2374 • 1 2	2321-10	2155.50	-10.15	-7.68
2	1 2434.53	2424.11	2286.53	-6.47	-6.02	21	2420.67	2429.42	2275.00	-9.04	-6.79
2	2 2537.60	2527.17	2407.00	-5.43	-4 + 9 9	22	2679.24	2627.97	2395.00	-11.87	-9.73
2	3 7618.86	260A.43	2527.00	-3.64	-3.72	2.3	~821.44	2770.16	2515.00	-12.18	-10.15
21	4 7652.8P	2642.45	2647.00	2 2	-17	24	2891.15	2839.97	2635.50	-9.70	-7.75
2 !	5 7697.54	2677.11	2719.50	1.18	1 - 5 6	25	7942.57	2891.29	2747.50	-7.10	-r + 2 3

Appendix A-5. Total Estimated Shift Hours and Percentage of Error.

SAY AREA RAPIO TRANSIT DISTRICT CONTRACT NUMBER IRODS3 RR/RL TUMNELS RERKELEY, CALIFORNIA MAY AREA RAPIO TRANSIT DISTRICT CONTRACT NUMBER 150011 TR TUNNEL SAN FRANCISCO, CALIFORNIA

RERKELEY. CALIFORNIA					SAN FRANCISCO, CALIFORNIA						
WEEK	CUMULATIV CALCUL INTEGRATION	E HOURS ATEO Summation	CUMULATIV HOURS- ACTUAL	E % DIFFE INTEGRATION	RENCE SUMMATION	b EEK	COMULATIV CALCUL INTEGRATION	ATED	CUMULATIV HOURS- ACTUAL	12 D T F F	ERENCF IN SUMMATION
1	153.76	92.52	88.00	-74.72	-c.13	1	94.94	83.08	64.08	-48.16	-29.65
2	354.05	289.72	208.00	-70.21	-39.29	2	250.66	234.95	182.50	-37.35	-28.74
3	547.82	482.65	328.00	-67.32	-47.15	3	110.44	393.75	298.66	-37.43	-31.84
	680.83	615.55	448.00	-51.97	-37.40	4	580.74	563.51	417.99	-38.94	-34.81
•		743.84	568.00	-42.46	-30.96	5	702.22	684.91	535.98	-31.02	-27,79
5	809+19 930+73	865.32	688.00	-35.28	-25.77	6	850.06	832.62	651.78	-30.42	-27.75
6	1065.33	999.89	808.00	-31.85	-23.75	7	998.04	980.48	767.06	-30.11	-27.82
•		1151.16	924.90	-31.11	-24.05	c	1142.48	1124.83	885.65	-29.00	-27.01
9	1216.67	1314.76	1048.00	-31.71	-25.45	9	1209.03	1191.37	1004.31	-20.38	-18.63
	1380.33	1975.63	1168.00	-31.96	-26.34	10	1247.76	1230.10	1117.18	-11.69	-10.11
10		1649.47	1288.00	-33.16	-29.06	11	1286.28	1268.62	1222.30	-5.23	-3.79
11	1715 - 14	1752.44	1364.00	-32.90	-29.10						
12	1618.12	1906.67	1488.CO	-32.55	-28.14	BAYA	REA RAPIO TR	ANSIT DISTRI	I C T		
1.7	1972.37	2045.48	1608.00	-31.29	-27.21	CONT?		57011			
1 4	2111.20		1728.00	-29.07	-25.26	SA's F	RANTISCO, CA	LIFORNIA			
15	2230.26	2164.54	1848.00	-27.12	-23.57		CALCUL	ATEO	CUMULATIV	\$ 01FF	ERENCE
16	2349.27	2283.49	1944.00	-25.10	-21.72	MEEK	INTEGRATION	SUMMATION	ACTUAL		N SUMMATION
17	7431.97	2366.23	2040.00	-23.83	-20.67	1	92.09	82.61	102.25	9.94	19.21
18	2526.04	2461.69	2160.00	-21.59	-18.61	2	202.08	191.00	221.75	8.87	13.87
19	2626.37	2562.00		-20.82	-14.00	3	353.30	340.66	338.25	-4.36	71
20	2754.83	2690.43	2280.0C	-20.02		4	533.24	520.45	432.25	-23.36	-20.40
21	2882.79	2919.42	2400.00	-20.12	-17.43	5	696.98	683.99	527.58	-32.11	-29.65
22	7905.04	2840.70	2520.00	-15.28	-12.73	6	889.14	P75.94	646.16	-37.60	-35.56
2 3	2912.49	2848.12	2640.00	-10.32	-7.88	7	1093.64	1080.26	763.66	-43.2I	-41.46
24	3045.29	2980.90	2760.00	-10.34	-R.00	8	1290.64	1277.15	882.16	-46.30	-44.78
25	7126.37	3061.98	2840.00	-10.08	-7.82	9	1442.07	1428.55	1000.46	-44.14	-42.79
26	7274.03	3209.63	2960.00	-10.61	-8.43	1 C	1505.37	1491.85	1117.96	-34.65	-33.44
27	7416.46	3352.05	3080.00	-10.92	-R.83	11	1557.81	1544.28	1196.54	-30.19	-29.06
28	7542.47	3478.06	3200.00	-10.70	-9.69						
29	76P5.03	3620.61	3320.00	-10.99	-9.05	PAY A	REA RAPIO TRA	NSIT DISTRI	C T		
30	₹817.29	3752.87	3440+00	-10.97	-0.00	SR TU	NNE L				
31	3670.99	3806.56	3560.00	-8.74	-4.93	SAN F	RANCISCO. CAL				
32	7995.57	3931.14	3680.00	-8.58	-6.82		CUMULATIVE CALCULA	TEO	CUMULATIVI HOURS-	\$ DIFF	ERENCE
3 3	4106.90	4042.47	3800.00	-8.08	-6.38	WEEK	INTEGRATION	SUMMATION	ACTUAL	INTEGRATIO	SUMMATION
34	4240.94	4176.51	3920+00	-8 • 19	-6.54	1	91.60	81.06	77.25	-18.57	-4.93
35	9363.48	4299.04	4040.30	-8.01	-6.91	2	243.20	229.88	193.50	-25.69	-1A.80
36	9469.17	4404.73	4160.00	-7.43	-5 - 8 8	3	290.26	276.90	239.33	-21.28	-15.70
37	4568.06	4503.62	4280.00	-6.73	- 5 • 2 2	4	415.76	402.10	334.33	-24.36	-20.27
3 8	4586.87	4 . 22 . 43	4400.00	-4.25	-2.78	5	582.00	567.96	453.00	-28.45	-25.36
						6	736.77	722.52	571.16	-28.99	-26.50
						7	892.12	877.79	685.99	-30.05	-27.96
						8	1046.34	1031.92	805.91	-29.83	-28.04
						0	1191.86	1177.37	923.33	-29.08	-27.51
						10	1313.55	1299.C3	1018.75	-28.94	-27.51
						1 1	1472.75	1458.22	1115.33	-32.05	-30.74

UPPER SALT CREEK #1 CONTRACT NUMBER 68-404-25 CH1CAGO, ILLINO1S

SAN	FRANCISCO, CA	LIFORNIA									
WEE	CALCUL CALCUL K 1917GRAT10%	E HOURS ATEO SUMMATION	CUMULATI: HOURS- ACTUAL	\$ 01FF	ERENCE ON SUMMATION	WEEK :	CUMULATIV CALCUL NTEGRATION	ATED	CUMULATIN HOURS- ACTUAL	% OIFF	ERENCE N SUMMATION
1	77.75	65.82	109.33	28.89	39.80	1	33.41	28.91	33.50	. 28	19.01
2	202.23	187.58	225.99	10.51	17.00	2	46.21	41.57	77.50	40.37	46.36
3	328.71	313.30	344.91	4.70	9.16	3	112.67	106.80	127.50	11.63	16.24
4	455.76	439.99	460.03	1.10	4.52	4	146.69	140-69	176.50	16.89	20 • 29
ė	515.55	499.76	526.50	2.08	5.08	5	149.42	143.42	184.50	19.02	22.27
6	646.25	630.29	643.75	~0.39	2.09	6	172.76	166.76	234.50	26.33	28.89
7	729.48	713.47	734.73	0.66	2.84	7	183.73	177.72	264.50	30.54	32.81
5	834.35	818.26	845.66	1.34	3.24	8	190.96	184.96	282.50	32.40	34 + 5 3
9	870.26	854.16	938.56	7.28	8.99	9	219.56	213.54	.32.50	33.97	35.78
10	951.38	935.24	1056.06	9.91	11.44	10	239.22	233.19	371 +50	35 - 61	37 • 2 3
11	1066.42	1050.26	1176.56	9.36	10.73	1 1	294.56	288 • 42	419.50	29.78	31.25
12	1168.36	1152.16	1295.06	9.78	11.03	1.2	329.83	323.67	469.00	29.52	30.84
1 3	1257.38	1241.16	1407.90	10.69	11.84	1.3	366.11	359.93	514+00	28.77	29.97
1 4	1350.79	1334.57	1488.0€	9.22	10.31	1 4	436.96	430.71	564.00	22.53	23.63
						15	500.50	494.2I	614.00	18.48	19.51
0341	AREA RAPIO TR TRACT NUMBER 1	S0051A	1 C T			16	531.20	524.91	658.00	19.27	20.23
	TUNNEL - MAPKE FRANCISCO, CA					1 7	565.72	559.43	699.50	19.13	20.03
	CUMULATIV		CUMUL ATT			1 8	576.53	570.23	715.50	19.42	20.30
₩ 8 8 W	CALCUL	SUMMAT10N	MOUPS-	1 DIFF	ERENCE IN SUMMATION	1 9	599.G3	692.73	765.50	21.75	22.57
1	285.14	135.57	116.03	-145.75	-16.84	2 ^	633.34	627.05	PI1.50	21.95	22.73
5	430.72	280.31	227.89	-89.00	-23.00	21	677.96	671.66	861.50	21.31	ž2.04
7	553.18	402.48	341.47	-62.00	-17.87	22	720.67	714.36	911.50	20.94	21.63
4	645.19	494.40	427+41	-52.38	-16.77	2 *	744.48	735.18	959.50	22.41	23.07
r	739.65	588.78	504.09	-46.47	-16.59	2 4	797.61	791.30	1007.50	20.83	21.46
4	877.63	726.59	621.19	-41.28	-16.97	25	811.11	804.80	1051.50	22.86	27.46
7	1002.85	851.71	737.61	-35.96	-15.47	26	831.18	°24.°7	1095.50	24.13	24.70
^	1154.33	1003.09	P52.78	-35.36	-17.63	27	877.64	F71+32	1142.50	23.18	27.74
9	1232.30	1081.06	909.25	-35.53	-18.90	2 6	955.47	949.08	1192.50	19.88	20.41
PAY	AREA RAPIO TP	ANSIT				29	990.03	983.70	1228.50	19.41	19.93
3 4 1	MUNET - MUDKE	I STRFFT				30	1045.67	1039.33	1278.50	18.21	10.71
	FRANCISCO, CAI					3 1	1106.97	1100 • 63	1328.50	16.68	17.15
» F F K	CALCULATIVE CALCULATION	ATED	CUMULATIV HOURS-	\$ 01FF	ERENCF	32	T143.47	I137.13	1379.50	17.05	17.51
1	74.76	SUMMATION	ACTUAL	INTEGRATIO	V SUPMATION	3 3	1202.43	1196.07	1423.50	15.53	15.98
2	179.52	50.54	66.30	-13.27	23.42	3 4	T240.73	1234.38	1461.50	15.11	I¢.54
3	247.24	153.15	183.75	2.30	16.65	3 5	1304.00	1297.64	1501.50	13.15	13.58
4	327.71	220.76	246.42	-0.33	10.44	36	1340.0P	1333.72	1539.50	12.95	17.37
	437.10	301.06	323.42	-1.33	6.91	3 7	1393.85	1377.48	1587.50	12.83	13.23
1.	563.74	410.19	439.76	0.49	6.62	3.8	1428.91	1422.55	1637.50	12.74	13.13
,	657.86	536.58	557.16	-1.18	3.70	39	1486.90	1465.53	1687.50	11.89	12.27
ų	747.58	630.61	640.85	-2.65	1.60	4 C	1558.06	1551.69	1737.50	10.33	10.69
9	859.73	720.29	721.45	-3.62	0.16	4.1	1609.31	1602.94	1787.50	9.97	10.33
10	894.70	832.36	A 36 - 14	2 32	0.45	42	1640.78	1634.41	1837.50	10.71	11.05
		867.33	P8 - 64	-1.02	2.07	43	1656.82	1650.45	1885.50	12.13	12.47
						44	1667.92	1661.55	1929.50	13.56	13.89
						45	1683.42	1677.05	1975.50	14.78	15.11
						46	1717.72	1711.35	202*-50	15.11	15.43
						4 7	1776.19	1769.82	2071.50	14-26	14.56
						4.9	1831.90	1025.02	2121.50	13.65	13.95

UPPER SALT CREEK #2 CONTRACT NUMPER 68-405-25 CHICAGO, ILLINOIS

WASHINGTON METPOPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMBER 1F0021 F24 PCNTAGON OUTROUNC WASHINGTON, D.C.

	CALCUL		CUMULATIV HOURS-	E S OIFF	FRENCE	CUMULATIVE HOURS CALCULATED		CUMULATIVE HOURS- % DIFFERENCE		FRENCE	
WEEK	1NTFGRATION		ACTUAL		N SUMMATION	WEEK 1	INTEGRATION		ACTUAL		N SUMMATION
1	23.65	19.20	40.00	40.87	50.50	1	97.26	86.60	88.50	-9.90	7 - 1 4
2	30.95	27.08	57.00	45.70	57.49	2	146.70	135.87	122.50	-19.76	-10.92
3	57.57	53 - 31	103.00	44.10	48.24	3	344.49	331.59	215.00	-60.22	-54.23
4	105.54	100.86	149.00	29.16	32.31	4	398.74	385.84	242.00	-64.77	-59.44
<u>\$</u>	206.88	201.14	212.00	2.41	r +12	5	577.12	563.69	315.00	-82.92	-74.67
6	231-81	226.56	252.00	8 • 0 1	10.29	6	614.22	600.79	342.00	-79.6C	-75.67
7	417.44	411.55	319.00	-30.86	-29.01	7	615.61	602.18	349.50	-76:14	-77.30
8	453.15	447.25	363.00	-24.84	-23.21	a	683.28	660.83	398.00	-71.68	-68.30
9	511.41	505.47	416.00	-22.94	-21.51	9	769.59	756.12	492.50	-56.26	-53.53
10	575.39	569.40	476.00	-2C.88	-19.62	10	946.97	934 . 34	600.50	-58.03	-55.76
11	585.89	579.89	494.00	-16.6C	-17.39	11	1136.37	1124.61	711.0C	-60.11	-58 - 17
12	636.68	630.67	538.00	-18 + 34	-17.22	12	1149.32	1135.56	728.50	-57.77	-588
13	673.28	667.26	586.00	-14.89	-13.87						
19	717.33	711.3C	629.00	-14.04	-17.08						
15	776.13	776.09	669.00	-16.01	-1 * +11						
16	827.84	821.80	703.00	-17.76	-16.90						
1.000		_									

UPPER SALT CREEK #7 CONTRACT NUMPER 68-406-25 CHICAGO, ILLINOIS

WASHINGTON METROPOLITAN APEA TRANSIT AUTHORITY CONTRACT NUMBER 150021 F2A PENITGON INPOUND WASHINSTON, C.C.

	CUMULATTO	C				WASH	1721 CM. C.C.				
HEEK	CUMULATIV CALCUL INTEGRATION	ATEC	HOURS-	\$ 01FFE			CUMULATIN	E HOURS	CUMUL # T11	v E	
1			ACTUAL	INTEGRATION	SUMMATION	WEEK	CALCUL INTEGRATION		HOUR5-	1 01F	FERENCE On SUMMATION
	22.68	19.24	40.00	43.3C	51.89	1	21.27	18.87	9.50		
2	63.11	58.40	90.00	21+11	27.00	?	34.53			-123.93	-98.68
7.	142.39	136.89	120.00	-18.66	-14.08	3		32.06	17.78	-94.22	-8C.33
4	190.63	175.07	160.00	-12.89	-9.42		74.57	71.06	56.78	-30.36	-25.14
5	218 +54	212.93	200.00	-9.27	-6.47	4	78.31	75.34	66.78	-17.26	-12.82
6	257.06	251.42	223.00	-15.27	-12.75	5	102.66	99.66	98.28	-4.46	-1 - 4 1
7	329.20	323.13	263.00	-25.21	-23.05	6	146.65	145.49	139.28	-6.73	-4 . 4 6
٩	389.01	163.29	303.00	-28.39		7	212.36	209.00	181.78	-16.82	-14.98
9	4 78.98	433.26			-24.50	9	249.87	246.49	207.28	-2C.55	-10.92
10	440.92		343.00	-27.9R	-24.31	9	296.15	292.74	240.78	-23.00	-21.58
11		475.19	383.00	-25.57	-24.07	10	331.97	32 P . 5 5	281.78	-17.81	-16.60
	501.05	095.32	423.00	-14.45	-17.1C	11	71.57	368.14	326.78	-13.71	
12	536.21	530+47	463.00	-15 - 81	-14.57	12	524.72	521.03	427.78		-12.66
13	576.96	K 71 • 22	500.00	-15.39	-14.24	13	749.71	745.72		-22.66	-21.80
14	€00.33	594.58	532.00	-12.84	-11.76	14	906.36		504.28	-48.67	-47.88
15	649.77	644.01	564.00	-15-21	-14.19	14		901.99	593.28	-52.72	-52.03
16	708 - 23	702.46	604.00	-17.26	-16.30	-	967.37	962.99	642.78	-50.45	-49.62
1 7	752.89	747.11	644.CD	-16.91	-16.01	16	1033.04	1024.99	714.28	-44.63	-44.06
1 8	609.33	503.54	684.00	-10.32	-17.48	17	1050.56	1046.48	732.78	-43.37	-42.81
19	658.De	F52.29	724.00	-10.52	-17.72	18	1052.26	1048.16	741.78	-41.86	-41.31
20	915.97	010.16	764.00			19	1122.69	1118.59	837.28	-34.09	-33.60
			704100	-19.89	-19.13	20	1224.83	1220.71	931.78	-31.45	-31.01
ē 1	949.51	043.70	804.00	-18.10	-17.38	21	1351.74	1347.59			
2.2	1007.70	1001.96	844.00	-19.40	-10.72				1032.28	-30.95	-30.55
23	1548.65	1042.83	884.00	-18.63	-17.97						
2 4	1676.49	1064.67	924.00	-15.85	-15.22						
2 5	1063.57	1077.70	964.00	-12.40	-11.79						
26	1106.67	1100.95	1004.00	-10.23	-9.65						
27	1147.09	1141.27	1044.20	-9.87	-9.32						
2 F	1190.65	1185.03	1064.00	-9.86	-0.32						
29	1226.77	1222.94	1124.00	-9.32							
					-8 • 8 C						

WASHINGTON METROPOLITAN AREA TRANSTT AUTHORITY CONTRACT NUMBER 1F0021 F2A BRAYN ROUTE OUTPOUNO WASHINGTON, C.C.

WASHINGTON METPOPOLITAN APEA TRANSIT AUTHORITY CONTRACT NUMBER IFCO12 FIB NGOID OUTECUNO WASHINGTON, O.C.

WEEK	CALCUL CALCUL INTEGRATION	ATED	CUMULATIN HOU9S- ACTUAL	1 DIFF	ERENCF N SUPMATION	WEEK	CALCUL CALCUL INTEGRATION	ATEO	CUMULATIN HCUPS- ACTUAL	1 01FF	EFENCF IN SUMMATION
1	102.71	9₽+16	56.50	-&1.78	-59.57	1	34.65	32+12	39.00	11.16	17 • 6 3
2	233.62	219.10	149.00	-56.80	-47.C5	2	66.84	64.15	64.00	20.43	27.63
3	256.10	241.58	183.50	-39.57	-31.65	3	188.32	184.12	160.00	-17.70	- 1 ^E • 0 8
4	271.25	256.72	200.00	-35.62	-28.36	4	351.11	346.25	256.00	-37.15	-35.25
c	419.18	403.97	274.00	-52.99	-47.43	5	430.59	425.68	348.50	~23.55	-27 + 14
6	516.42	501.09	328.50	-57 • 21	-52.54	6	476.19	465.28	392.00	-19.95	-18.69
7	677.59	661.98	422.50	-60.39	-56.68	7	534 + 21	F20+26	478.0C	-11.76	-10 + 73
8	778.19	762.53	513.00	-51.69	-49.64	8	618.6C	613.64	581.50	-6 • 3 8	-5.53
9	943.95	928.14	621.50	-51.88	-49.34	9	640.93	635.98	638.50	38	.39
10	1084.94	1069.07	730.0C	-48.62	-46.45	10	694.33	689.37	705.00	1.51	7.72
1 1	1214 + 71	1198.79	832.50	-45.91	-44.00	11	715.84	710.87	755.CC	5.19	e . 8 4
1 2	1357.38	1341 + 41	916.00	-46.19	-46.44	12	768.56	763.59	812.00	5.35	5.96
13	1494.92	1479.92	989.5C	-51.08	-49.46	13	825.17	820.20	869.00	5 + C 4	r . 6 Z
- 14	1580.76	1564.75	1082.00	-46.10	-44.62	14	887.01	882.04	926.00	4 • 2 1	4.75
15	1600.50	1584.49	1135.50	-4C •95	-39.54	15	905.96	950.99	945.00	4 - 1 3	4.66
1 6	1625.54	1609.53	1180.50	-37.70	-36.34						

WASHINGTON HETPOPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMBER 1F7021 F2A BRAYTH ROUTE 1NBOUNG WASHINGTON, O.C.

WEEK	CUMULATIV CALCUL INTEGRATION	CUMULATIVE HOURS- % DIFFERENCE ACTUAL INTEGRATION SUMMATION			DASHINGION METROPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMBER 1F0012 F10 NCOPT INFOUND						
						WASH1	NSTON, D.C.				
2	48.25	47.64 154.67	17.50 104.00	-175.73 -57.89	-143.68 -48.72		CALCUL	ATED	CUMULATI:	1 01FF	ERENCE
3	205.09	195.50	139.00	-47.55	-40.65	MEEK	INTEGRATION	SUMMATION	ACTUAL	INTEGRATIO	N SUMMATION
2	205.09	19-450	139.00	-47.55	-40.65	1	55.68	54.10	56.0∏	-6.57	7.38
4	354.53	343.55	237.5C	-49.28	-44.65	2	227 24				
5	487.10	475.73	336.00	-44.97	-41.59	?	223.24	213.56	128.00	-74.40	-66.85
						3	331 + 17	321.21	209.50	-50.83	-54.06
6	588.77	577.28	399.50	-47.38	-44.50	4	404.90	394.90	265.00	-52.79	-49.02
7	762.59	750.79	511.00	-49.23	-46.93		101770	3742.0	20 7 41 0	-36.17	-49.02
٤	924.33	912.38	619.50	-49.21	-47.28	5	477.62	467.59	331.50	-44.08	-41.05
r	924.37	712.38	614.70	-49.21	-47.28	6	504.62	494.59	407.50	-23.83	-21.37
9	1697.72	1985.67	728.00	-50.79	-49.13	7	5 * 6 . 1 7				
19	1153.96	1141.91	801.00	-44.06	-42.56	,	549.17	539.13	476.7C	-15-20	-13+70
						P	612.91	602.86	562.70	-8.92	-7 - 14
11	1270 - 26	1258.19	961.50	-40.90	-30.57	9	717.80	707.70	658.20	-9.05	-7.52
12	1380.29	1368.20	1010.00	-36.66	-35.47					7.00	- 7 * 3 2
13	1498.13	1486.02	1100.00	-36.19	~3K +C9	10	802.94	792.82	722.7C	-11.10	-9.70 .
13	14.0.1.	1400.12	1100.00	-36+19	-3-469	11	869.49	859.36	787.20	-10.45	-0.17
14	1575.10	1562.99	1193.00	-32.03	-31 +0 I	12	890.46	080.33	70		
15	1590.07	1577.96	123° •50	-28.7C	-27.72	1.4	8-0.46	680*53	P14.70	-9.30	-0.06
1.	1693.15	1681.02	1368.50	-23.72	-22.84						
17	1725.75	1713.63	1421.50	-21 +40	-20 455						

#ASMINCTON METPOFOLITAN ARFA TPANSIT AUTHORITY CONTRACT NUMBER IFOUI2 FIR SOUTH OUTBOUND WASHINGTON, C.C.

WASHINGTON METROPOLITAN AREA TRANSIT AUTHORITY CONTRACT NUMBER 1F0012 FIP SOUTH INPOULD NAMED IN THE PROPERTY OF THE NORTH NAMED IN THE NAMED NASHINGTON, N.C.

8421	THAIL MA CECE										
b EEK	CUMULATTV CALCUL 1915/GRATION	ATEC	CUMULATIV HOURS- ACTUAL	% 01FF	ERENCF ON SUMMATION	WEEK	CUPULATII CALCUI INTEGRATION	LATED	CUMULATIV HOURS- ACTUAL	1 01FF	FERENCE ON SUMMAT 10
1	25.00	23.34	16.00	-56.55	-45.65	1	9.87	93.24	71.50	-39.68	-39.12
2	66.04	63.86	56.00	-17.94	-14.03	2	175.02	167.92	169.50	-3.26	.93
3	94.56	92.32	80.00	-18.20	-15.40	3	276.53	269.14	257.00	-7.60	-4.72
4	146.97	144.57	113.00	-30.06	-27.94	4	405.92	398.7€	343.00	-18.34	-16.12
5	219.28	216.71	177.00	-23.89	-22.44	r	545.62	537.86	430.50	-26.74	-24.94
6	201.27	288.62	254.50	-14.45	-13.41	6	614.91	607.13	487.00	-26.26	-24.67
7	376.18	367.45	332.00	-11.50	-10.68	7	721.97	714.17	575.0G	-25.56	-24.20
8	447.9R	445.21	435.50	-2.86	-2.23	ρ	641.68	833.85	668.50	-25.91	-24.73
9	509.83	507.05	507.00	56	01	9	946.46	938.60	767.50	-23.32	-22.29
10	521.9n	519.12	523.00	.21	.74	10	1040.56	1032.69	859.5C	-21.07	-20.15
1 1	542.49	539.71	554.00	2.08	2.58	1 1	1130 - 19	1122.32	943.50	-19.79	-18.95
12	598.67	595.98	623.50	3.98	4.43	12	1215.55	1207.67	1031.00	-17.90	-17.14
13	651.72	648.92	701.00	7.03	7.43	13	1284.93	1277.05	1113.00	-15.45	-14.74
14	666.51	663.71	724.50	8.30	8.39	14	1335.07	1327.19	1179.50	-13.19	-12.52
15	698.46	695.66	787.00	11.25	11.61						
16	766.88	764.07	872.50	12.11	12.43						
1 7	850.69	847.87	960.00	11.39	11.68						
1 4	809.43	896.61	1039.00	12.68	12.95	CONTRA	STON METPOP CT NUMPER 1 UTH INROUNC		TRANSIT AUT	HORITY	
19	975.92	973.10	1117.50	12.67	17.92		GTON. O.C.				
20		1064.04	1255.50	15.02	15.25		CALCUL	ATED	CUMULATIV	% OIFF	
21	1159.56	1156.71	1358.00	14.61	14.82	MEEK 1	NTFSPAT10N	SUMMATION	ACTUAL	INTEGRATIO	N SUMMATION

14.33

14.17

13.54

13.06

1434.00 14.13

1615.50 13.37

1711.00 12.89

1520.00

13.98

1228.55

1304.61

1396.70

1231.40

1307.47

1399.56

1490.37 1487.51

22

23

2 4

	CUMULATIV	E HOUPS	CUMULATIV	E			
CALCULATED			HOURS-	1 OIFFE	1 DIFFERENCE		
₩ EEK	INTEGRATION	SUMMAT10N	ACTUAL	INTEGRATION	SUMPATION		
1	75.48	68.55	96 • 00	21.38	28.59		
2	226.91	217.23	213.00	-6.53	-1.98		
3	395.15	384.71	332.50	-18.84	-15.70		
4	515.93	505.35	462.50	+11.55	-9.27		
۴.	614.30	603.67	569.50	-7.87	-6.00		
6	763.44	752.6E	764.50	-8.37	-6.84		
7	867.67	876.87	834.50	-6.37	-5.06		
6	994.16	977.33	949.50	-3.65	-2.°1		

-2.55

-1.46

9 1012.73 1001.90 987.50

Appendix A-6

The format of the keypunch cards used to record the weekly progress data from which the various equations were derived.

Variable meanings and values assigned are as follows. The dotted line represents the decimal point; the format is 7F10.5.

Variable No.	Description
1	The survey station at the beginning of the week's tunneling.
2	Lineal feet tunneled during the week.
3	Cumulative feet tunneled through the end of the week.
4	Tunneling hours during the week from Ring Logs.
5	Tunneling down hours in week due to shield and its ancillaries' failure.
6	Down hours in week due to excavating equipment; e.g., the rotating wheel and digger arm.
7	Down hours in week due to the conveyor belt.
8	Down hours in week due to muck transportation and/or the bringing in of necessary supplies; e.g., primary lining rings.
9	Down hours in week due to other work causes.
10	Down hours in week due to administrative decision; e.g., a shutdown for surveyor's alignment.
11	Total shift hours in week. Tunneling hours (4) plus down hours $(5+6+7+8+9+10) = total$ shift hours.

Variable No.

Description

Note: In some cases, tunneling did not begin immediately at the beginning of the week's first shift and frequently shutdown earlier than the end of the week's last shift. Where this was known, the interim time was assigned to administrative down hours (10). Where actual week's beginning and end times were unknown, the week's total shift hours were computed between the time for the first shove and the last ring erection.

- 12 Fraction of the face as silt and clay +1.
- Fraction of the face as clay and sand +1.
- 14 Fraction of the face as sand and gravel +1.
- Fraction of the face as cobbles and boulders + 1.
- Fraction of the face as cemented ground +1.
- Fraction of the face as peat and trash + 1.
- Fraction of the face as cohesive ground + 1.

Note: The sum of the fractions logged for variables 12, 13, 14, 15, and 17 should equal 1.

- Average tunnel pressure during the week-psig.
- A measure of the average wetness in the tunnel during the week. Refer to Section 4.2. The range is from 1.0 to 2.0.
- Driver horsepower to cutting wheel or digger arms.

 These data were not complete and therefore the variable was not used in the equation derivations.
- Total jacking potential of shield in short tons (2000 lb/ton). In some cases, the jacking potential was greater than the ring strength; a relief valve was installed in the hydraulic line to reduce the pressure. The reduced pressure is to be used in calculating the jacking potential tons.

Description Variable No. 23 Outside diameter of shield - ft. 24 If a rotating wheel excavator is used = 2, otherwise = 1. If an oscillating wheel excavator is used = 2, otherwise = 1. 25 None of the tunnels investigated used this equipment. 26 If a digger arm excavator is used = 2, otherwise = 1. If manual excavation is used = 2, otherwise = 1. 27 Note: In some tunnels, intial excavation was manual (2 logged) until the digger arm could be brought to bear. Then, due to the limited radius of the arm, excavation was 50 percent manual (1.5 logged) and 50 percent digger arm (1.5 logged). 28 If a conveyor belt and train are used = 2, otherwise = 1. 29 If a conveyor belt and truck are used = 2, otherwise =1. 30 If a rubber tired mucking truck is used = 2, otherwise = 1. 31 Fraction of the face as non-cohesive ground + 1. (This variable was eliminated as being the converse of variable 18.) 32 Fraction of the face as running ground + 1. 33 If ribs and lagging primary lining is used = 2, otherwise = 1. 34 If concrete pipe lining is jacked into place = 2, otherwise = 1. 36 If it was the last week of tunneling = 1, otherwise = 0. This was an added variable, and it was not practical to redo all the data sets to add a l or a 2. A l was added to all data sets for just the last week. During the computer data processing, a 1 was added to all number 36 variables so that the 1/2 relation would hold. 38 The tunnel RoA intercept. See Section 5.2. 39 The hours/ft for the shove operation. See Section 4.4. 40 The hours/ft for the ring erection. See Section 4.4.

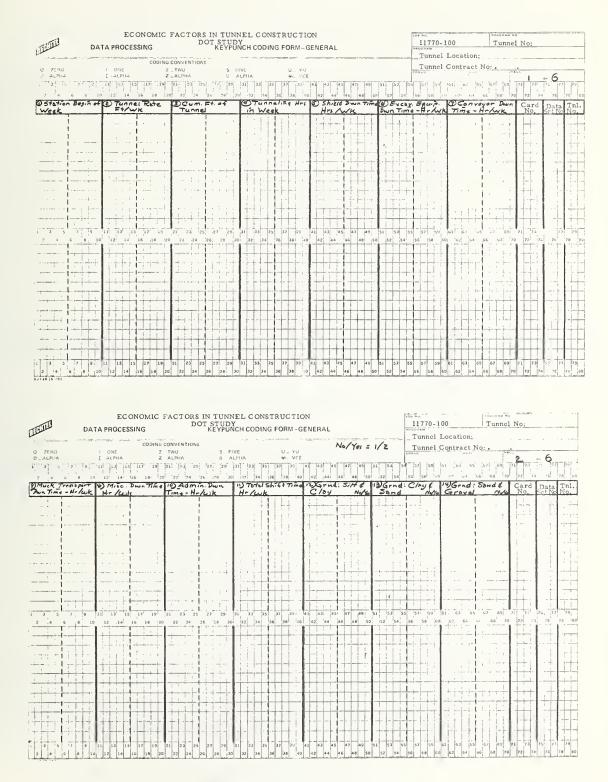
Variable No.

Description

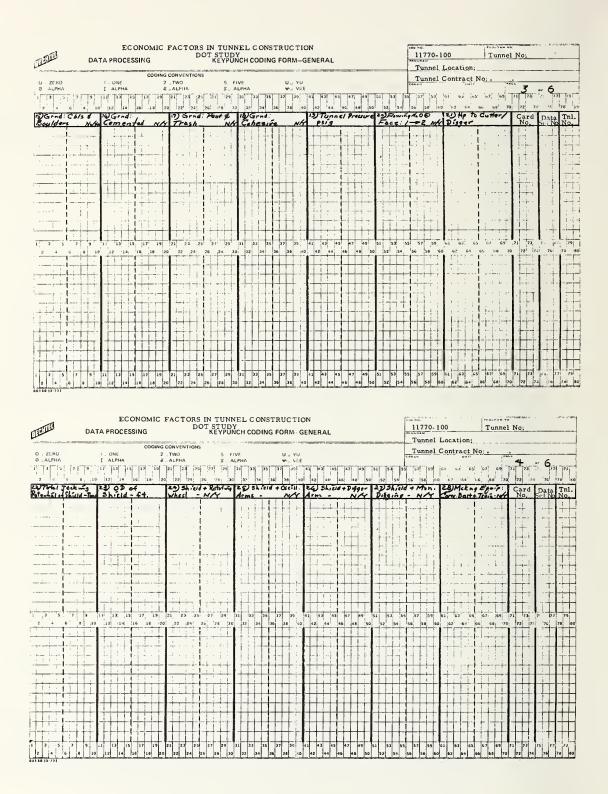
The hours/ft for the dead time. See Section 4.4.

Note: The data for variables 39, 40, and 41 were only obtained for tunnels in which the original ring logs were used for tunneling advance rates.

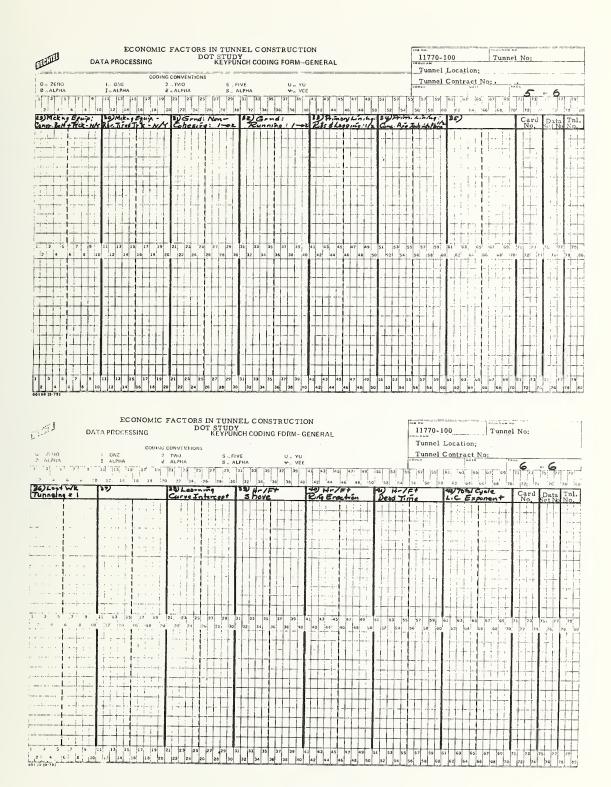
The learning curve RoA exponent. See Section 5.2.



Appendix A-6 Keypunch Forms



Appendix A-6 (Continued)



Appendix A-6 (Continued)



Appendix B

MEXICO CITY TUNNEL DATA

In this appendix, the data submitted by the contractor who conducted the tunneling effort for the Mexico City deep sewer (Ingenieros Civiles Asociados, S.A.) are presented for reference. It is felt that the data herein may be of value either to support or lead to modification of the equations derived in this report.

November 11, 1976

Bechtel Corporation Fifty Beal Street San Francisco, California 94119 U.S.A.

Attention: Mr. L.R. Damskey, Long Range Planning

In response to your wishes, we are sending you a report detailing the incidents during the period of excavation in one of the tunnels which we are drilling in the soils of Mexico City.

The adjoined information contains the details requested of us during your stay in this city and constitutes the complement to the data supplied earlier.

We would be grateful if, at the conclusion of your investigations, you would send us a copy of the final result of your studies.

Respectfully,

Engineer Manuel Salvoch Director

7. THE DRAINAGE PLAN

In this plot of land, it was necessary to proceed with a deep reduction of the level of the ground waters, in virtue of the fact that this level was localized at 10.0 m above the crown of the tunnel. Not to dewater this would have presented serious problems of piping in the sandy matter especially. The surface or deep-well type dewatering system covers 60 m ahead of and 40 m behind the face. It was made up of 15 shafts on the average and the capacity of the battery of pumps was 80 to 100 liters/each. The system remained installed and functioning for at least fifteen days previous to when the tunnel would pass through the corresponding zone and was maintained for the necessary time until the primary revetment of the concrete grout would be injected in its periphery.

In Figure B-1 is shown a plan of the line for lowering the level of the water by pump.

In Figure B-2 is presented a cross-section of a typical pump-shaft.

A. DESCRIPTION: CASE HISTORY DATA

1. PROJECT NAME: Federal District Deep Drainage

2. LOCATION: CENTRAL INTERCEPT TUNNEL: SHAFT AREA 11 -

SHAFT 13; excavation with shield stage.

3. OWNER: Head Office of Hydraulic Works of the Department

of D.F.

4. CONTRACTOR: TUNEL, S.A. de C.V.

5. DATES: START: 9/25/72 COMPLETE: 11/7/73

6. PROJECT SCOPE (INCLUDE ANY APPURTENANT STRUCTURES): The Federal District Deep Drainage System consists of a complex of tunnels which conduct by gravity the sewerage and rain waters from the Mexico Valley basin to a distant river in the state of Hidalgo. It is made up on two ancillary tunnels: the Central Intercept and the East Intercept, which unite in one major tunnel: the Central Emission tunnel (See plan I-2-5 annexed). The present report refers only to the stage of excavation with the shield, in alluvial soils in Mexico City, from the face of shaft 11 toward shaft 13 of the Central Intercept.

7. OWNER FURNISHED MATERIAL AND EQUIPMENT LIST Concrete grout
Steel for reinforcement
Type II cement
Tubing for the conductance of compressed air
Rails
Metal frames for shoring
Transformers for the electric current
Electric energy

8. OTHER OWNER SUPPLIED ITEMS (e.g. INSURANCE) Materials laboratory

CASE HISTORY DATA - (CONT.)

B. DESIGN INFORMATION

1.	PLAN AND PROFILE ATTACHED:	YES	NO
2.	TYPICAL SECTION DRAWING ATTACHED:	YES	NO
3.	TEMPORARY LINING DETAILS ATTACHED:	YES	NO
4.	PERMANENT LINING DETAILS ATTACHED:	YES	NO
5.	GEOLOGICAL PROFILE ATTACHED:	YES	NO

- 6. VERBAL DESCRIPTION OF SOIL CONDITIONS: Alluvial soils characteristic of Mexico City in its section named the transition zone. In this zone there are in general on the surface clay deposits and organic silts, covering very compressible clay volcanic strata of variable thickness interspersed with beds of compact silty sand or clear sand, which rest upon stiff layers in which the predominating substance is sand or silt. The natural water content in the clay formations and in the sandy silt is, on the argillaceous average, 200% and 40% respectively, displaying cohesion (obtained by means of simple cohesion tests) of 0.4 kg/cm² for the former and 0.3 and 0.6 kg/cm² for the latter.
- 7. DEWATERING PLAN ATTACHED: YES NO
- 8. GROUND WATER CONDITIONS DESCRIPTION: The normal level of ground water in the excavation zone of the tunnel is 10 meters above the crown. With the system of well-shafts this was brought down to below the tunnel invert. In spite of this system, in some sites with sandy substance, the use of WELL POINTS became necessary on the periphery of the face of the tunnel in order to channel the water deposits and remove them by pumping through the tunnel to the surface.
- 9. SITE PREPARATION AND RESTORATION DESCRIPTION: On the surface the CONTRACTOR supplied the land areas required for the installation of the deep well pumping system, since the project was localized for an inundation of Mexico City. Also, in the access shafts he supplied an area for the installations; towers, mantle capstans, offices, workshops, and storage grounds.

10. UNDERPINNING DESCRIPTION

11. UTILITIES DESCRIPTION: The tunnel remains localized at an average depth of 30.0 m. As a result it passes much below the municipal service lines so that there would not be a problem of relocation of the installations.

C. CONSTRUCTION METHODS

DESCRIPTIONS: The entire length considered in the present report was excavated in normal atmospheric pressure conditions. It was carried out by means of an open face shield of 6.42 m external diameter and 6.40 m length, with remote control hydraulic operation. In the rear it has a thrust system made up of 26 hydraulic jacks at 200 ton capacity each, which operate by resting against the primary revetment. In the front the shield bears 17 jacks with a capacity of 120 tons each, whose function is to hold the wood strut which supports the face. By means of pneumatic hammers operating manually the material of the face is loosened and falls to a lower central compartment, whence it is removed by an EIMCO 40 H air mucker of 1 m2 capacity mounted above platforms above the track. Then the convoy is pulled by a locomotive up to the shaft through which the muck is lifted to the surface, and from there is transported to the storage beds in back loader trucks (See Fig. B-3).

TEMPORARY LINING:

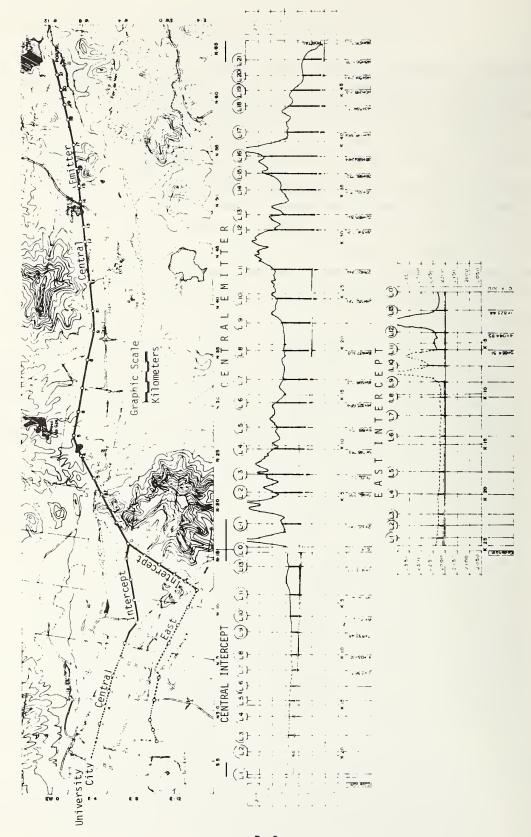
As the shield advances there is put into place the primary revetment, constituted of eleven segments of prefabricated reinforced concrete 1.50 m. long, 0.20 m. thick, and 0.75 cm. wide, which are connected with each other and with the preceding rings by means of screws and nuts, with which they reckon on the necessary cavities and ductile areas. In order to maintain the circular ring, it is propped up with tubular scaffolding equipped with machanical jacks for its adjustment. This support is maintained unit1 the zone is injected.

The segmented ring is set up with the aid of an eractor arm behind the shield's jacket, which has a thickness of 5 cm. Consequently, the advance of the shield leaves a void which is refilled immediately with gravel, applied with a small pneumatic conveyor.

CASE HISTORY DATA - (CONT.)

Ten meters behind the shield there takes place the process of injection of the cement grout in its refill or consolidation stage, later to pass on to the impermeability stage.

FINAL LINING: The tunnel bears a definitive revetment of concrete filtered on the site, maintaining a final surface of 5.00 mts. diameter. To make this a metallic frame formed by 9 telescopic sections 7.32 m. long, each is utilized. See Fig. B-4. The concrete is produced on the surface, lowered down the tunnel by gravity, loaded onto transport carts (See Fig. B-5), carried to the face, unloaded with the transport belt, fed into pneumatic conveyors, pumped, and filtered (See Fig. B-6).



B **-** 8

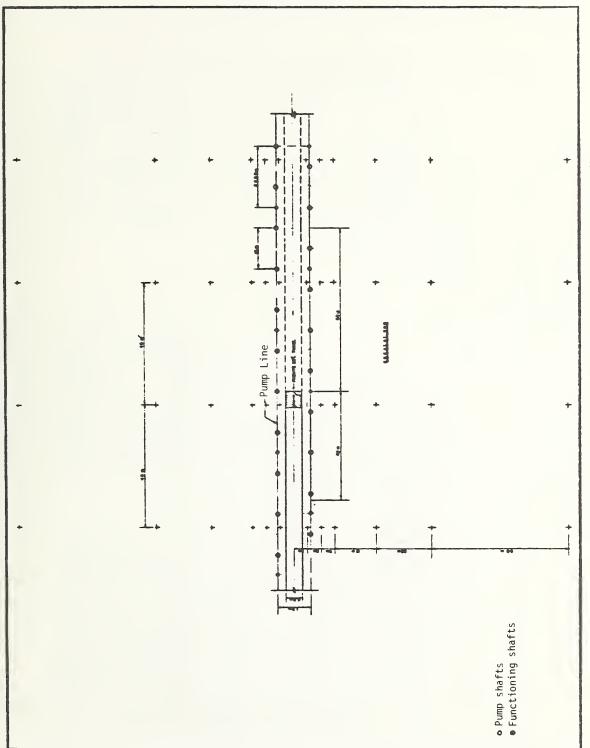


FIGURE B-1. PUMPING AND INSTRUMENTATION PLAN

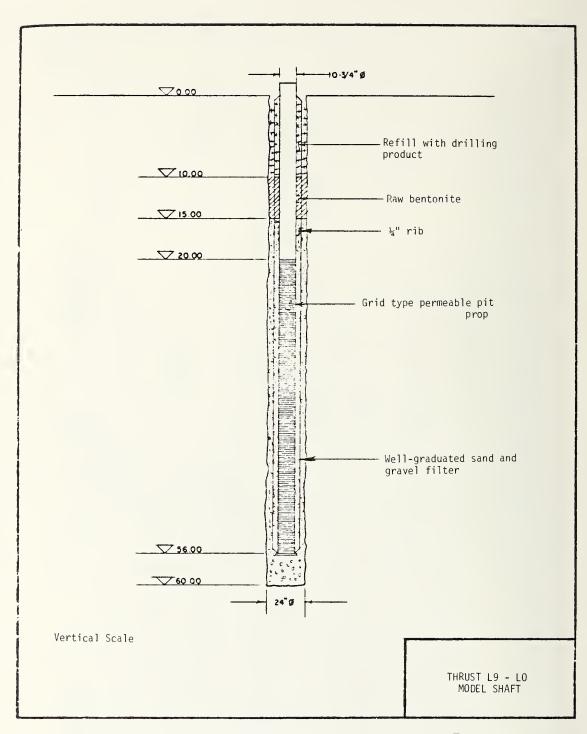


FIGURE B-2. CENTRAL INTERCEPT

FIGURE B-3, CENTRAL INTERCEPT

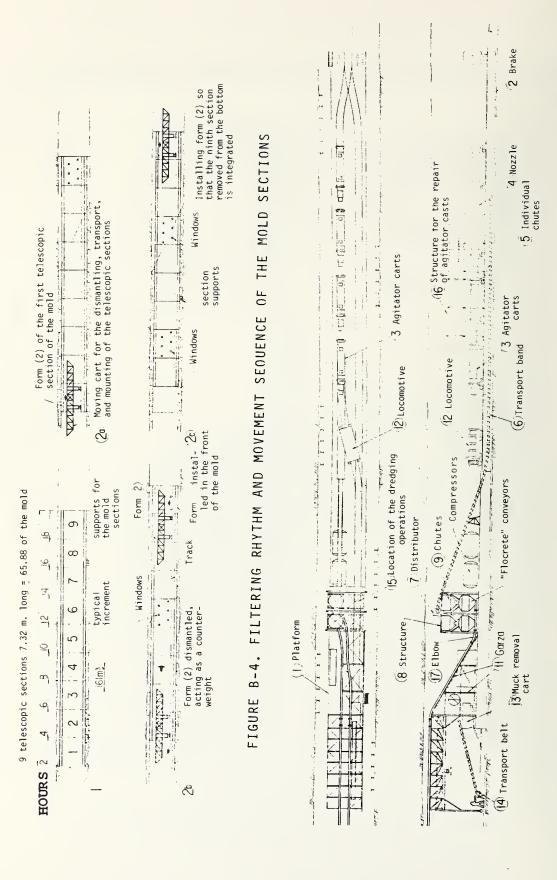


FIGURE B-6. FILTER TRAIN

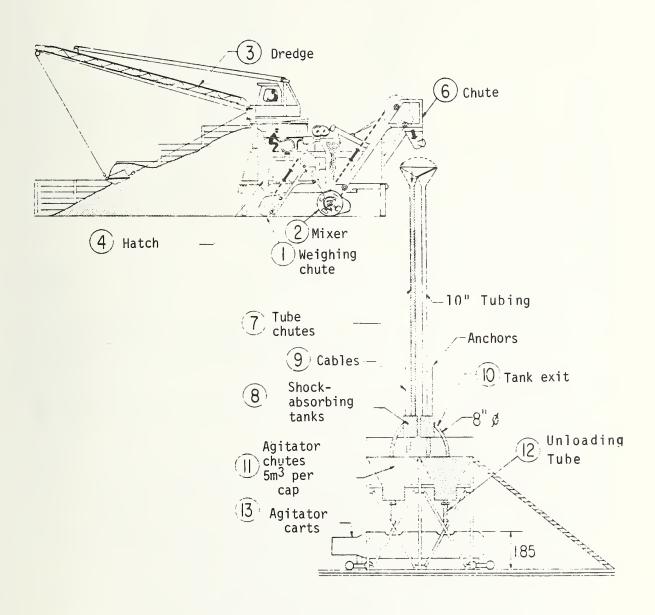


FIGURE B-5. PRODUCING AND UNLOADING OF THE CONCRETE

SHAFT FACE 11 - SHAFT 13 OF THE CENTRAL INTERCEPT

OBSERVATIONS				Installation of California switch and accomodation into the track							Serious problems of creep- ing sands and increase of the filtrations into the	face will make it necessary to install MELL POINTS in	the face.	Sands in the face with creeping water	Holiday 12/24/72	Holiday 1/1/73	Strong thrusts are noted in	the ground which deform the circle of voussoirs and	which are stopped by injecting the zone.	
Amount of water in the face (*)	2.00	1.75	1.75	1.75	1.75	1.75	1.75	1.75	1.75	2.00	2.00		2.00	2.00	2.00	2.00	2.00			
y E Due to neither personnel nor equip- ment hr/wk	09	24	18							∞	104		84	6.	108	88	100			
Break- down in the muck removal	(hr/wk)			104	12															
Break- down in the shield (hr/wk)									24	_										
Effective excavation work time hours/wk	8.4	120	126	40	132	144	144	144	120	136	40		09	52	36	99	44			
Cumul- ative advance m/wk	11.25	0	57,61	65.11	90.61	117,61	146.86	180.61	208.78	236.53	244.03		255.28	265.03	271.78	282.28	290.53			
Advance m/wk	11.25	22.75	23.61	7.50	25.50	27.00	29.25	33.75	28.17	27.75	7.50		11.25	9.75	6.75	10.50	8.25			
Chain	0+104.12	0+138.12	0+161.73	0+169.23	0+194.73	0+221.73	0+250.98	0+284.73	0+312.90	0+340.65	0+348.15		0+359,40	0+369.15	0+375.90	0+386.40	0+394.65			
Date	23-IX-72 30-IX-72	7-X-72	14-X-72	21-X-72	28-X-72	4-XI-72	11-XI-72	18-XI-72	25-XI-72	2-XII-72	9-XII-72		16-XII-72	23-XII-72	30-XII-72	6-1-73	13-1-73			

SHAFT FACE 11 - SHAFT 13 OF THE CENTRAL INTERCEPT

0BSERVATIONS	Strong thrusts in the ground, cracking the voussoirs.		HOI1day 2/5//3	The thrusts begin to be minor.				The shield of face 11-10 begins to operate so that from now on the same shaft services two faces.				Holidays 19, 20, 21/4/73		Holiday 5/1/73		Comparison of frame	progress; 0 + 768.46= 0 + 770.25.
Amount of water in the face (*)	2.00	2.00	1./5	1.75	1.75	1,75	1.75	1.75	1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50
Due to neither personnel nor equip- ment hr/wk	100 52	72	36	26	34	09	40	52	12		24	7.2	24	28	8	8	4
Silip Break- down in the muck removal system	(hr/wk)·																
Breakdown in the shield (hr/wk)			12		30												
Effective excavation work time hours/wk	44 92	72	96	88	80	84	104	9.5	132	144	120	7.2	120	116	136	136	140
Cumul- ative advance m/wk	298.78	328.03	340.78 358.03	374.53	388.78	404.53	424.03	441.28	466.34	501.59	529,34	542.84	565.34	587.09	612.59	638.09	664.34
Advance m/wk	8.25	12.00	12.75	16.50	14.25	15.75	19.50	17.25	25.06	35.25	27.75	13.50	22.50	21.75	25.50	25.50	26.25
Chain	0+402.90	0+432.15	0+444.90	0+478.65	0+492.90	0+508.65	0+528.15	0+545.40	0+570.46	0+605.71	0+633.46	0+646.96	0+669.46	0+691.21	0+716.71	0+742.21	0+768.46
Date	20-1-73	3-11-73	10-11-73	24-11-73	3-111-73	10-111-73	17-111-73	24-111-73	31-111-73	7-14-73	14-IV-73	21-1V-73	28-1V-73	5-V-73	12-V-73	19-V-73	26-V-73

SHAFT FACE 11 - SHAFT 13 OF THE CENTRAL INTERCEPI

OBSERVATIONS		Introduction of large volume of water into the face 46 liters Exploratory and drainage boreholes are made in the face.
Amount of water in the face (*)	1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50	2.00 2.00 2.00 2.00 1.75 1.75 1.75
VE to Due to neither personnel nor equip-	16 4 4 28 12 12 4 4 40	124 108 124 100 32 4
Break- down in the muck removal	(hr/wk)	
Breakdown in the shield (hr/wk)		
Effective excavation work time (hr/wk)	128 140 144 136 136 132 144 144 140 120	20 20 20 44 112 140 132 144 144
Cumul- ative advance m/wk	688.34 714.59 741.59 767.09 788.84 813.59 840.59 869.09 899.09 926.84 958.34	1007.09 1008.59 1012.34 1020.59 1071.59 1097.84 1129.34 1162.34
Advance m/wk	24.00 26.25 27.00 25.50 21.75 24.75 30.00 30.00 27.75 31.50	3,75 1,50 3,75 8,25 21.00 30,00 26,25 31.50 33.00
Chain	0+794.25 0+820.50 0+847.50 0+873.00 0+894.75 0+919.50 0+916.50 0+975.00 1+005.00 1+005.00 1+089.00	1+113.00 1+114.50 1+118.25 1+126.50 1+147.50 1+177.50 1+203.75 1+203.75 1+268.25 1+268.25
Date	2-VI-73 9-VI-73 16-VI-73 23-VI-73 30-VI-73 7-VII-73 14-VII-73 21-VII-73 4-VIII-73 11-VIII-73 18-VIII-73	1-1X-73 8-1X-73 15-1X-73 22-1X-73 29-1X-73 6-X-73 13-X-73 20-X-73 27-X-73 3-X1-73

SHAFT FACE 11 - SHAFT 13 OF THE CENTRAL INTERCEPT

OBSERVATIONS	Holiday 11/20/73 The tunnel is connected.
Amount of water in the face (*)	1.75 1.75 1.75 1.75
ue to either ersonnel or equip-	4
wn Break- D down in m the muck p removal	(hr/wk)
Breakdown in the shield (hr/wk)	
Effective excavation work time hours/wk	144 144 144 104
Cumul- ative advance m/wk	1233.59 1294.34 1333.34 1354.81
Advance m/wƙ	35.25 33.00 27.75 39.00 21.47
Chain	1+339.50 1+372.50 1_400.25 1+439.25 1+460.72
Date	10-XI-73 17-XI-73 24-XI-73 12-XII-73 7-XII-73



Appendix C

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Appendix D

REPORT OF INVENTIONS

No new inventions were developed during this study. Existing principles were applied to a problem in a new way, and a logic of problem-solution was developed.

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